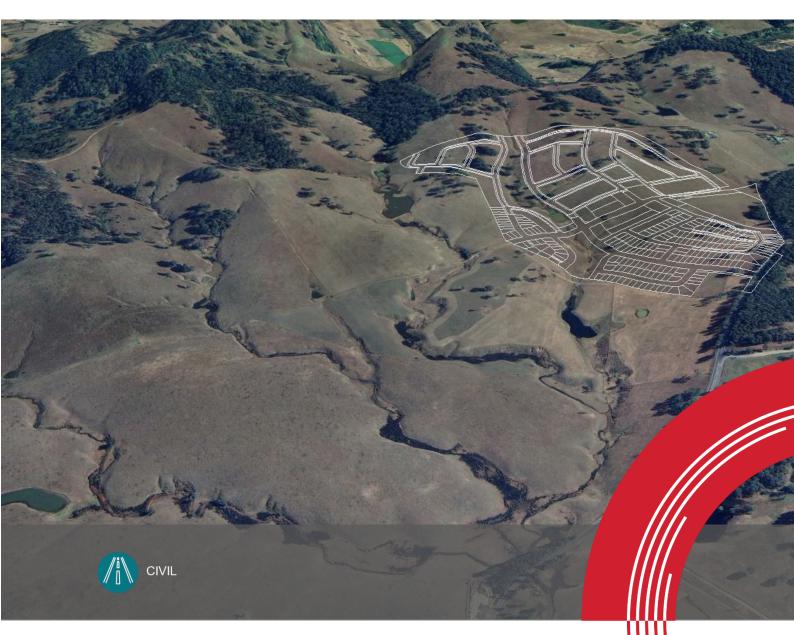
# NORTHROP



# Flood Impact and Risk Assessment

for

## 559 Anambah Road, Gosforth

for Thirdi Anambah Pty Limited

NL222055 / 30 August 2024 / Revision A

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## **Acronyms**

1D One-Dimensional2D Two-Dimensional

AEP Annual Exceedance Probability

AHD Australian Height Datum

ARR 2019 Australian Rainfall and Runoff 2019

BoM Bureau of Meteorology

DA Development Application

DCP Development Control Plan

DRAINS 1D - Hydrodynamic Modelling Software

DTM Digital Terrain Model

EY Exceedances per Year

FIRA Flood Impact and Risk Assessment

GPU Graphics Processing Unit

GSDM Generalised Short-Duration Method

Ha Hectares – Measure of Area

HPC Heavily Parallelised Computation

IFD Intensity-Frequency-Duration

LGA Local Government Area

LiDAR Light Detection and Ranging Terrain Data (also see ALS)

m Measure of length / height / distance (metres)

m AHD Meters above Australian High Datum

m/s Measure of velocity (metres per second)

m³/s Measure of flow rate (cubic metres per second)

PMF Probable Maximum Flood

OSD On-site Detention

RAFTS Hydrologic model

SW Storm Water

TP Temporal Pattern

TUFLOW A 1D and 2D hydraulic modelling software



## Introduction

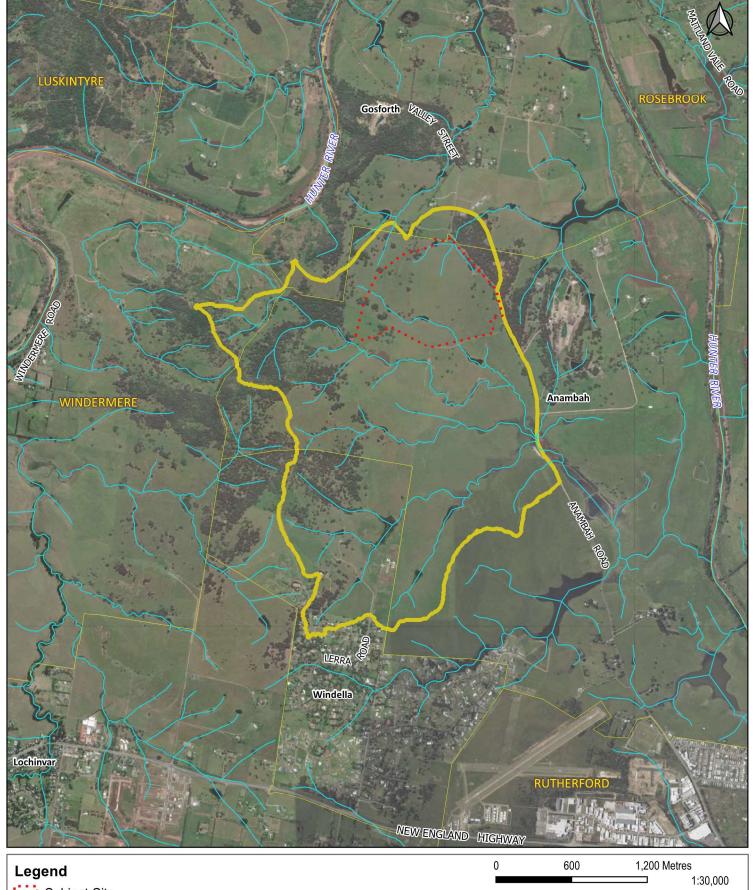
Northrop Consulting Engineers have been engaged by Thirdi Anambah Pty Limited to prepare a Flood Impact and Risk Assessment (FIRA) for the proposed residential development located at 559 Anambah Road, Gosforth, herein referred to as the subject site or the site. The subject site locality is presented in **Figure 1** overleaf.

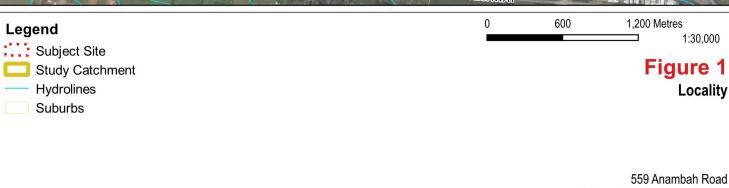
This FIRA aims to review the impact the proposed development has on existing flood behaviour within the subject site, adjacent properties and downstream areas, and has been prepared to support the Development Application (DA) to Maitland City Council (MCC).

This assessment has been prepared with the consideration of the following guidelines and documents:

- Maitland Development Control Plan (DCP 2011).
- Maitland City Council Manual of Engineering Standards 6 Stormwater Drainage (MOES).
- Australian Rainfall and Runoff 2019 Guidelines (ARR 2019).
- Flood Risk Management Manual The Management of Flood Liable Land (NSW Government June, 2023 "the manual").

		Date
Prepared by	RB	30/08/2024
Checked by	GB	30/08/2024
Admin	GB	30/08/2024





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## Methodology

This assessment has been undertaken generally using the following procedure:

- Desktop review of available previous investigations and information including design plans, LiDAR and survey data, stormwater infrastructure information and land use classifications.
- Preparation of a RAFTS (in DRAINS) hydrological model to determine the 10%, 5%, 1%, 1 in 500 AEP and PMF flows derived from the local upstream catchment.
- Preparation of an Existing Case two-dimensional TUFLOW hydraulic model to quantify the existing flood behaviour across the model extent.
- Modification of the Existing Case RAFTS (in DRAINS) hydrologic and TUFLOW hydraulic model to include the proposed development layout and terrain, creating the Developed Case and Developed Case Stage 1 scenarios.
- A comparison of the Existing and Developed case results to review the impact the proposed development has on the existing flood behaviour on-site, in adjacent properties and downstream areas has also been prepared.

This study has been prepared with consideration to the following plans and reports:

- Architectural plans prepared by PAA Design architects.
- Civil drawings and design surfaces prepared by Northrop Consulting Engineers.
- Detailed site survey plan prepared by Delfs Lascelles Surveyors.
- Council's Lochinvar Flood Study prepared by WMAwater in 2019.



## Subject Site and Proposed Development

## **Subject Site**

The subject site is located within the Maitland City Council (MCC) Local Government Area (LGA) at 559 Anambah Road, Gosforth and is contained within parcels of land known as Lot 55 DP 8741070 and part of Lot 177 DP 874171. The total site area is approximately 66 hectares with terrain elevations ranging from approximately 19m AHD to 58m AHD. An average slope of approximately six percent is observed across the site. The site current land use is predominantly grassland, scattered trees/shrubs and farm dams.

The site is surrounded by rural landscapes and has approximately 700m frontage adjacent to Anambah Road to the north-east. The typical existing site frontage is presented in **Photos 1** and **2** below



Photo 1 - Anambah Road Frontage (Google Maps 2024), Looking to North-West



Photo 2 - Anambah Road Frontage (Google Maps 2024), Looking to South



## **Study Catchment**

The study catchment extent is shown in the above **Figure 1**. The catchment predominantly falls from the west and directs runoff towards the Hunter River floodplain. Three major ephemeral watercourses traverse the catchment and generally drain from the west to the east towards Anambah Road culvert crossings. From Anambah Road, these watercourse discharge to the Hunter River. There are also two minor drainage paths discharging to the north. A summary of the catchment characteristics is presented in **Table 1** below.

Table 1 - Study Catchment Characteristics

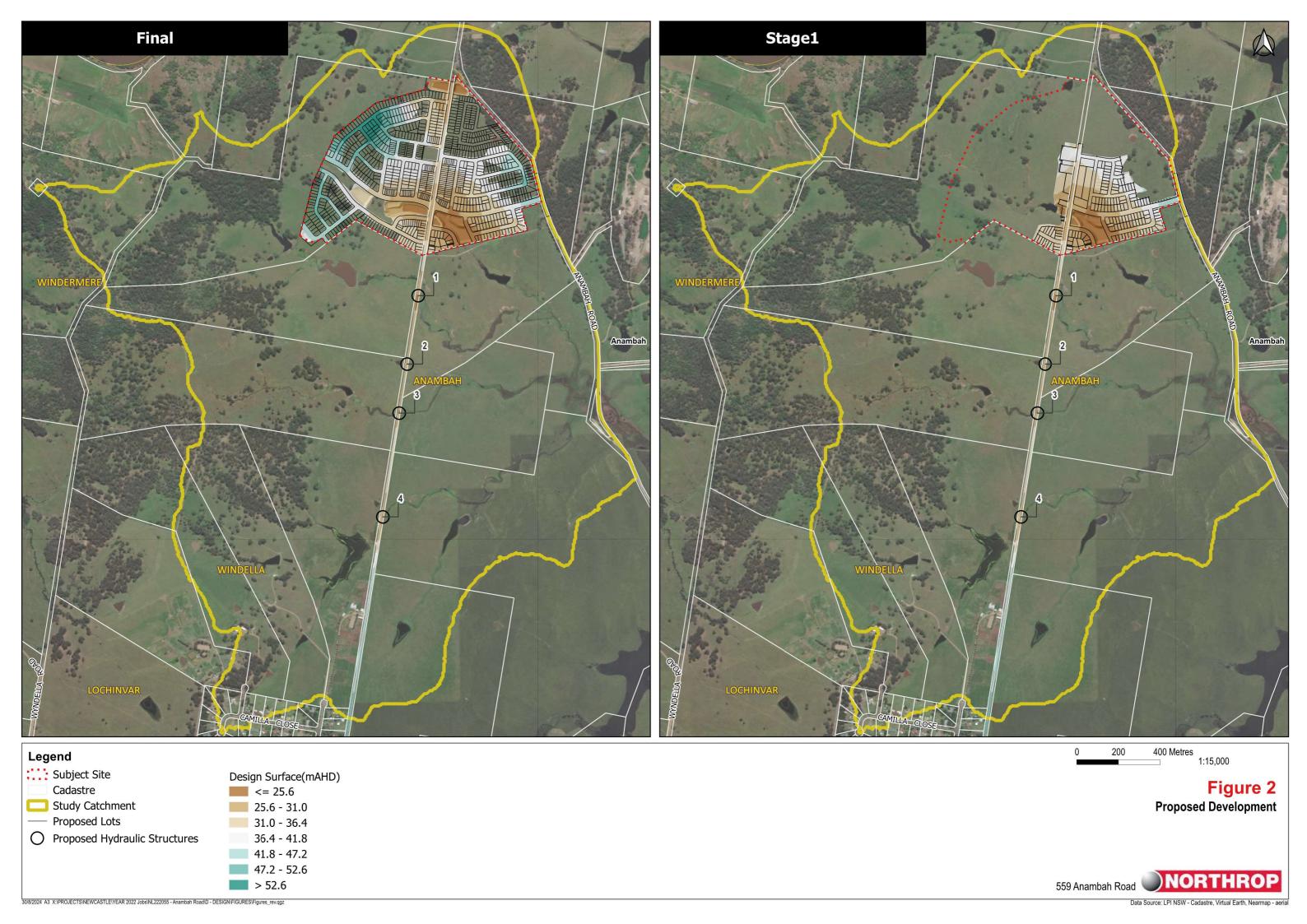
Characteristics	Value
Total Area (ha)	555
Average Elevation (m AHD)	44
Highest Elevation (m AHD)	173
Lowest Elevation (m AHD)	8
Average Slope (%)	9
Typical Land Use	Grassland and Pastures, Bushland, Scattered Shrubs and Trees, Farm Dams, Rural Residential, Low-density Residential, Sealed and Unsealed Roads.

#### **Proposed Development**

The proposed residential subdivision consists of approximately 900 low and medium density residential lots, a local park located centrally within the site, access road, and stormwater quantity and quality treatment infrastructure.

As a part of the development, construction of a local emergency access road is proposed along the existing River Road reserve. The road will establish connection with residential areas of Windella located approximately 2.2km to south and provide flood free egress (up to the 1% AEP local catchment flood) for the development in case of potential inundation of Anambah Road during major local catchment flood events or/and Hunter River flooding.

This report has been prepared to support the proposed concept master plan and Stage 1 works. The proposed subdivision works for Stage 1 relate to the southeastern section of the subject site. The proposed subdivision layouts, design surfaces for both the concept master plan and Stage 1 including locations of the proposed four hydraulic structures (Culverts) along River Road, are shown in **Figure 2** overleaf.





## Model Parameters

Detailed two-dimensional hydraulic modelling was undertaken using the TUFLOW hydrodynamic modelling software. One-dimensional DRAINS modelling software has been used to configure and size on-site detention basins/hydraulic structures and generate runoff inflows for the TUFLOW model. The hydrological and hydraulic model parameters are presented below.

## **Hydrological Model**

The DRAINS modelling software with RAFTS hydrology used in this assessment. As recommended by the latest Australian Rainfall and Runoff (ARR) 2019 guidelines the Initial and Continuing Loss (ILCL) model, coupled with median pre-burst rainfall has been adopted in this study.

Hydrological parameters including rainfall losses, pre-burst rainfall depths, catchment Manning's 'n' values were sourced from Council's Lochinvar Flood Study (WMAwater 2019). Lochinvar Creek catchment is an adjacent catchment and located west of the study catchment.

The input data for the hydrology model used in this study includes sub-catchment data, design rainfall, temporal patterns, pre-burst rainfall and the Initial and Continuing Losses. These are summarised below in **Table 2**.

#### **Sub-Catchment Properties**

Sub-catchments have been delineated using a combination of LiDAR, aerial imagery, cadastral boundaries, and detailed survey for the existing, developed and Stage1 development cases. The following **Table 2** presents the sub-catchment properties, and the catchment extents for both existing and developed cases are presented in **Figure 3** overleaf.

Table 2 - Existing Sub-Catchment Properties

Catchment Reference	Area (ha)	Vectored Slope (%)	Effective Impervious (%)	Catchment Reference	Area (ha)	Vectored Slope (%)	Effective Impervious (%)
C01	5.57	8.3	0	C26	10.84	6.5	0
C02	16.43	13.3	0	C27	15.68	6.5	0
C03	5.39	11.0	0	C28	10.04	10.1	0
C04	22.14	7.8	0	C29	9.27	12.8	0
C05	6.67	6.4	0	C30	13.25	14.9	0
C06	15.75	14.5	0	C31	5.02	6.3	0
C07	12.03	21.3	0	C32	14.45	10.7	0
C08	9.70	15.7	0	C33	11.76	8.6	0
C09	8.44	8.8	0	C34	10.28	6.4	0
C10	17.14	7.2	0	C35	3.89	8.4	0
C11	8.70	7.0	0	C36	10.63	13.8	0
C12	9.45	7.3	0	C37	10.31	7.8	0
C13	5.60	13.0	0	C38	4.33	9.0	0
C14	6.11	5.9	0	C39	9.88	7.9	0
C15	20.55	6.8	0	C40	7.23	12.5	0
C16	14.97	8.4	0	C41	10.56	25.2	0



Catchment Reference	Area (ha)	Vectored Slope (%)	Effective Impervious (%)	Catchment Reference	Area (ha)	Vectored Slope (%)	Effective Impervious (%)
C17	19.43	10.4	0	C42	10.07	6.7	0
C18	19.54	8.3	0	C43	6.07	12.5	0
C19	26.07	7.6	0	C44	8.43	5.9	0
C20	9.84	9.0	0	C45	12.05	7.8	0
C21	15.10	7.3	0	C46	14.01	5.9	0
C22	9.63	12.4	0	C47	10.73	16.1	0
C23	12.78	6.6	0	C48	7.33	18.5	0
C24	17.31	6.4	0	C49	7.50	7.7	0
C25	7.38	5.5	0				

Sub-catchments over the extent of the proposed development have been further refined to capture proposed modifications to the terrain and land use introduced as part of the development. A typical impervious fraction of 64% has been assumed over the extent of the proposed development.

A summary of the developed catchments is presented in the below **Table 3** and **Figure 3** overleaf.

**Table 3 - Developed Case Catchment Properties** 

Catchment Reference	Area (ha)	Vectored Slope (%)	Effective Impervious (%)	Catchment Reference	Area (ha)	Vectored Slope (%)	Effective Impervious (%)
C02	16.43	13.3	0	C31	5.02	6.3	0
C03	5.39	11.0	0	C32	14.45	10.7	0
C04	22.14	7.8	0	C33	11.09	8.9	0
C05	3.68	6.0	0	C34	12.26	6.1	0
C06	15.75	14.5	0	C35	2.31	9.7	0
C07	12.03	21.3	0	C36	10.63	13.8	0
C08	9.70	15.7	0	C38	2.11	9.3	0
C09	8.44	8.8	0	C39	9.25	8.1	0
C10	17.14	7.2	0	C40	7.23	12.5	0
C11	8.70	7.0	0	C41	10.56	25.2	0
C12	9.45	7.3	0	C42	10.07	6.7	0
C13	6.63	12.1	0	C43	6.07	12.5	0
C15	20.55	6.8	0	C45	6.93	7.3	0
C16	14.97	8.4	0	C46	14.01	5.9	0
C17	19.43	10.4	0	C47	10.73	16.1	0
C18	19.54	8.3	0	C48	7.33	18.5	0
C19	26.07	7.6	0	C49	7.50	7.7	0
C20	9.88	9.1	0	D01	2.36	3.5	64
C21	15.06	7.3	0	D02	3.65	3.5	64



Catchment Reference	Area (ha)	Vectored Slope (%)	Effective Impervious (%)	Catchment Reference	Area (ha)	Vectored Slope (%)	Effective Impervious (%)
C22	9.63	12.4	0	D03	3.03	3.0	64
C23	12.78	6.6	0	D04	1.53	3.5	64
C24	17.31	6.4	0	D05	20.72	3.0	64
C26	1.67	5.0	0	D06	7.02	3.0	64
C27	13.01	6.4	0	D07	10.34	3.5	64
C28	10.04	10.1	0	D08	7.32	3.5	64
C29	9.27	12.8	0	D09	3.84	3.5	64
C30	13.25	14.9	0				





#### **Burst Rainfall**

The latest ARR 2019 rainfall has been obtained from the Bureau of Meteorology (BoM) while the accompanying rainfall temporal patterns have been obtained by the ARR Data Hub for a location over the study catchment.

ARR 2019 recommends the use of the storm ensemble method using 10 temporal patterns for each storm duration. For this investigation, storm durations ranging from the 10, 15, 20, 25, 30, 45-minute, 1, 1.5, 2, 2.5, 3, 4, 4.5, 5, 6-hour for 10%, 5%, 1%, 1 in 500 AEP and PMF design storm events were assessed in the hydrological model. The following **Table 4** presents the rainfall depths used for the investigation.

Areal Reduction Factor (ARF) was not applied to design rainfall due to the size of the catchments. We believe this is an appropriately conservative assumption.

1 in 500 **Duration** 10% AEP **5% AEP 1% AEP PMF AEP** 10 min 20.2 23.8 33.3 44.0 15 min 25.3 29.8 41.8 55.2 160 20 min 29.0 34.2 47.9 63.4 25 min 32.0 37.7 52.6 69.7 34.4 74.9 30 min 40.6 56.4 230 45 min 39.9 47.0 64.9 86.3 300 1 hour 43.9 51.6 71.2 94.5 340 1.5 hour 50.0 58.7 80.7 107 420 2 hour 54.9 64.4 88.4 117 480 2.5 hour 520 62.7 73.7 101 134 560 3 hour 4 hour 620 4.5 hour 72.4 \_ 85.2 118 155 5 hour 680 \_ \_ 95.2 720 6 hour 80.7 133 174

Table 4 - IFD Rainfall Depths (mm)

#### **Pre-Burst Rainfall**

The median (50%-percentile) pre-burst rainfall depths have been adopted for the purposes of the investigation. These were obtained from the ARR Data Hub for a location over the study catchment and consistent with the pre-burst depths used in the Lochinvar Flood Study. **Table 5** presents the median pre-burst rainfall depths used for the assessment.

1 in 500 **Duration** 10% AEP **5% AEP 1% AEP AEP** 10 min 1.6 1.9 1.4 1.4 15 min 1.6 1.9 1.4 1.4 1.4 1.4 20 min 1.6 1.9

Table 5 - Median Pre-Burst Rainfall Depths (mm)



Duration	10% AEP	5% AEP	1% AEP	1 in 500 AEP
25 min	1.6	1.9	1.4	1.4
30 min	1.6	1.9	1.4	1.4
45 min	1.6	1.9	1.4	1.4
1 hour	1.6	1.9	1.4	1.4
1.5 hour	1.6	2.1	1.2	1.2
2 hour	2.5	3.3	3.4	3.4
3 hour	1.2	1.3	2.7	2.7
4.5 hour	3.3	4	5.7	5.7
6 hour	5.3	6.6	8.7	8.7

### **Infiltration Losses and Catchment Roughness**

As mentioned above, the Initial and Continuing Loss (ILCL) model has been used for this study with the storm losses obtained from Council's Lochinvar Flood Study. The ILCL method simulates catchment storage as an initial loss in rainfall followed by a constant loss rate (continuing loss). For PMF event, zero initial and continuing loss was adopted. The following **Table 6** presents the Initial and Continuing losses used for the analysis.

**Table 6 – Infiltration Loss Parameters** 

Land Use	Initial Loss (mm)	Continuing Loss (mm/hr)
Modelled Pervious	18.0	2.0
Modelled Effective Impervious	0.0	0.0
PMF Modelled Pervious	0.0	0.0
PMF Modelled Effective Impervious	0.0	0.0

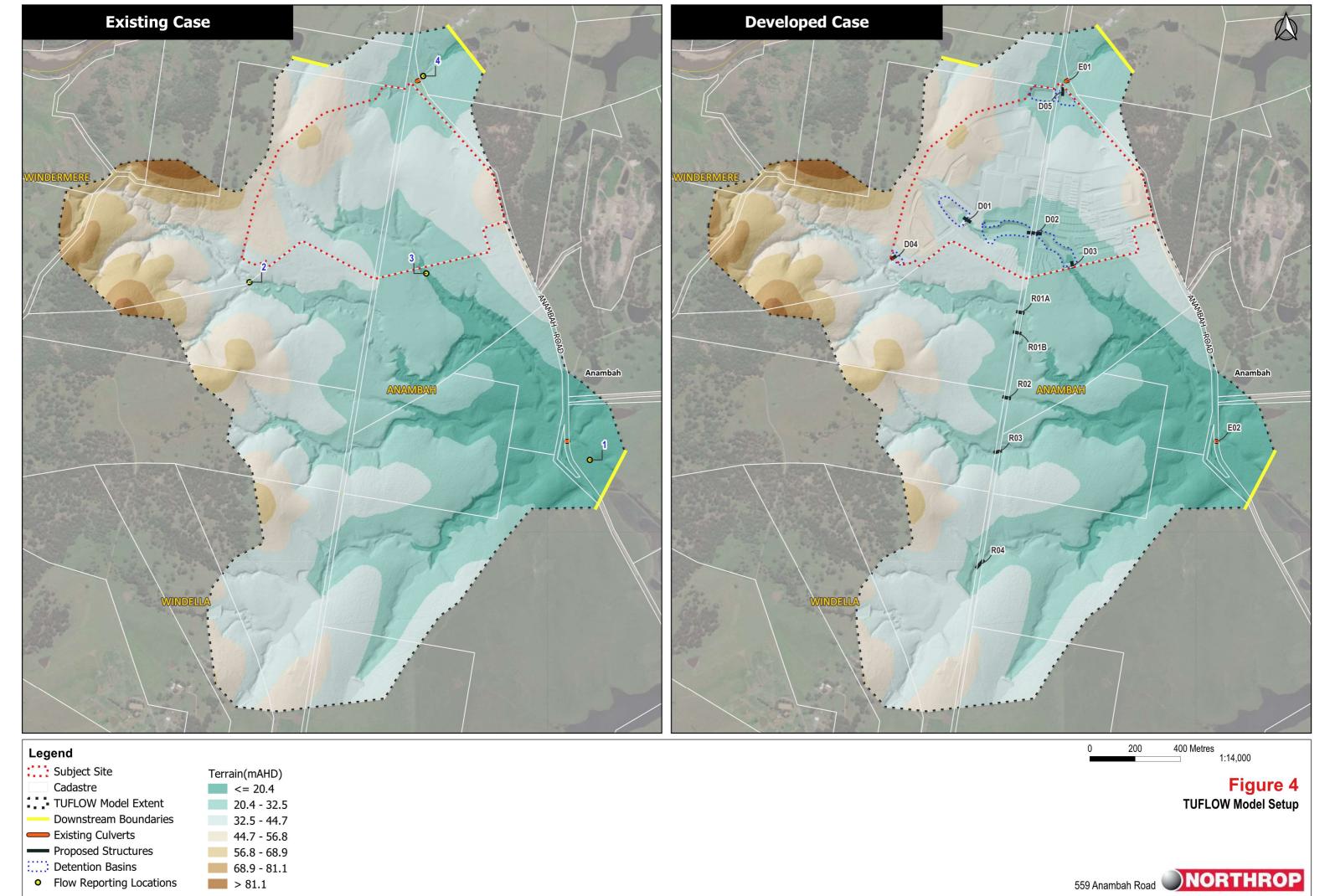
A hydrological roughness of 0.015 has been used for impervious areas which is consistent with concrete surfaces and roads while, roughness value of 0.040 have been adopted for pervious areas which are consistent with predominantly grassed areas expected over rural catchments.

### **Hydraulic Model**

The hydraulic model used for this study is the combined 1D/2D TUFLOW hydrodynamic software. For this study, the TUFLOW version 2020-10-AD with HPC GPU solver has been used.

#### **Model Domain**

The TUFLOW model extent is presented in **Figure 4** overleaf for both existing, developed and developed Stage1 conditions. The TUFLOW model terrain was developed using a combination of the latest LiDAR, detailed topographical survey and design surfaces. A 1.5 metre grid size was adopted in this flood assessment as it was determined to provide a reasonable balance between model run time and flood behaviour through watercourses.





## **Boundary Conditions**

Sub-catchment flows derived by the RAFTS (in DRAINS) model were applied directly to the two-dimensional grid via a series of inflow polygons. Three model outlet boundaries are shown in **Figure 4**. A "HQ" boundary was used for each of the outlets with a "free outflow" tailwater condition and slopes generally consistent with the observed existing terrain grades at the location of the outlet boundaries.

### **Hydraulic Structures**

The location of the modelled existing and developed case stormwater infrastructure entered the twodimensional TUFLOW model is presented in **Figure 4**.

A summary of modelled existing and proposed hydraulic structures (refer to **Figure 4** for locations) is presented in the following **Table 7**. Blockage factor of 25% has been used for all road crossing structures for all modelled events. The applied 25% blockage is generally consistent with the latest ARR 2019 blockage guidelines for small predominantly rural and with moderate slope catchments.

**Table 7– Proposed Hydraulic Structures** 

Culvert Reference	Description	Type and Size
E01	Existing Anambah Rd Crossing North	RCP 2 x D0.75m
E02	Existing Anambah Rd Crossing South	RCP 4 x D1.80m
R01A	Proposed River Road	RCBC 6 x W 2.70m x H 0.90m
R01B	Proposed River Road	RCBC 1 x W 2.70m x H 0.90m
R02	Proposed River Road	RCBC 3 x W 1.20m x H 0.90m
R03	Proposed River Road	RCBC 5 x W 1.80m x H 0.90m
R04	Proposed River Road	RCBC 3 x W 3.60m x H 1.20m
D01	Proposed Basin Outlet	RCP 1 x D0.9m Weir width 10m, depth 0.5m
D02	Proposed Basin Outlet	RCBC 1 x W1.5m x H1.5m
D03	Proposed Basin Outlet	RCP 2 x D0.75m RCBC 1 x W1.8m x H0.6m Weir width 15m, depth 0.35m
D04	Proposed Basin Outlet	RCP 1 x D1.5m
D05	Proposed Basin Outlet	RCP 1 x D0.6m RCBC 1 x W1.8m x H0.6m Weir width 7m, depth 0.4m

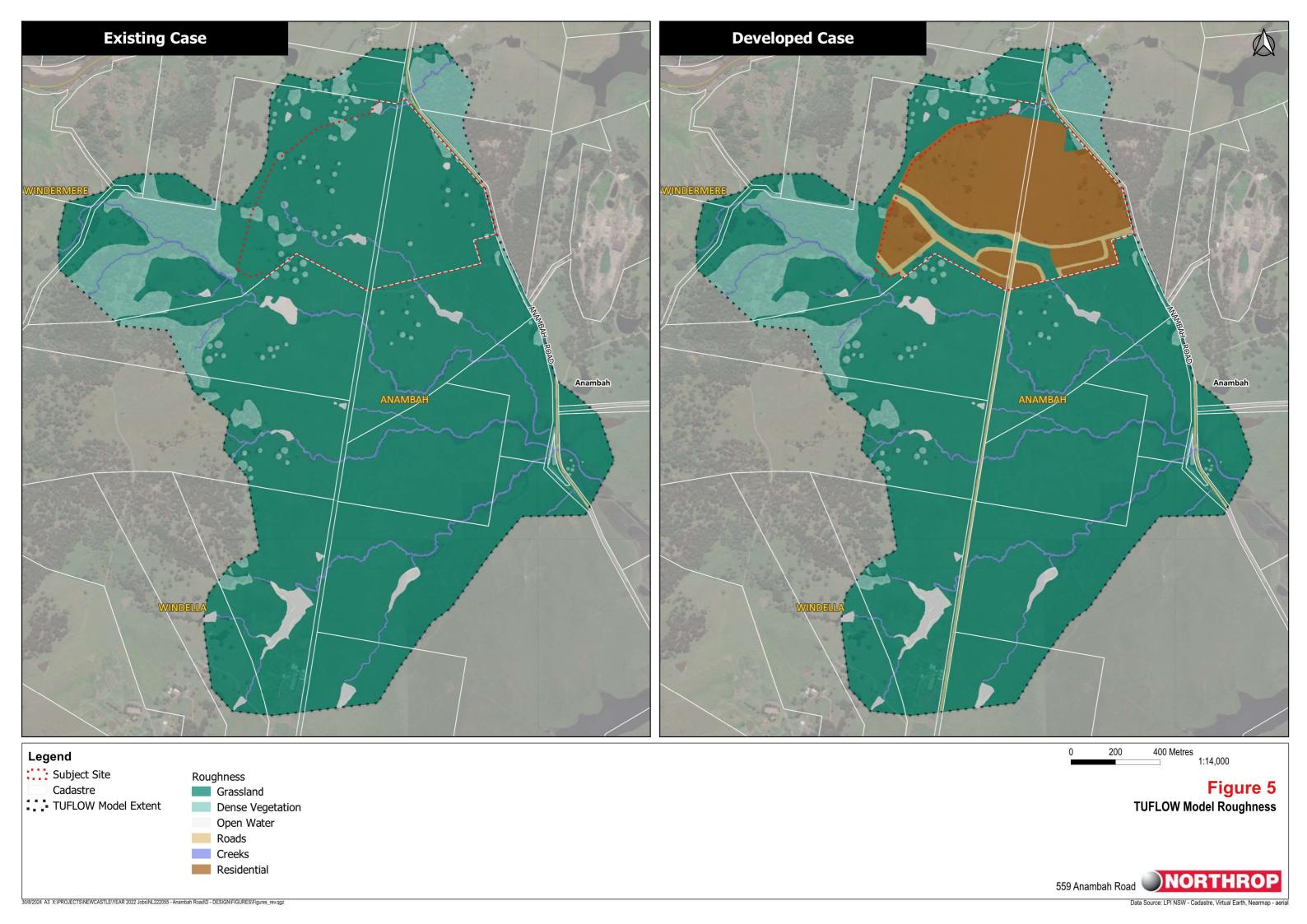


## **Hydraulic Roughness**

The following **Table 8** below presents the modelled land use and the adopted surface roughness values. The adopted surface roughness values are consistent with values used in the Lochinvar Flood Study. The modelled TUFLOW land use roughness areas for both existing and developed conditions are shown in **Figure 5** overleaf.

Table 8 - Land Use Roughness (Manning's)

Land Use	Roughness (Manning's)
Dense Vegetation	0.080
Open Water	0.022
Grassland and Pastures	0.040
Creeks	0.035
Roads, Concrete Surfaces	0.020
Development Lots	0.050





## Results

#### **Critical Duration**

To determine the critical storm duration for the subject site and vicinity the guidance provided in the latest ARR 2019 guidelines was considered as summarised below:

- Classification of the median value of the ten temporal patterns (TP) for each storm duration.
- Selection of the duration that produces the maximum median value for each return interval.

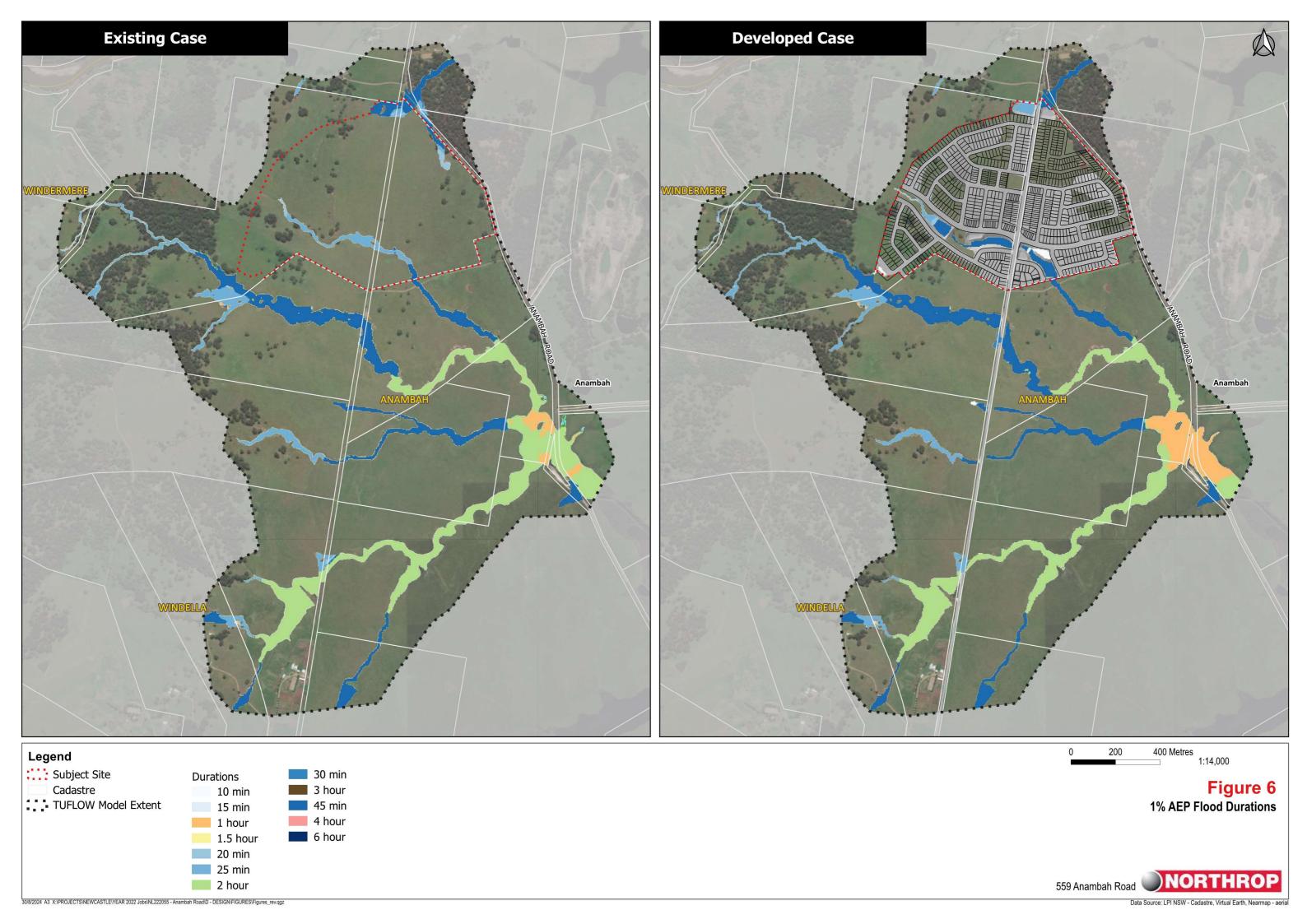
The flood elevation results were used in this investigation to define the maximum median value.

All ten rainfall patterns for the 10, 15, 20, 25, 30, 45, 60-minute and 1.5, 2, 3, 4.5, and 6-hour durations were entered into the two-dimensional model to determine the critical storm duration for the 10%, 5%, 1% and 1 in 500 AEP flood events local catchment flooding. Similarly, the 15, 30, 45, 60-minute and 1.5, 2, 2.5, 3, 4, 5 and 6-hour durations were used to determine the critical duration for the PMF event.

The below **Table 9** presents the critical durations and rainfall temporal patterns modelled during the existing and developed case scenarios for 10%, 5%, 1%, 1 in 500 AEP and PMF design flood events. 1% AEP critical duration maps for both existing and developed cases are presented in **Figure 6** overleaf.

**Table 9 - Critical Durations and Patterns** 

Event	10% AEP	5% AEP	1% AEP	1 in 500 AEP	PMF
1	1hr TP3	20min TP2	10m TP7	10m TP7	15m
2	1hr TP6	1hr TP3	20m TP4	20m TP4	30m
3	1hr TP7	1hr TP6	25m TP1	25m TP1	45m
4	1.5hr TP4	1hr TP7	25m TP5	25m TP5	-
5	1.5hr TP6	1.5hr TP6	25m TP6	25m TP6	-
6	2hr TP1	1.5hr TP7	25m TP7	25m TP7	-
7	2hr TP7	2hr TP5	45m TP6	45m TP6	-
8	-	2hr TP7	45m TP8	2hr TP10	-
9	-	-	2hr TP4	-	-
10	-	-	2hr TP10	-	-





#### Flood Behaviour

## Flood Depth, Elevation, Velocity and Hydraulic Hazard

Maximum modelled flood depth/elevations, velocity and hazard for the 10%, 5%, 1%, 1 in 500 AEP and PMF local catchment flood events for the existing and developed case scenarios are presented in **Figures BC1-1** to **BC6-3** of **Appendix A**.

Similarly, the 1% AEP flood depth/elevation, velocity and hazard for the Stage 1 of the development are presented in **Figures BC5-1** to **BC5-3** of **Appendix A**.

Flood hazard conditions have been assessed based on the latest ARR 2019 guidelines and Australian Institute of Disaster Resilience (AIDR) hazard categories presented in **Figure 7** below.

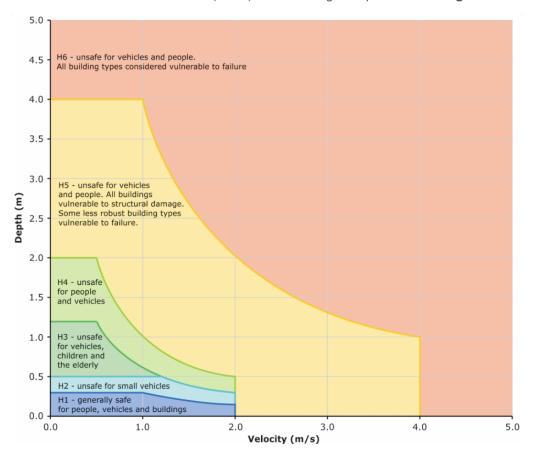


Figure 7 - Australian Rainfall and Runoff (2019) Hazard Categories



#### **Peak Flows**

Modelled local catchment peak flows for the 10%, 5%, 1%, 1 in 500 AEP and PMF local catchment flood events for the existing and developed case scenarios at the flow reporting locations (refer to **Figure 4**) are presented in **Table 10** below.

Table 10 - Peak Flows at Reporting Locations

Location Reference	Location Description	Flood Event (AEP)	Existing Case (m³/s)	Developed Case (m³/s)	Difference (m³/s)	Difference (%)
	200m D/S of Anambah Road South	10%	24.96	25.06	0.10	0.4
		5%	38.91	38.93	0.02	0.1
1		1%	87.92	87.08	-0.84	-1.0
	Crossing	1 in 500	117.8	111.6	-6.20	-5.3
		PMF	658.6	656.3	-2.30	-0.3
		10%	8.83	8.88	0.05	0.6
	130m D/S of	5%	9.27	9.36	0.09	1.0
2	South-West Basin Outlet	1%	22.62	22.46	-0.16	-0.7
		1 in 500	27.60	27.89	0.29	1.1
		PMF	129.0	129.5	0.50	0.4
	D/S of Central Corridor Basins Outlet	10%	7.02	4.36	-2.66	-37.9
		5%	9.00	6.32	-2.68	-29.8
3		1%	15.92	11.12	-4.80	-30.2
		1 in 500	20.71	15.03	-5.68	-27.4
		PMF	84.83	76.22	-8.61	-10.1
	20m D/S of Anambah Road North Crossing	10%	3.60	2.22	-1.38	-38.3
4		5%	4.19	2.58	-1.61	-38.4
		1%	8.44	4.21	-4.23	-50.1
		1 in 500	11.70	8.14	-3.56	-30.4
		PMF	51.11	46.67	-4.44	-8.7

The results in the **Table 10** show that the proposed stormwater detention infrastructure attenuates peak flows from the development generally for all modelled events. A few peak flow increases observed in locations 1 and 2 are typically less than one percent and minor in magnitude. These are discussed further in the Discussion section of this report.

## **Flood Immunity**

Developed case modelling indicates the proposed River Road has 1% AEP local catchment flood immunity and trafficable for up to including 1 in 500 AEP local event (H1 flood hazard observed across the road surface during 1 in 500 AEP event at the proposed culvert R01B).



Modelling also indicates that Anambah Road at the south Anambah Road culvert crossing has 10% AEP local catchment flood immunity and trafficable for up to 5% AEP local event including small vehicles (H1 flood hazard). Similarly, Anambah Road at the northern culvert crossing is flood free during 10% AEP event and generally safe for all vehicles for up to 5% AEP event (H1 flood hazard).

#### **Flood Level Effects**

**Figures D1** to **D6** of **Appendix B** present the flood impact to flood level for the modelled 10%, 5%, 1%, 1 in 500 AEP and PMF flood events. The 1% AEP flood impact for the Stage 1 of the development presented in **Figure D5** of **Appendix B**.

The results presented in **Figures D1 to D6 of Appendix B** typically shows a reduction in flood levels is expected to occur during all modelled events downstream of the proposed development.

During the 10% AEP event, a localised increase of up to 12mm is observed upstream of the southern Anambah Road culvert crossing. This increase is minor in extent and magnitude as there is no change in the existing flood hazard conditions and flow velocity regime. This is not expected to create a significant adverse impact in this location.

Similarly, during the 1 in 500 AEP event, an increase of up to 170mm is observed upstream of the proposed River Road culvert R01 (refer to **Figure 4** for location). This increase is expected due to the road fill across the existing watercourse and considered not to create significant adverse impact as the increase is localised within the watercourse channel and not changing the existing flood hazard conditions.

During the PMF event, **Figure D6** of **Appendix B** shows an increase of up to approximately 80mm, 450mm and 550mm are observed in watercourses upstream of the existing Anambah Road northern crossing, and upstream of the proposed River Road crossings R01 and R03, respectively. As the PMF design storm event has an extremely rare chance of occurring, it is not typically used to guide development and generally, the greatest concern during an event of this nature is whether a change in the risk to life occurs as a result of the development.

Review of **Figure BC6-3** of **Appendix A** shows no significant changes in flood hazard conditions observed during the PMF. H5 and H6 flood hazard conditions are already observed across the watercourses under the existing conditions, as such, no increase in the risk to life and, therefore, a significant adverse impact are expected during the PMF local flood event developed conditions.

Based on the above, the proposed development is not expected to create a significant adverse impact on the subject site, in adjacent properties or downstream areas.



## Discussion

## **Suitability of Flood Level Impacts**

As discussed above, where there is an increase greater than 10mm, a merit-based assessment has been carried out to determine whether the increase is likely to cause a significant adverse impact.

Through consideration of the magnitude of the increase, likelihood of the event, the existing development in the area of increase, and hazard category changes in the area of increase, we do not believe the flood level increases determined cause a significant adverse impact.

## **Consideration of Changes in Flood Behaviour**

Consideration of other flood characteristics and the likely changes resulting from the development is presented below in Table 11.

Table 11 - Consideration of Impacts on Flood Behaviour

Characteristic	Commentary	Assessment of Significance
Flood Level Changes	The development is generally located outside the Hunter River floodplain. No changes in flood levels in this event are expected.	Minor
riood Level Changes	As discussed above, minor localised changes in flood level have been determined. We do not believe this results in a significant adverse impact.	WIITO
	The development is generally located outside the Hunter River floodplain. No velocity changes in this event are expected.	N
Velocity Changes	Peak flow differences have been determined as generally a reduction or small increases less than two percent. We believe this will result in a commensurate reduction, or no significant change in flood velocities.	Not significant
Flood Function	The development is generally located outside the Hunter River floodplain. No changes to flood function in this event are expected.	Not
Flood Function Changes	Local drainage gullies have been maintained in the riparian corridor design for the development. We believe the flood function of these gullies will be maintained on this basis.	significant
Hazard Categorisation	The development is generally located outside the Hunter River floodplain. No changes to flood hazard are expected in this event.	Not significant
Changes	No significant changes to local flood hazard are expected as a result of the proposed development.	Signilicant
Change in Flooding Duration	The development is generally located outside the Hunter River floodplain. No change in flood duration is expected for this event.  The local catchment has a duration of concentration for	Not significant
	flood levels of events two hours or less. We note some	



Characteristic	Commentary	Assessment of Significance
	increases in the rising and falling limbs of the hydrographs may occur due to the increase in impervious fraction, and the presence of detention and this is not expected to be a significant increase.	
Change in Frequency of Inundation	New lots are to be constructed above the Flood Planning Level and not inundated in this event. Since not changes are proposed to the Hunter River floodplain no change to the frequency of inundation of Anambah Road in this event is expected.	Not significant
	The development is generally located outside the Hunter River floodplain. There will be no changes to warning or evacuation time in this event.	
Change in Warning and Evacuation Time	For the local catchment the warning time will be short due to the critical durations for flood levels. Flood free land in the local PMF will be available within the development footprint and the duration of isolation in this event is expected to follow the duration of rainfall.	Not significant

## Alignment to Existing Floodplain Risk Management Study

Consideration with compliance with the Hunter River Floodplain Risk Management Study and Plan (MRFRMSP, 2015) has been assessed in the below Table 12.

This plan considers three broad categories for floodplain risk management including the following.

- Flood modification measures.
- · Property modification measures.
- Response modification measures.

Table 12 - Alignment to HRFRMSP

Category	Measure	Commentary	Compliant
Flood	New Levee Banks	This is not applicable as the development is predominately located out of the Hunter River floodplain.	Not applicable
Flood	Alterations to existing levees	This is not applicable as the development does not propose any modifications to existing levees or spillways.	Not applicable
Property	Minimise risk to property	The proposal locates new lots outside the flood planning area in the developed case, designs the riparian corridor to enhance flood resilience, and adopts development controls appropriate to the proposal.	Yes
Property	House raising and flood proofing	Not applicable. This measure relates more to existing flood prone development.	Not applicable



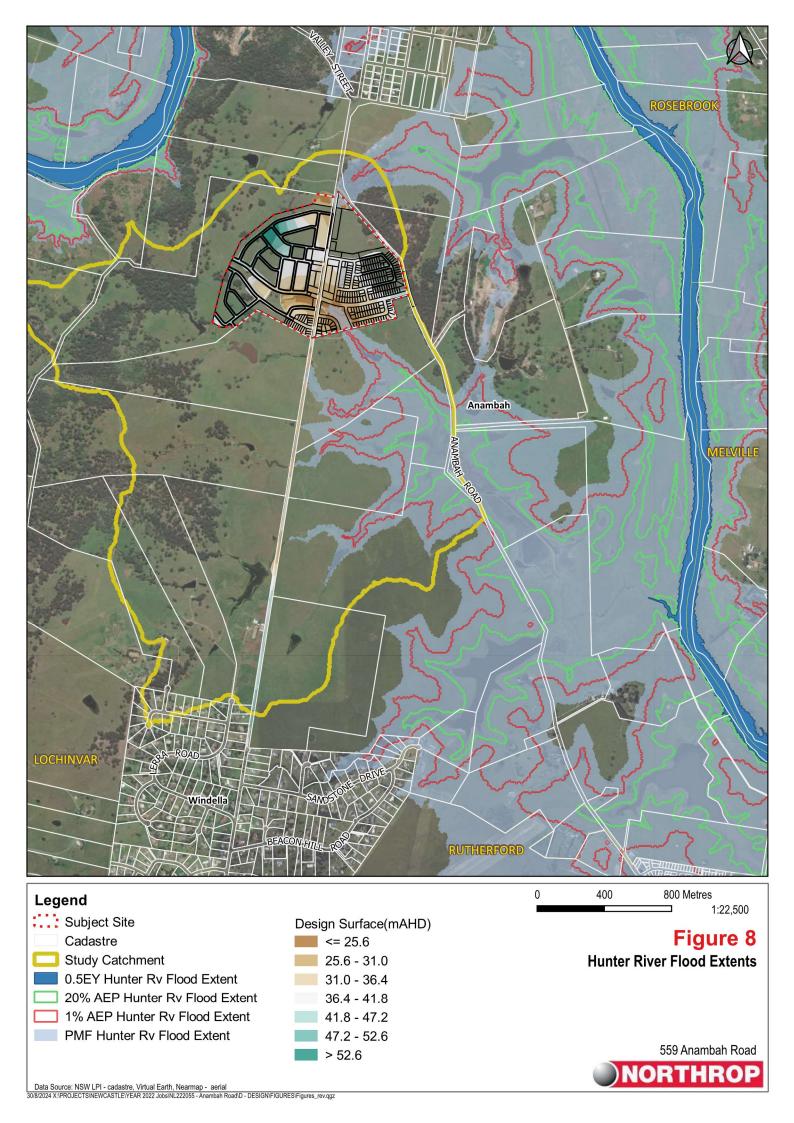
Category	Measure	Commentary	Compliant
Property	Amphibious housing	Not applicable. This is not proposed as part of the development.	Not applicable
Property	Rezoning	Not applicable. This site is already zoned for the use proposed in the development.	Not applicable
Property	Voluntary purchase	Not applicable. The development is generally located outside the Hunter River floodplain.	Not applicable
Property	Importation of fill	Redistribution of fill within the development to the creation of River Road acts to improve the flood access immunity to the development.	Yes
Response	Evacuation routes	The site maintains flood free land in the Hunter River, and local catchment PMF events. The flood access immunity for the development has been enhanced through the construction of the River Road access to be above the 1% AEP in the local catchment events.	Yes
Response	Flood warning and evacuation planning	No changes to flood warning products are expected as a result of the development. Flood free land is available on-site in the Hunter River and local PMF events.	Yes
Response	Public information and raising flood awareness	These measures relate more to broad community awareness rather than specific items related to development.	Not applicable

## **Evacuation Route**

Egress from the site is expected to be available via the proposed River Road to Windella and further to New England Highway when Anambah Road is compromised by flood waters during the major local catchment flood events or/and Hunter River flooding.

As requested by Council in the pre-DA meeting, the immunity of this access has been adopted as the 1% AEP.

A figure showing the development relative to Hunter River flood events is presented overleaf in Figure 8.





## **Risk Assessment**

An assessment of the development risks, from a floodplain risk management perspective is presented below in Table 13.

Table 13 - Risk Assessment

Risk Category	Description	Commentary on Measures to Mitigate	Mitigated
Property	Flood levels affecting new dwellings.	New lots situated above the flood planning level.	Yes
Property	Impacts on surrounding properties.	Detention and road crossing implemented to reduce peak flows from the unmitigated condition on downstream lots.	Yes
Life	Emergency access and response measures.	Provision of River Road at the 1% AEP, and flood free land located above the PMF within the development.	Yes
Environment	Velocities in riparian corridors and downstream.	Provision of riparian corridor design to minimise changes in velocity downstream.	Yes



# Compliance with Council Policies

Compliance with Council's LEP requirements are presented below in Table 14.

Table 14 – LEP requirements

Requirement	Response
5.21 Flood Planning	
(1) The objectives of this clause are as follows	
(a) to minimise the flood risk to life and property associated with the use of land,	This is noted. Discussed below.
(b) to allow development on land that is compatible with the flood function and behaviour on the land, taking into account projected changes as a result of climate change,	This is noted. Discussed below.
(c) to avoid adverse or cumulative impacts on flood behaviour and the environment,	This is noted. Discussed below.
(d) to enable the safe occupation and efficient evacuation of people in the event of a flood.	This is noted. Discussed below.
(2) Development consent must not be granted to considers to be within the flood planning area unled development	
(a) is compatible with the flood function and behaviour on the land, and	The subject site is generally located outside the Hunter River floodplain, and function of the local drainage gullies has been considered in the riparian corridor design. We believe the development is compatible with the flood function of the land.
(b) will not adversely affect flood behaviour in a way that results in detrimental increases in the potential flood affectation of other development or properties, and	Consideration has been given to changes in flood levels and behaviour. It was determined the changes in level were localized and did not affect the flood hazard. On this basis we believe the level changes are not detrimental.
(c) will not adversely affect the safe occupation and efficient evacuation of people or exceed the capacity of existing evacuation routes for the surrounding area in the event of a flood, and	The provision of River Road at the 1% AEP facilitates a higher level of access immunity for the proposed development.
(d) incorporates appropriate measures to manage risk to life in the event of a flood, and	We believe the provision of River Road is an appropriate measure to manage the risk to life in the event of a flood.
(c) will not adversely affect the environment or cause avoidable erosion, siltation, destruction of riparian vegetation or a reduction in the stability of riverbanks or watercourses.	Standard engineering responses to water quality treatment and riparian corridor design have been documented in the civil design to respond to this item.
(3) In deciding whether to grant development conconsent authority must consider the following materials	



Requirement	Response
(a) the impact of the development on projected changes to flood behaviour as a result of climate change,	The 1 in 500 AEP has been considered here as a proxy for climate change.
(b) the intended design and scale of buildings resulting from the development,	The scale of the development does not result in significant adverse impacts and on this basis we believe it is acceptable from a floodplain risk management perspective.
(c) whether the development incorporates measures to minimise the risk to life and ensure the safe evacuation of people in the event of a flood,	The development incorporates the construction of a new emergency access which is flood free in both the Hunter River and local catchment 1% AEP events to the existing Windella township.
(d) the potential to modify, relocate or remove buildings resulting from development if the surrounding area is impacted by flooding or coastal erosion.	There is potential to remove development, which we believe is unecessary due to the location of the development generally outside the Hunter River floodplain, and proximity to the coast.



## Conclusion

A Flood Impact and Risk Assessment has been prepared for the proposed development including Stage 1 of development located at 559 Anambah Road, Gosforth NSW.

It was concluded that the proposed development.

- Is not expected to create a significant adverse impact to the existing flood behaviour on the subject site, in surrounding the subject site and downstream areas.
- Includes appropriate measures to manage risk to property.
- Includes appropriate measures to manage risk to life.
- Includes appropriate measures to manage risk to the environment.

We commend our findings to Council for their review.



#### **Limitation Statement**

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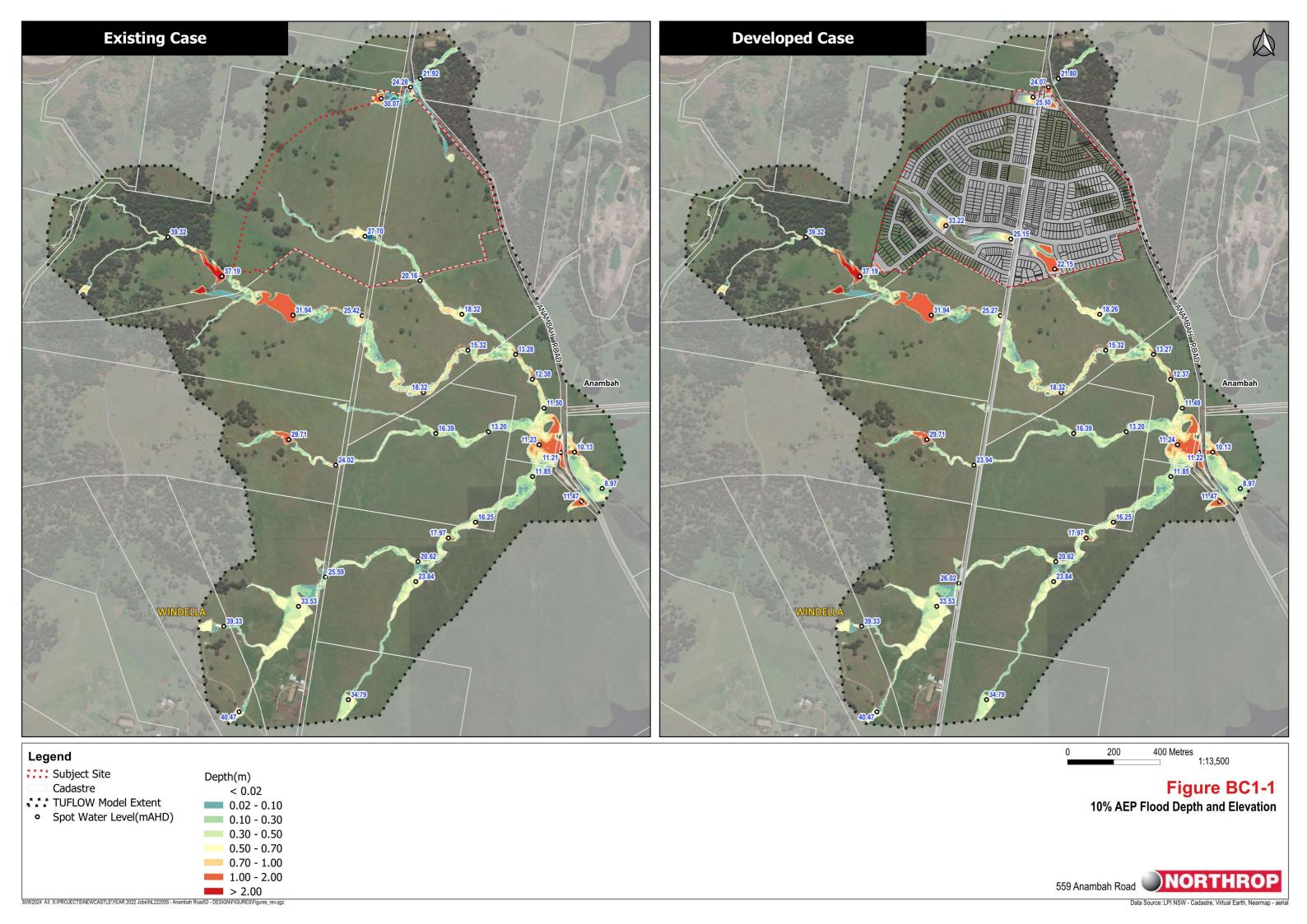
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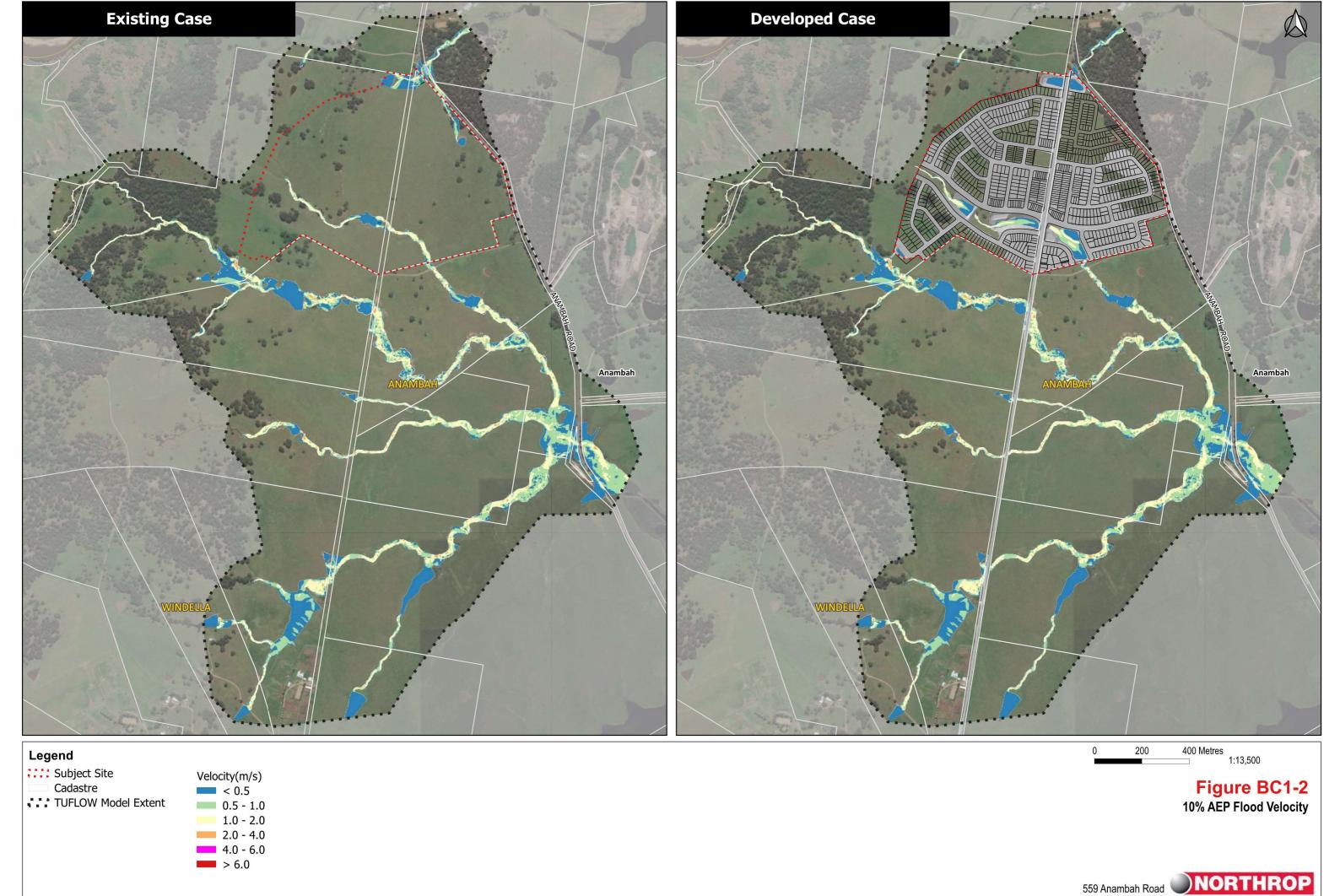
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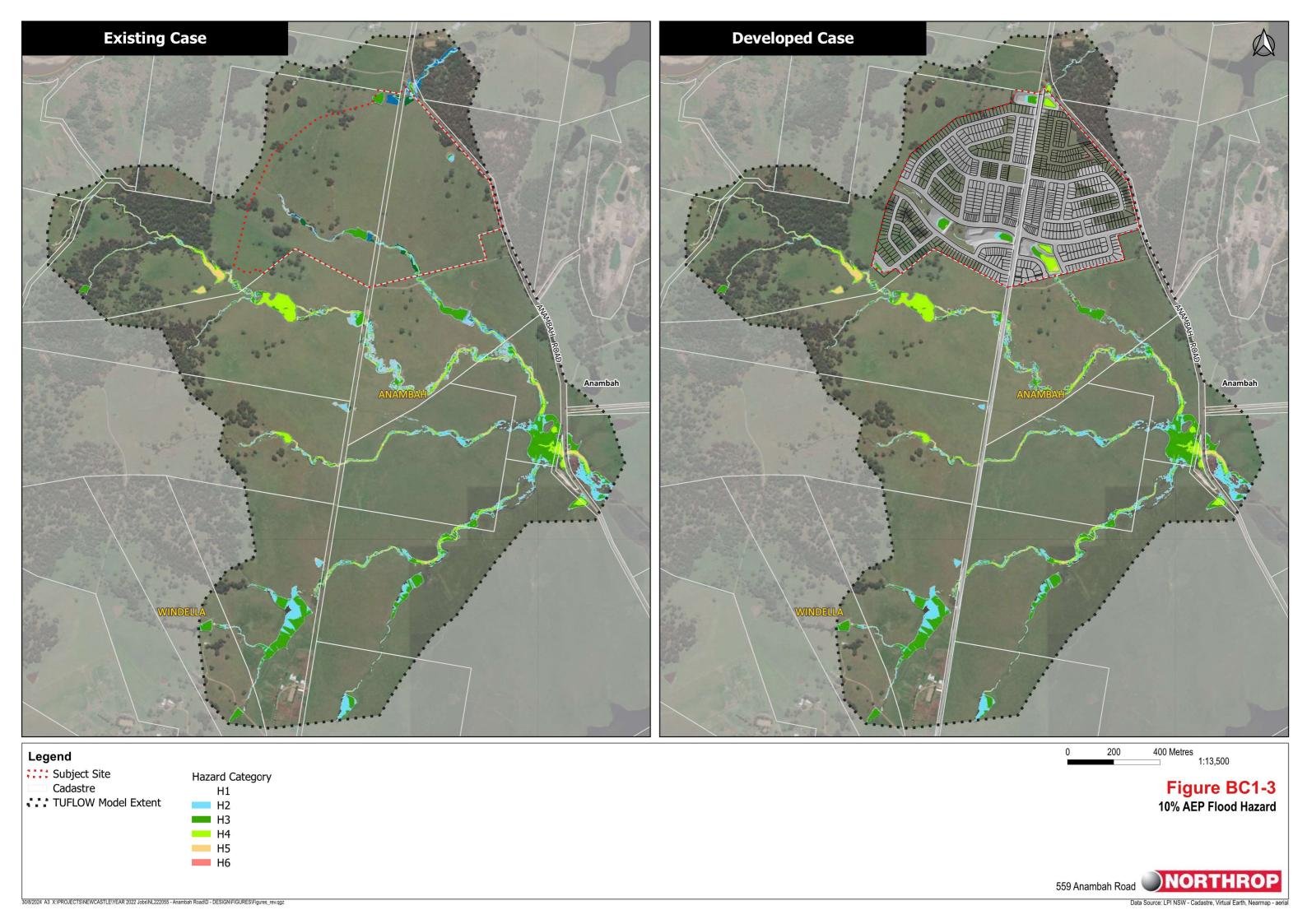
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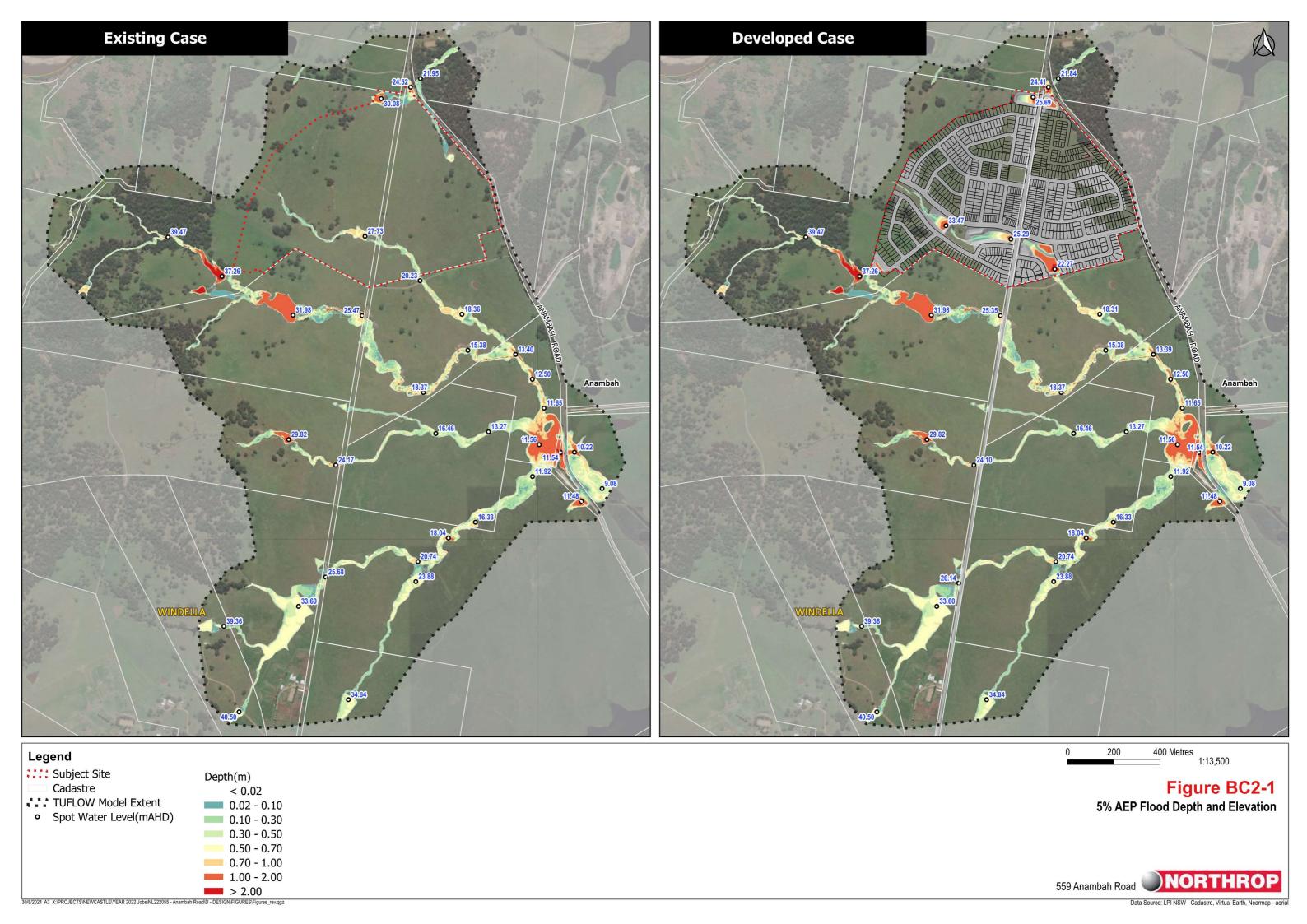


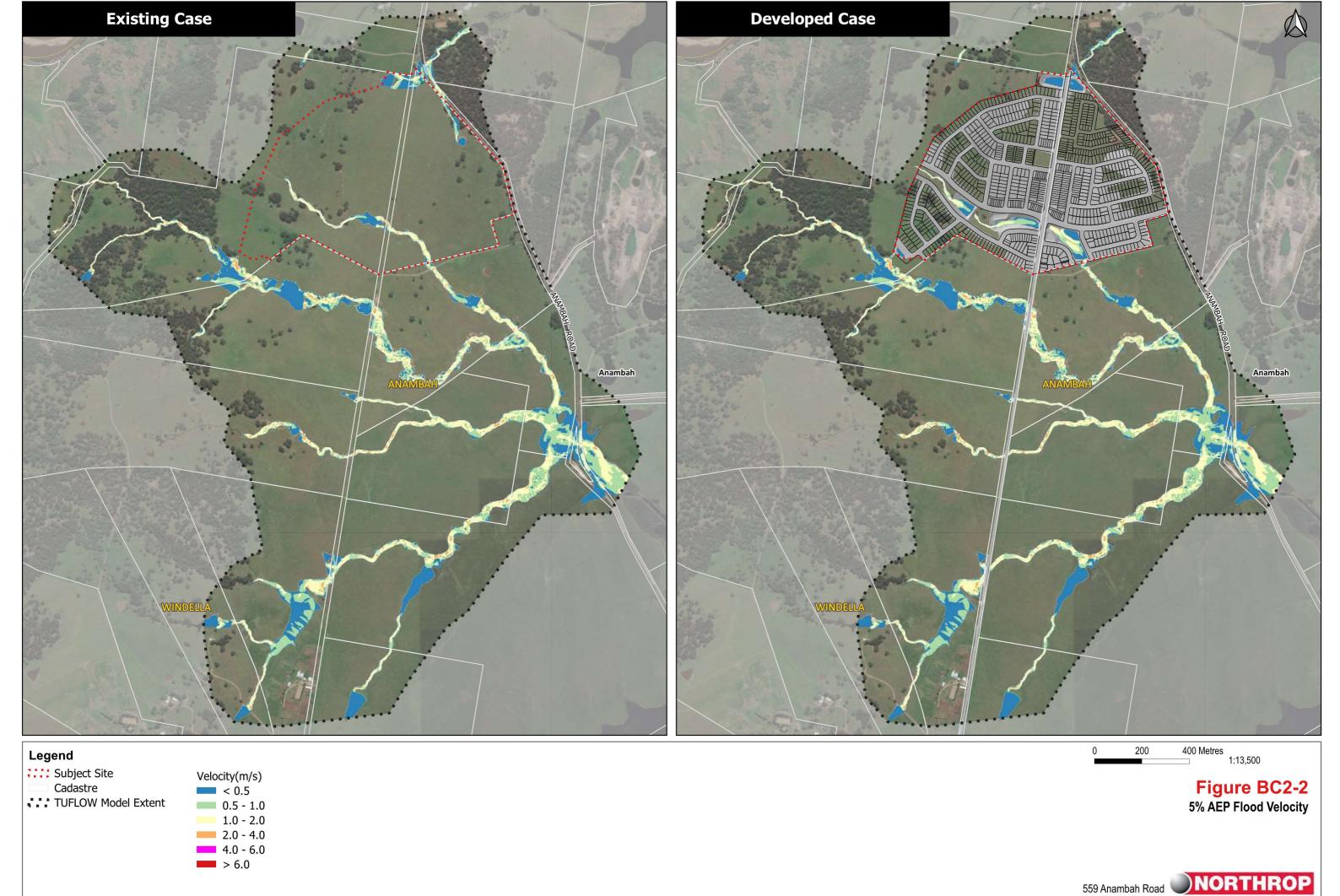
# Appendix A – Flood Figures



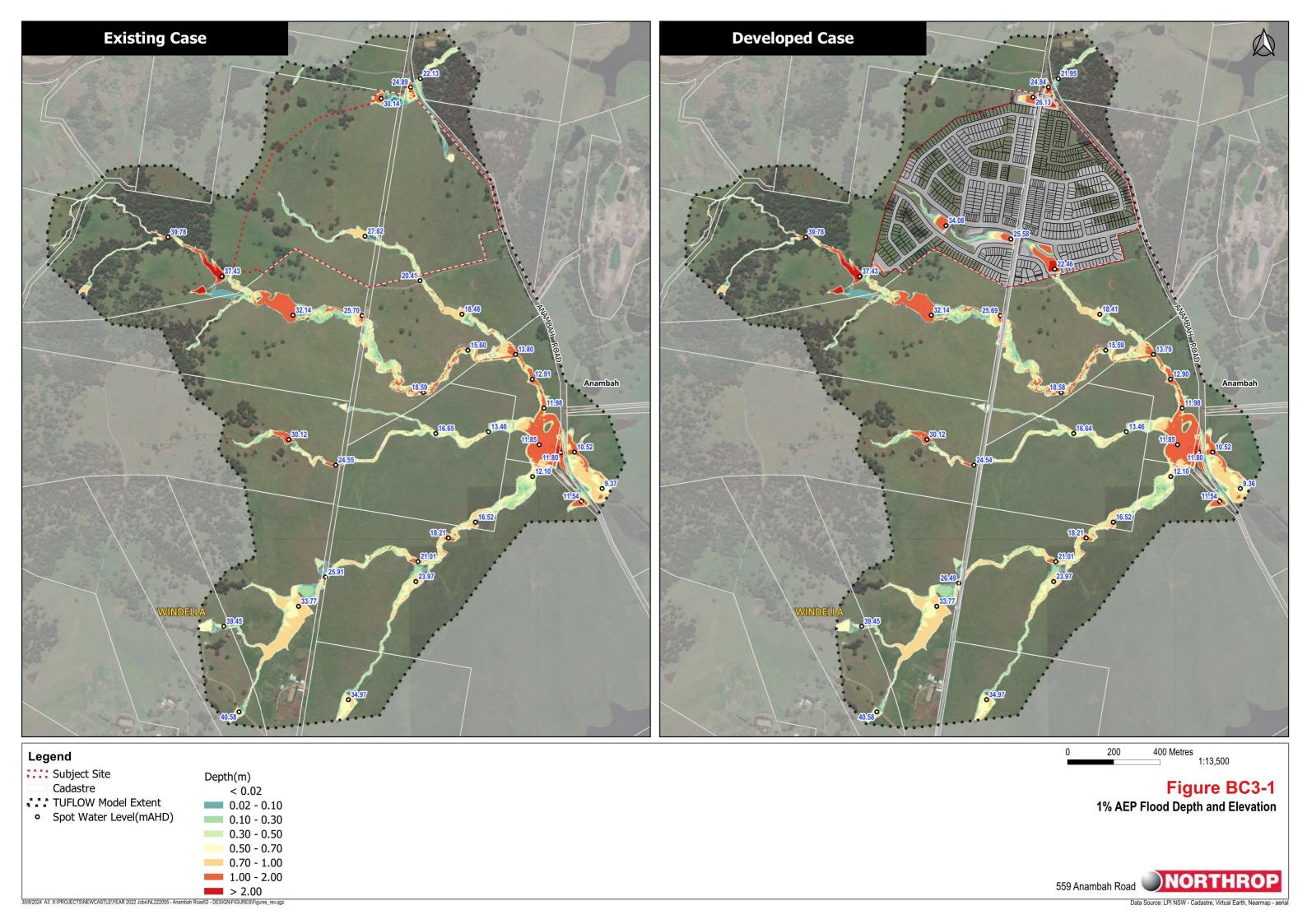


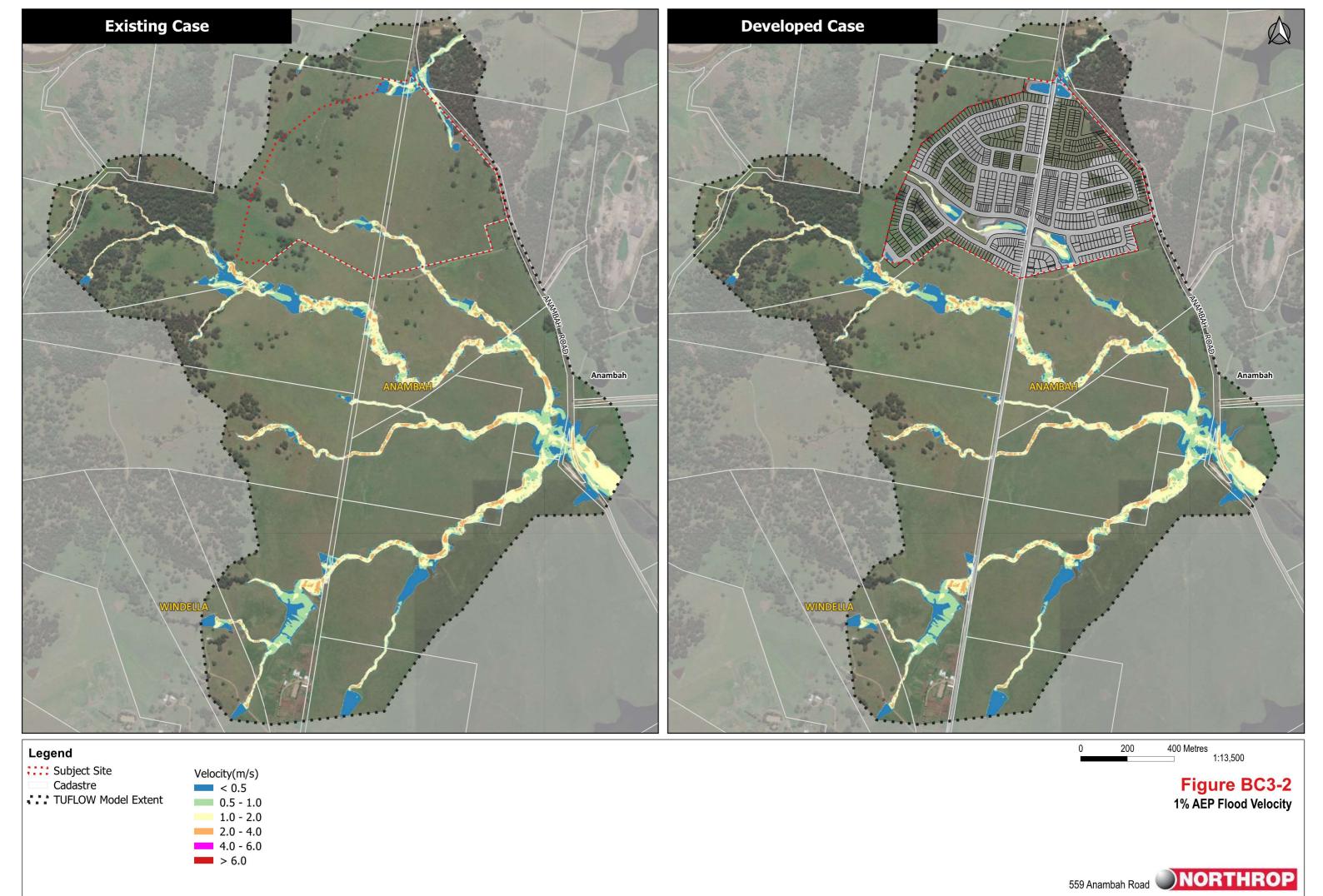


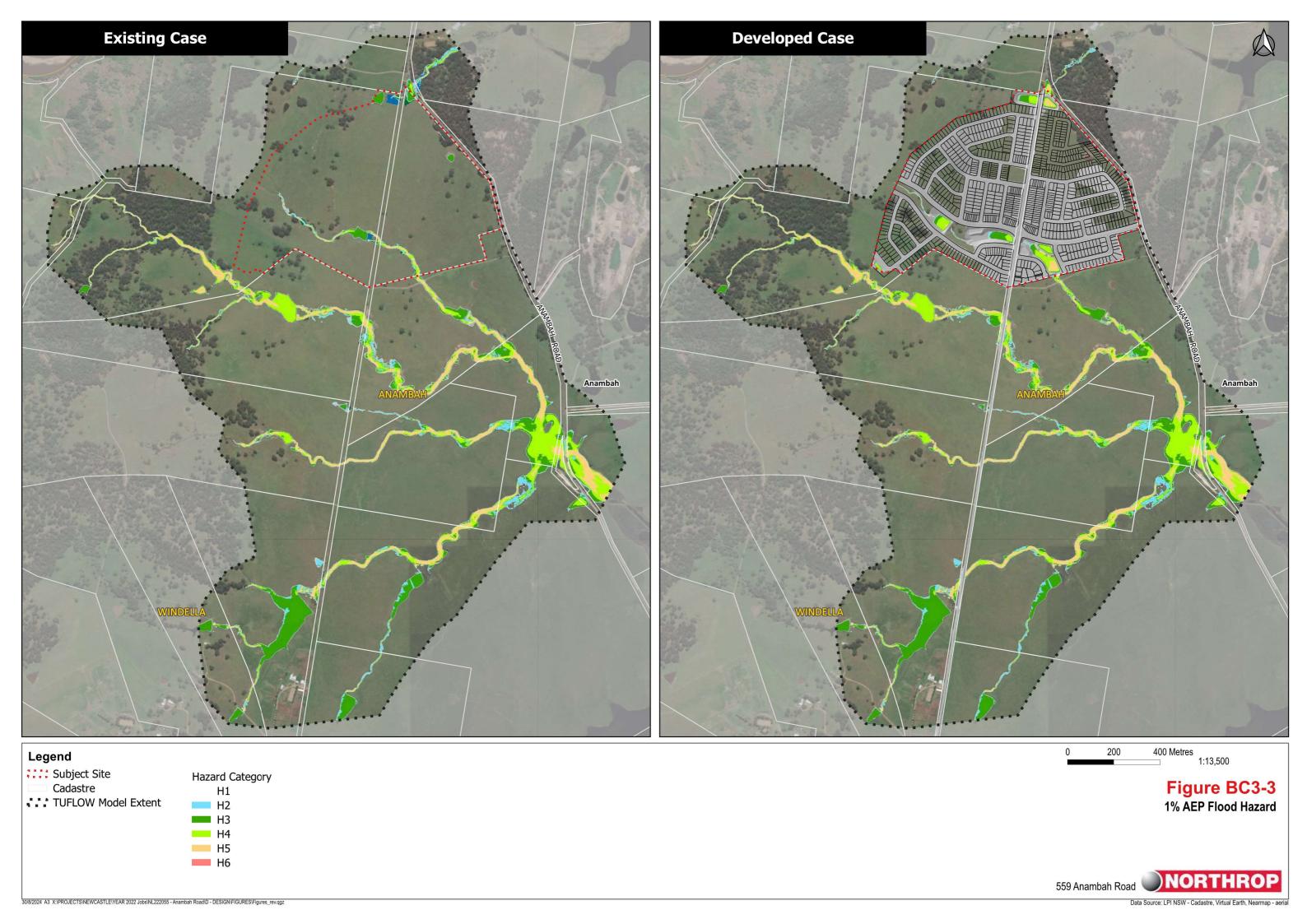


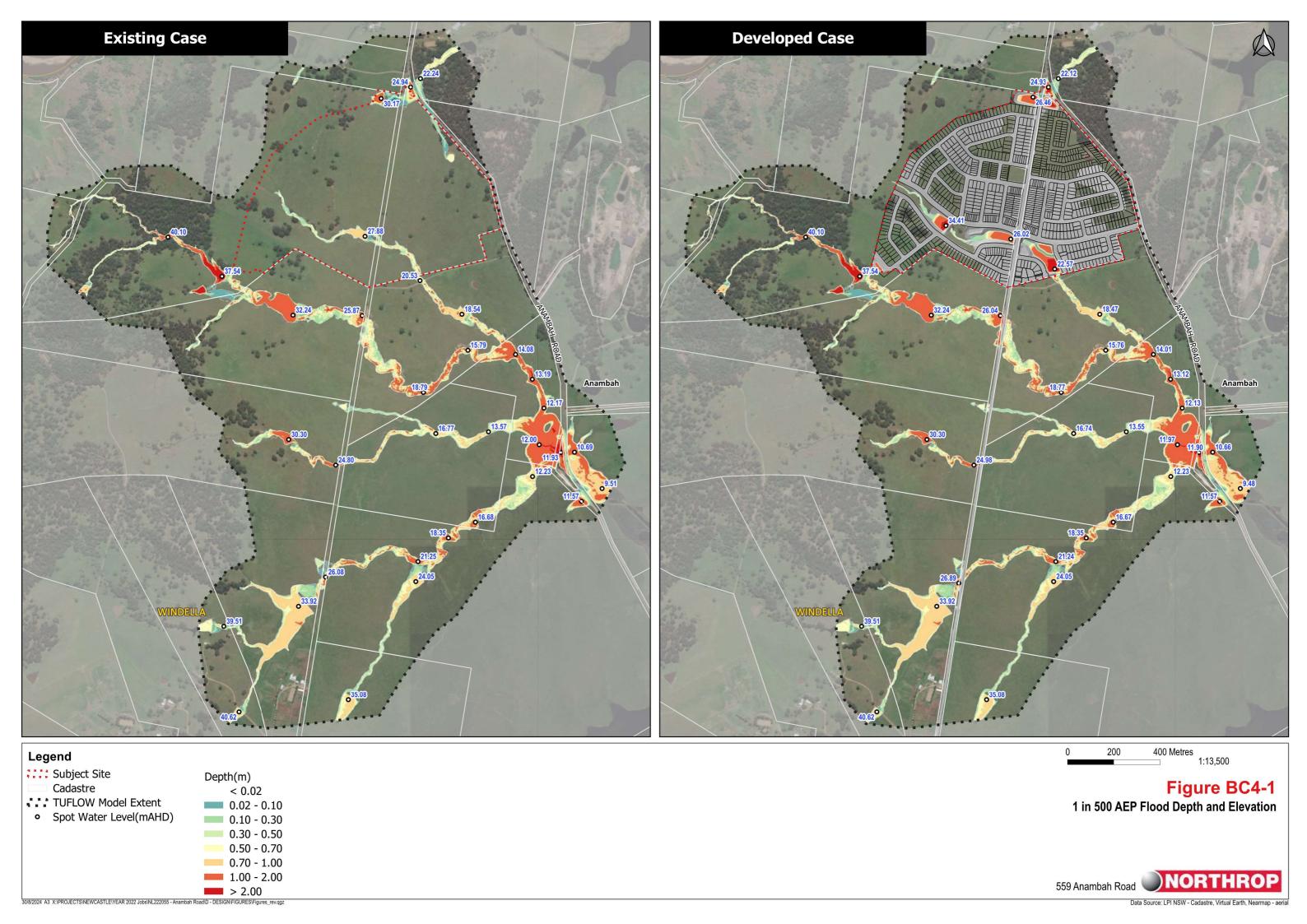


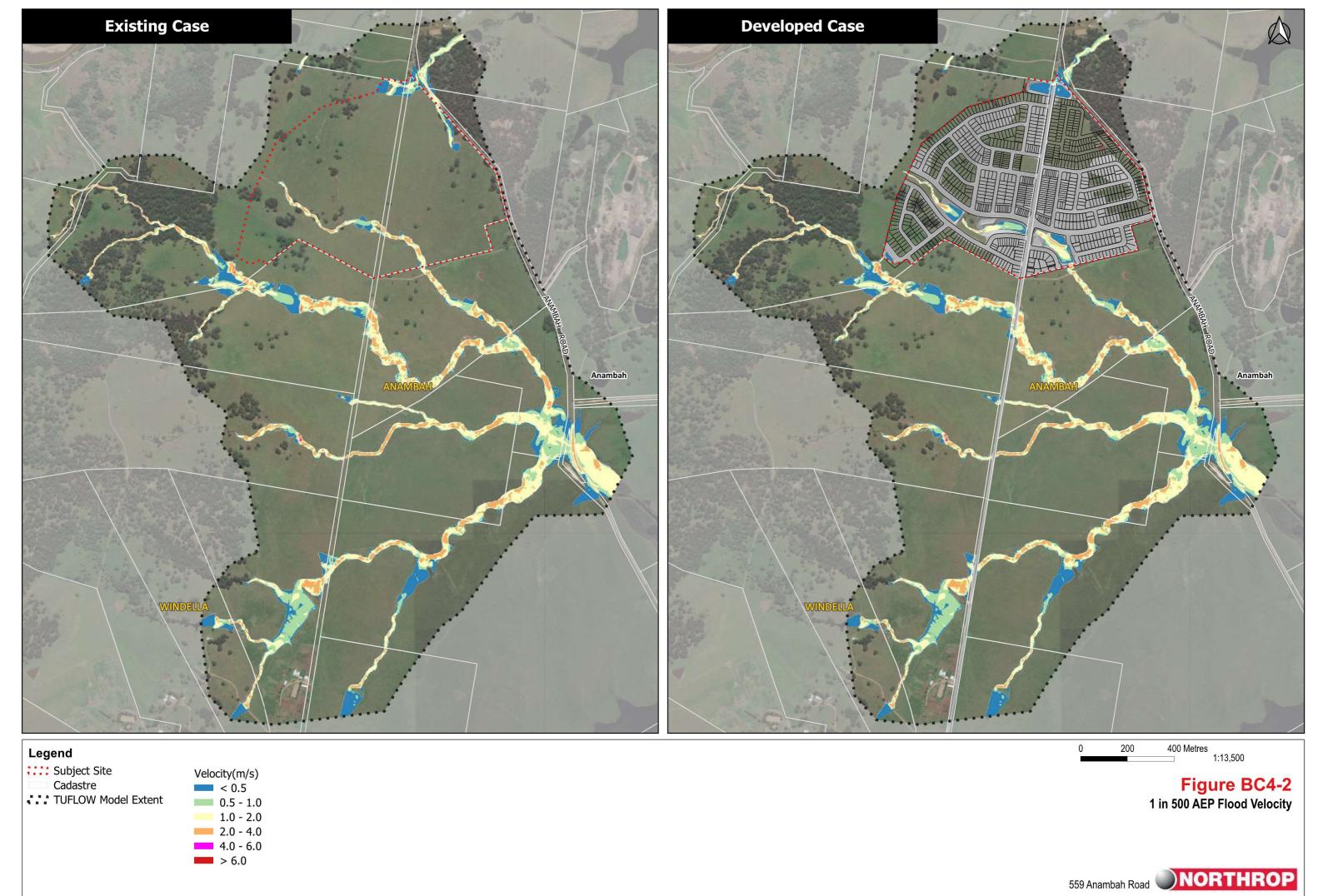


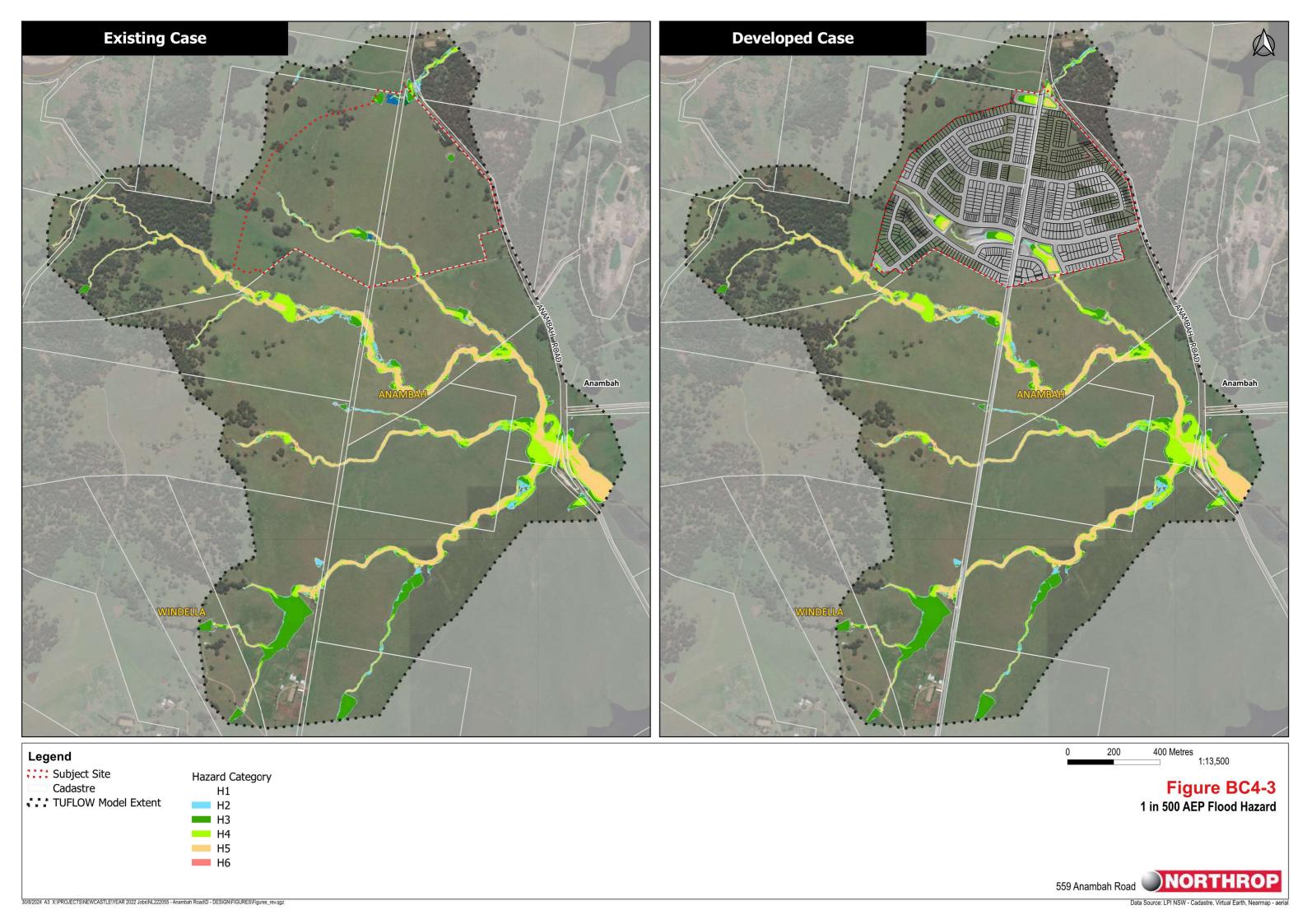


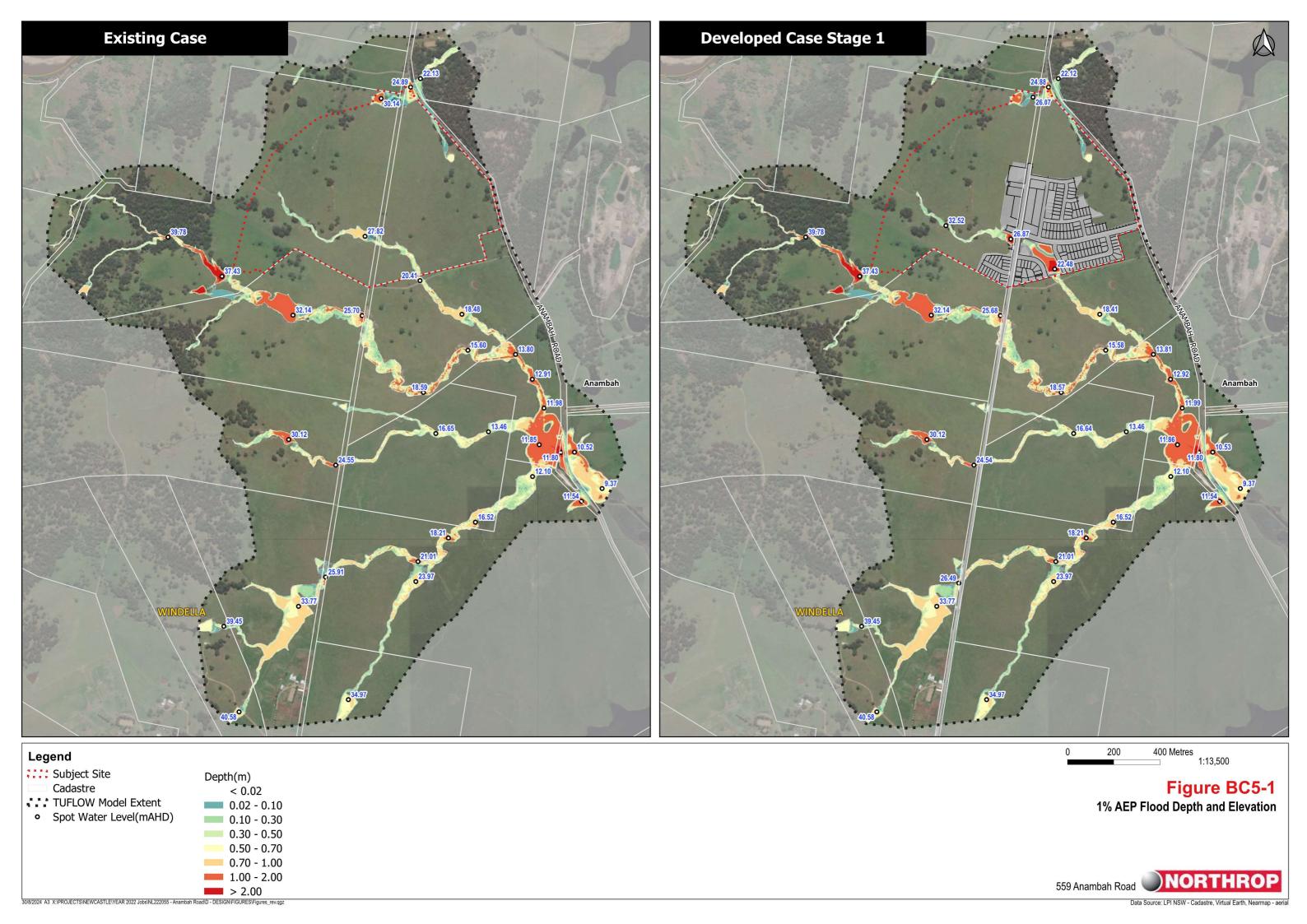


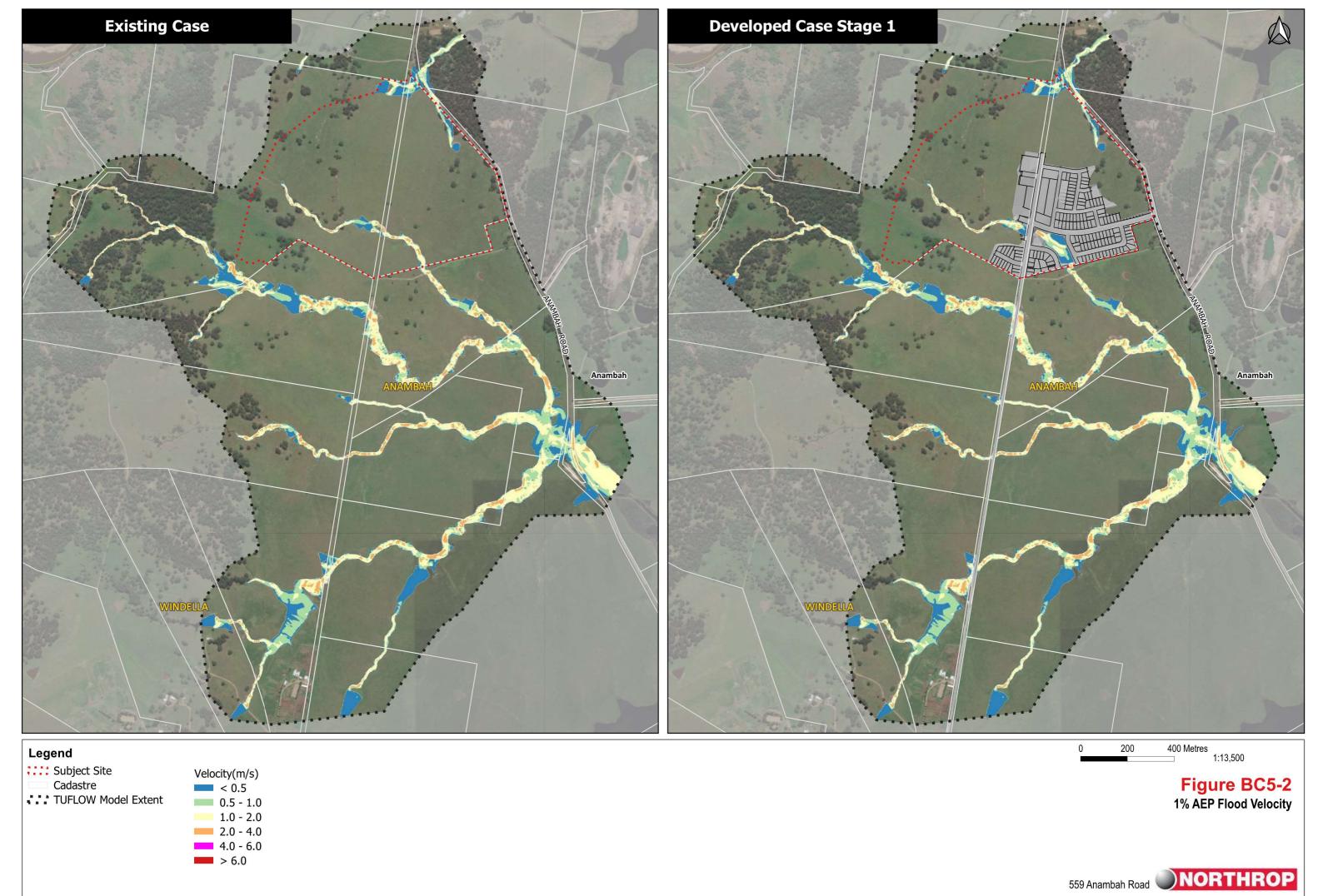




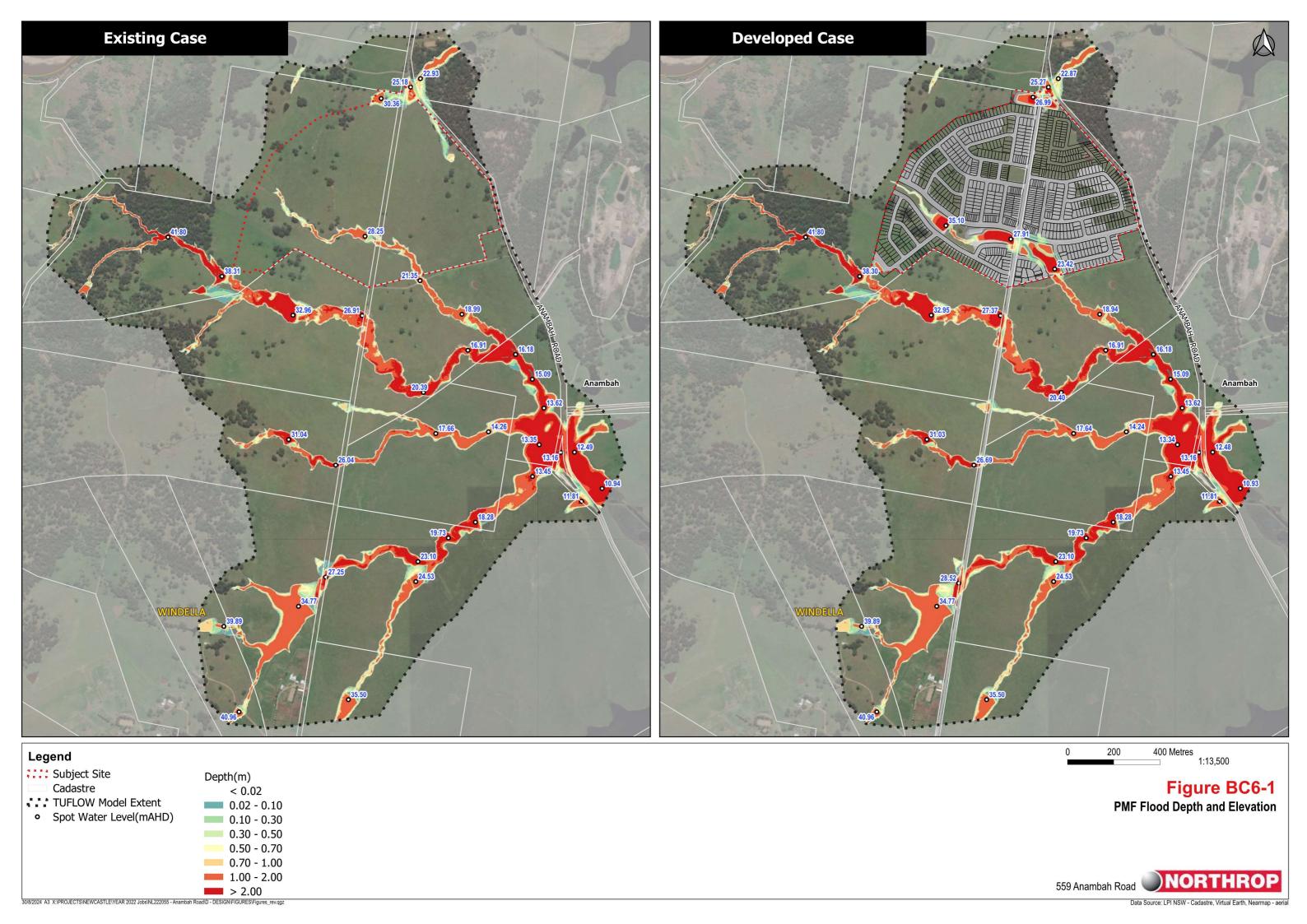


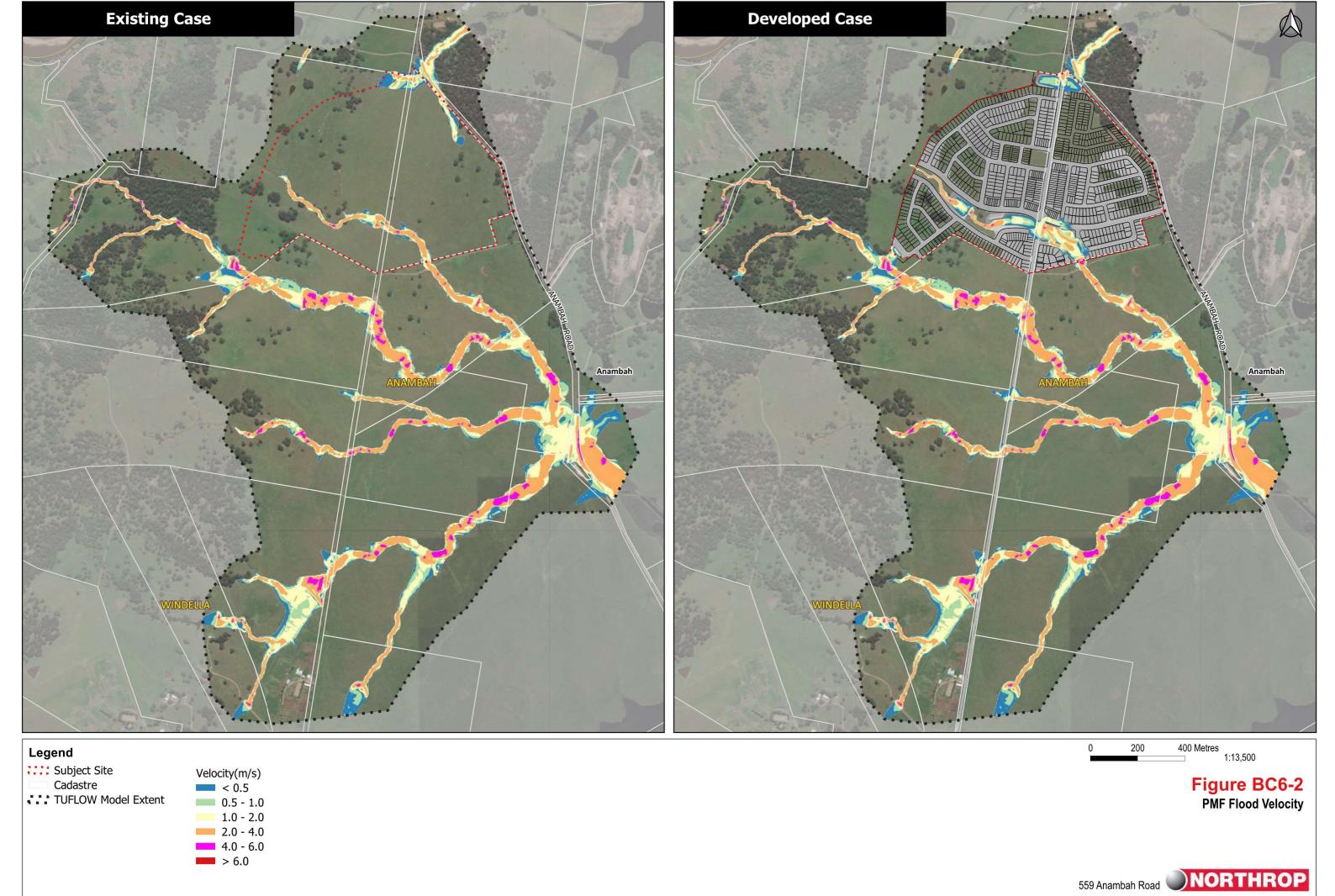


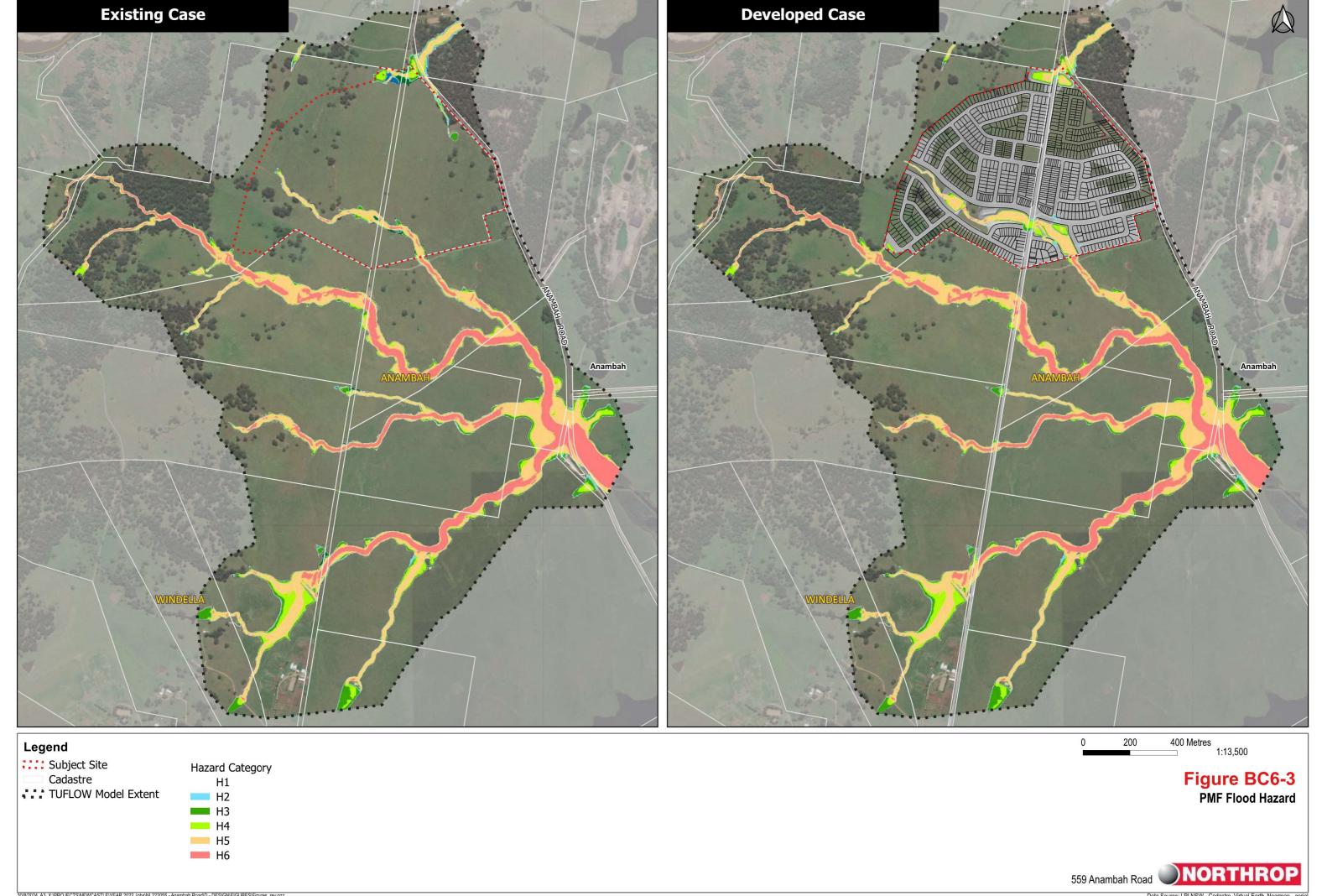






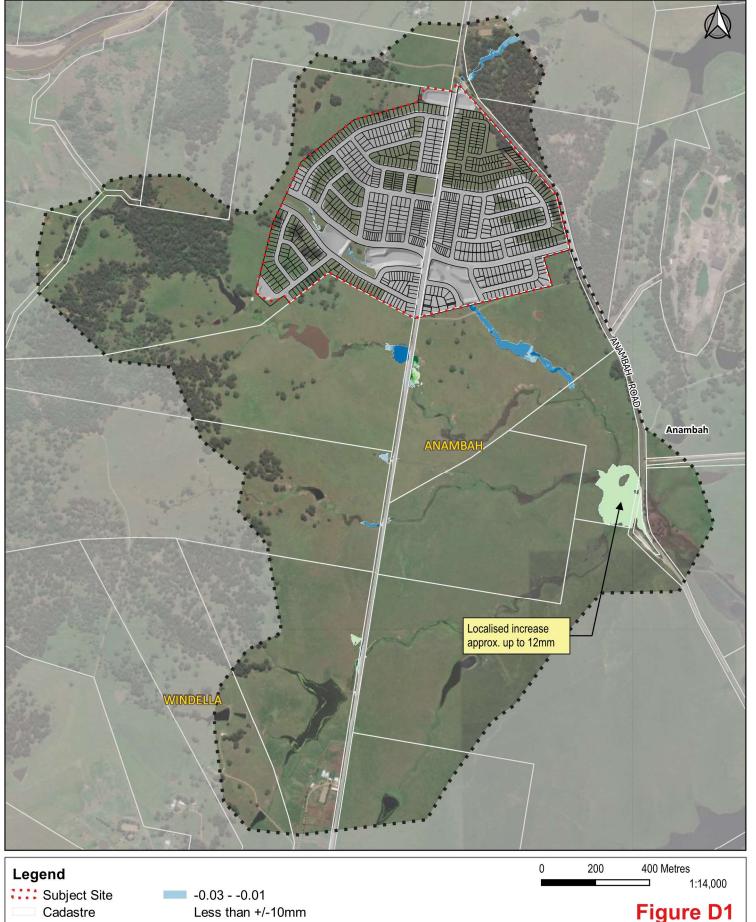


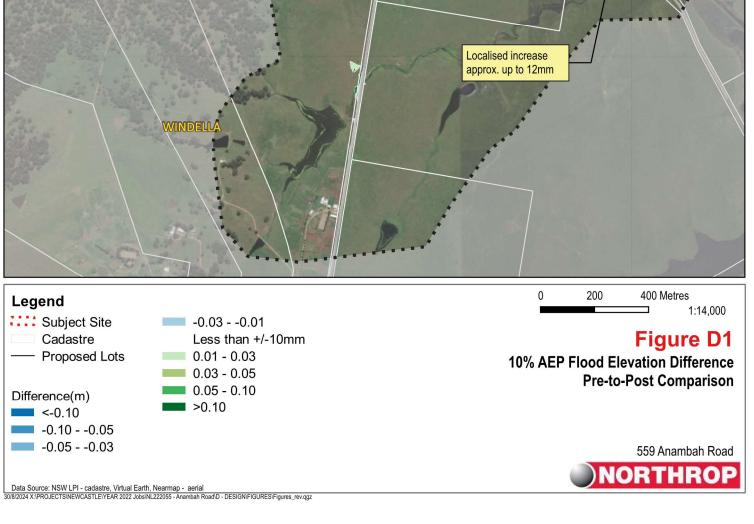




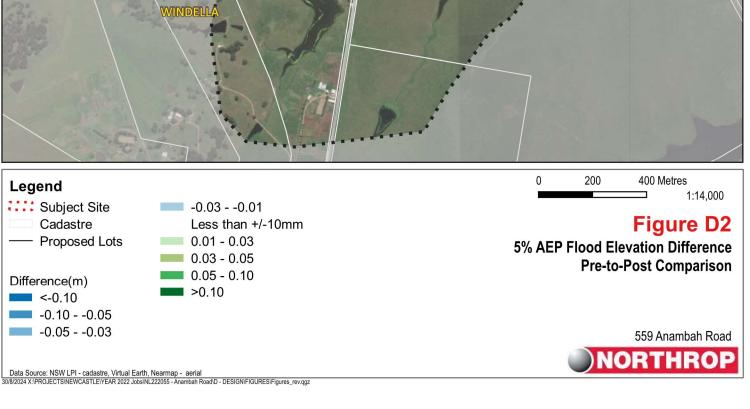


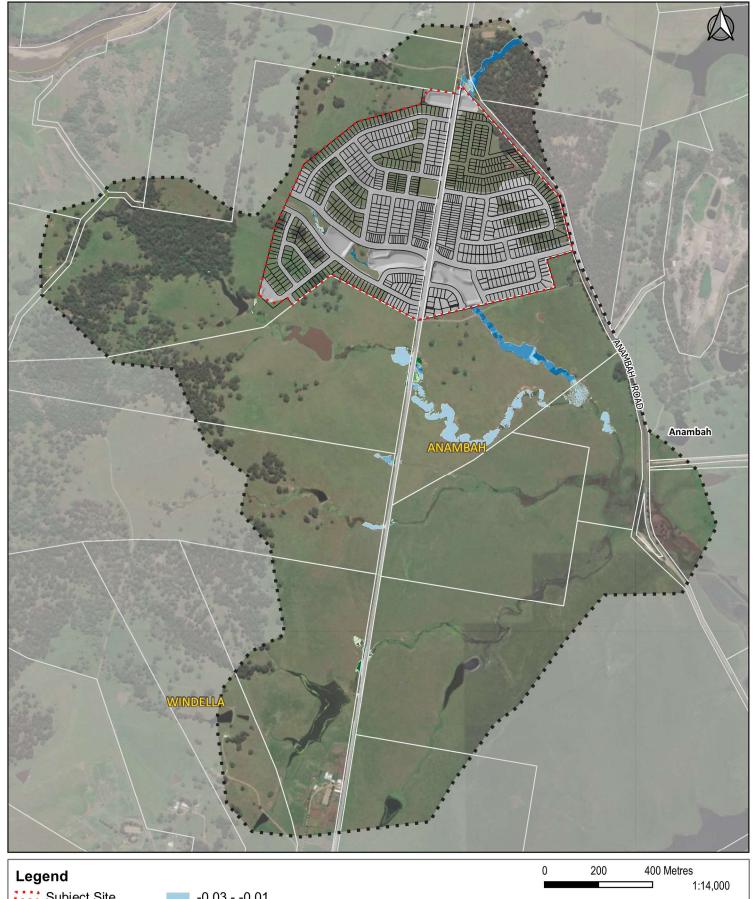
## Appendix B – Flood Impact Figures



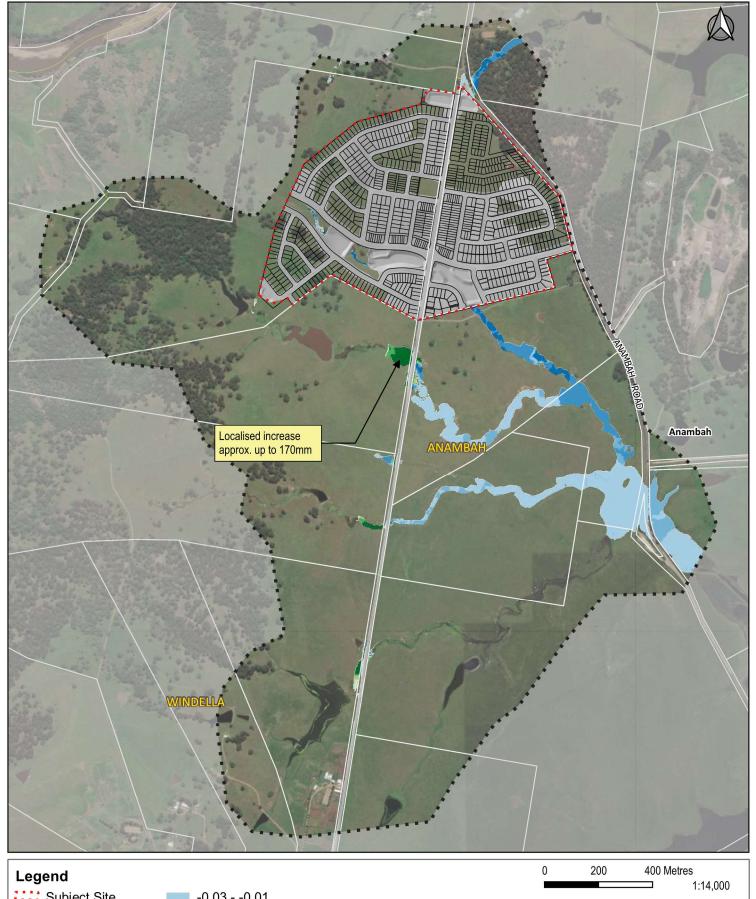


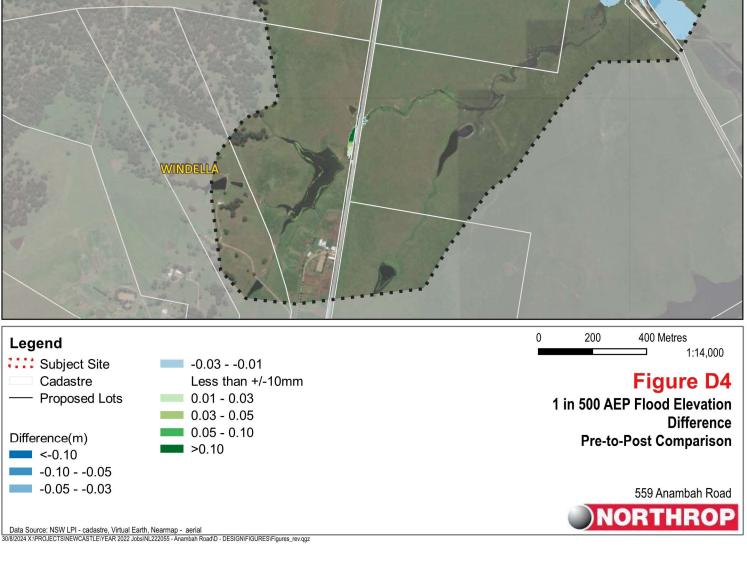


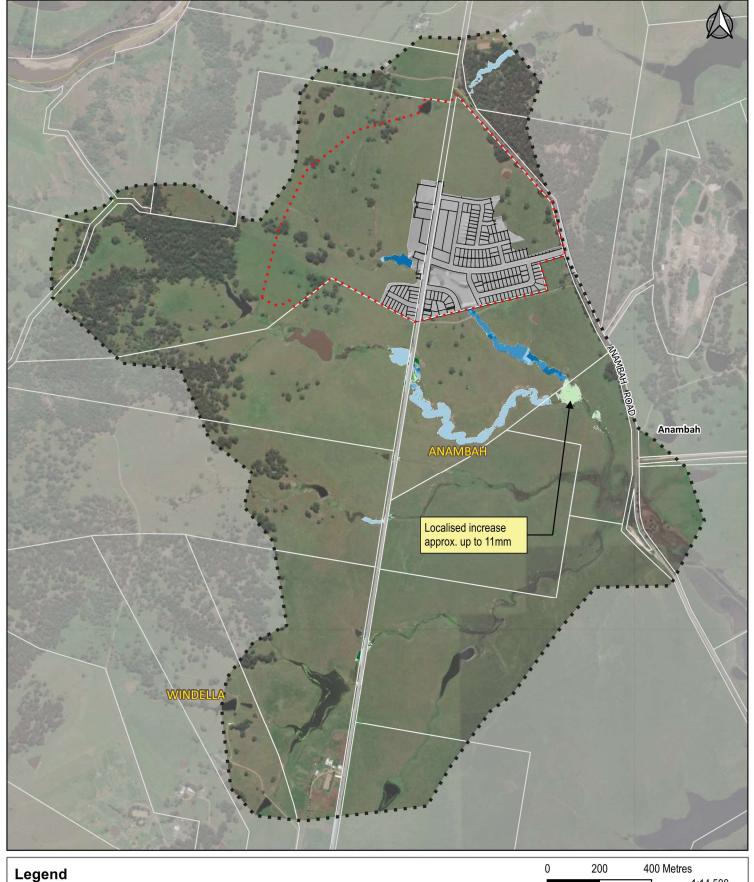


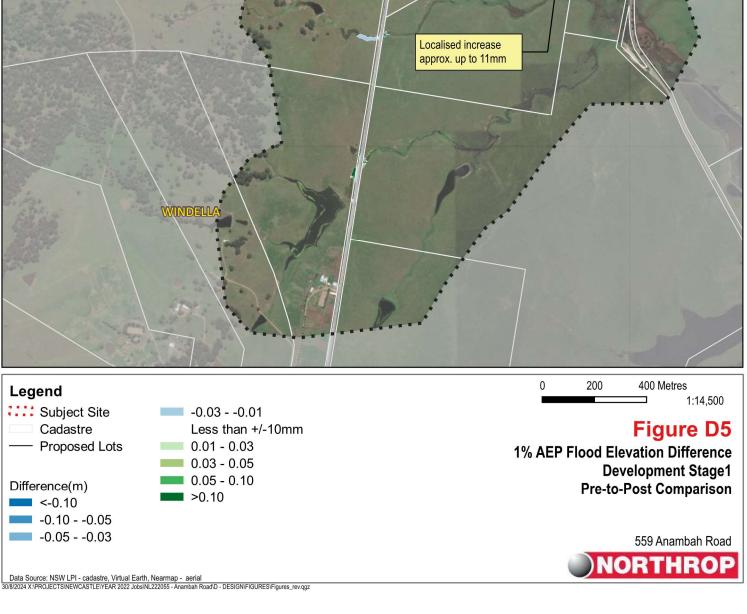


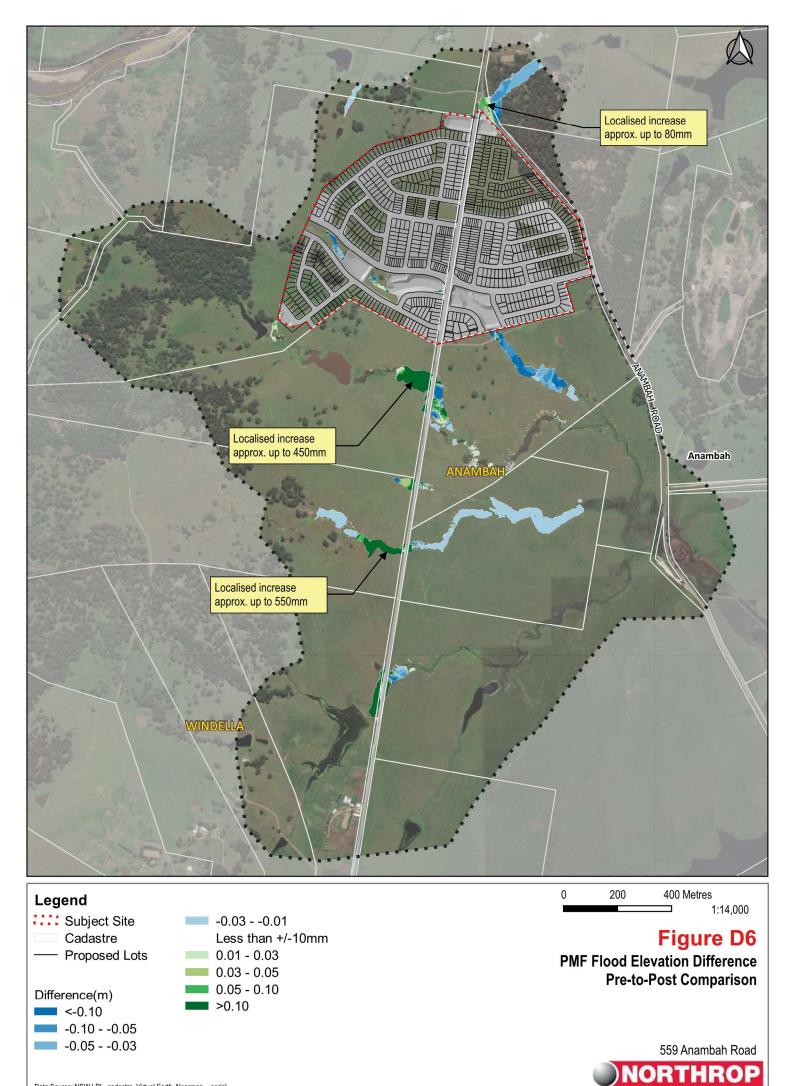












Data Source: NSW LPI - cadastre, Virtual Earth, Nearmap - aerial 30/8/2024 X:PROJECTSINEWCASTLE\YEAR 2022 JobsNL222055 - Anambah Road\(D\) - DESIGN\(F\)IGURES\(F\)Igures\_rev.qpz