

Prepared for: Thirdi Anambah Pty Ltd c/- Vara Consulting EP3627.002 29 August 2024











Geotechnical Investigation Report

559 Anambah Road, Gosforth NSW 2320

Thirdi Anambah Pty Ltd c/- Vara Consulting 53 Hume St, Crows Nest NSW 2065

29 August 2024

Our Ref: EP3627.002

LIMITATIONS

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1 Introduction

EP Risk Management Pty Ltd (EP Risk) was engaged by Thirdi Anambah Pty Ltd c/- Vara Consulting to undertake a Geotechnical Investigation at 559 Anambah Road, Gosforth NSW 2320 for the proposed approximately 900 residential lots as part of the "Anambah Urban Release Area".

The masterplan creates a new urban subdivision within the Anambah Urban Release Area accommodating a mix of housing types incorporating open space, roads, pedestrian networks, utilities and services, intersection upgrade and drainage infrastructure.

The proposed development will be undertaken in stages with Stage A comprising of approximately 240 lots that includes subdivision of the land, construction of the roads, services, bulk earth works and the dedication of reserves.

The geotechnical investigation is required for the entre master plan area included in **Appendix A** – **Masterplanning Development Application Civil Engineering Package.**

The engagement was undertaken in line with the conditions of engagement and the investigation scope as outlined in our proposal EP17828 dated 25 March 2024.

1.1 Objectives and Scope of Works

It is understood that the geotechnical investigation is required to inform the preliminary site classification, pavement design, excavatability assessment and general construction notes.

EP Risk carried out the following scope of works for the geotechnical investigation:

- Prepared all the WHS documentation and procure Before You Dig Australia plans for the site.
- Excavation of twenty-five (25) test pits to a maximum depth of 3.0m below ground level (BGL) or prior bedrock refusal within the proposed road alignments to inform the pavement design including the classified roads within the development.
- Excavation of fifteen (15) test pits to a maximum depth of 3.0m BGL or prior bedrock refusal to inform the preliminary site classification and service excavations.
- Dynamic Cone Penetrometer was conducted adjacent to the test pits to assess the consistency of the strata.
- Collection representative undisturbed, disturbed, and bulk samples for laboratory testing.
- Upon completion the test pits were filled with spoil and light compaction by excavator bucket, mounded and tracked over.
- Preparation of a geotechnical report including the investigation findings, pavement design, preliminary site classification, excavatability assessment and laboratory test results.



2 Site Location and Description

The Site is located at 559 Anambah Road, Gosforth NSW 2320, legal described as Lot 177 in DP874171 and Lot 55 in DP874170. The site is bounded by Anambah Road to the east and undeveloped land to the north, west and south.

The elevation of the site ranges from approximately 50m AHD in the north-western part of the site to approximately 20m AHD in the southern sections of the site. Rock outcrops were observed on the elevated part of the site in the north-west area.

The drainage of the site is assumed to follow the contour lines in a predominantly south and south-east direction and towards the north along natural drainage lines to lower elevated areas of the site. Part of the site drains also towards north to lower elevations. The fieldwork was undertaken following a prolonged period of rain and water ponding was observed in several areas across the site. Water dams associated with the grazing were also observed on site, constructed in natural drainage lines. The site vegetation comprised of short pasture grass used for grazing and scattered trees. Several erosion scarps were observed along the drainage lines. Photos collected during site investigation are shown in **Appendix B – Photolog**.

An excerpt from SixMaps showing the indicative location of the site is presented in Figure 1.



Figure 1. Indicative Site Location



3 Desktop Study

3.1 Regional Geology

Based on geological data sourced from NSW Government website (www.minview.geoscience.nsw.gov.au), the Site is underlain by:

- Carboniferous Aged Seaham Formation (Curs) known to contain tillite, varved siltstone, tuff, red and green zeolitic mudstone with dropstones interbedded in thick-bedded lithic sandstone and conglomerate.
- Permian Aged Lochinvar Formation (Pdal and Pdal_b) containing basalt, siltstone, sandstone.

An excerpt of the geological map is shown in Figure 2.



Figure 2. Geological Map Excerpt

3.2 Soil Landscape

NSW Department of Industry, Resources and Energy (<u>www.environment.nsw.gov.au</u>), onsite soil landscapes have been identified to comprise of Rothbury (SI5601ro).

The Rothbury soil landscape covers undulating to rolling hills with elevations ranging from 60 - 140 m. Average slopes are 6 - 10% with some to 12%. Slope lengths are 800 - 1,000 m with local relief of 60 - 80 m. Drainage lines are common throughout the area and occur at intervals of 200 - 1,000 m. As limitations or this type of soil are erosion hazard, localised waterlogging, and poor drainage.



3.3 Mine Subsidence

Reference to the Mine Subsidence District Data Source, the Site is not located within a Mine Subsidence District. The closest Mine Subsidence District Maitland West Mine Subsidence District is located more than 5km away from the site.

3.4 Acid Sulphate Soils (ASS)

The NSW Government data available on www.geo.seed.nsw.gov.au indicates the site is located within Class 5 acid sulphate soil classification. Acid sulfate soils are not typically found in Class 5 areas. Areas classified as Class 5 are located within 500 metres on adjacent class 1,2,3 or 4 land. An extract of the acid sulphate soil map is shown in Figure 3.



Figure 3. Acid Sulphate Soil Map Extract



4 Geotechnical Investigation

4.1 Investigation Methodology

The site investigation was carried out from 22 to 24 April 2024 under full time supervision of an experienced EP Risk Geotechnical Professional in accordance with AS1726-2017 Geotechnical Site Investigations and comprised the following:

- Preparation of a Safe Work Method Statement (SWMS) for all the fieldwork and procuring the site service plans rom Before You Dig Australia.
- Excavating forty (40) test pits at locations of interest within the footprint of the proposed development.
- Logging of soil/rocks encountered and collection of representative soil and rock samples to be tested by a NATA-accredited laboratory.
- Reinstatement test pits with spoil. Upon completion the soil placed in test pits was compacted by the excavator bucket and by excavator run over.

The test pits were excavated using a Kobelco Geospec 24T excavator fitted with a 600mm bucket. Ripper attachment was used to advance the test pits in medium to high strength bedrock. The locations of the test pits are presented in **Appendix C- Geotechnical Investigation Locations**.

4.2 Subsurface Profile

A project geological classification has been developed based on the results of the investigation and a summary of the units and their distribution is presented in Table 1 and Table 2. The borehole logs and accompanying explanatory notes are presented in **Appendix D – Test Pit Logs**.

Table 1.	Table 1. Observed Geotechnical Units							
Unit #	Origin	Material	Description					
Unit 1	Topsoil	Silty/Sandy CLAY	Low to medium plasticity, black, grey, dark brown, fine to medium grained sand					
Unit 2	Slopewash	Silty CLAY	Medium to high plasticity, grey					
Unit 3	Residual soil	Sandy/Silty CLAY	Medium to high plasticity, grey, brown, red, yellow, fine to coarse grained sand					
Unit 4a		MUDSTONE	Silty/Sandy CLAY, medium to high plasticity, yellow and brown					
Unit 4b	XW* Material	SANDSTONE	Sandy CLAY/ Clayey Gravelly SAND, medium to high plasticity, grey, red, brown, fine to coarse grained sand, fine to coarse grained, sub-angular to angular gravel					
XW-extrem	ely weathered.							



	Depth Below Ground Level (m BGL)								
TP - ID	Topsoil	Slopewash	Residual Soil	XW Material					
	Unit 1	Unit 2	Unit 3	Unit 4a	Unit 4b				
TP01-L	0.0-0.15	0.15-0.7	0.7-1.3	1.3-3.0*	NE				
TP02-P	0.0-0.3	NE	0.3-1.1	1.1-2.1*	NE				
TP03-L	0.0-0.18	NE	0.18-0.6	0.6-2.5*	NE				
TP04-P	0.0-0.21	NE	0.21-0.8	0.8-2.7*	NE				
TP05-P	0.0-0.14	NE	0.14-0.5	0.5-3.0*	NE				
TP06-L	0.0-0.2	NE	0.2-1.4	1.4-3.2*	NE				
TP07-P	0.0-0.2	NE	0.2-0.6	NE	0.6-3.0*				
TP08-L	0.0-0.3	NE	0.3-0.5	1.9-3.0*	0.5-1.9				
TP09-P	0.0-0.23	0.23-1.1	1.1-2.5	2.5-3.0*	NE				
TP10-P	0.0-0.17	NE	0.17-0.7	0.7-3.0*	NE				
TP11-L	0.0-0.13	NE	0.13-0.7	0.7-3.0*	NE				
TP12-P	0.0-0.15	NE	0.15-0.6	0.6-3.0*	NE				
TP13-L	0.0-0.2	0.2-0.5	0.5-0.7	0.7-3.0*	NE				
TP14-P	0.0-0.2	NE	0.3-0.7	0.7-2.8*	NE				
TP15-P	0.0-0.16	NE	0.16-0.6	0.6-3.0*	NE				
TP16-L	0.0-0.2	NE	0.2-0.6	0.6-3.0*	NE				
TP17-P	0.0-0.15	0.15-0.5	0.5-0.7	0.7-3.0*	NE				
TP18-L	0.0-0.2	0.2-0.5	0.5-0.7	0.7-3.2*	NE				
TP19-L	0.0-0.18	0.15-0.6	0.6-1.0	1.0-2.5*	NE				
TP20-P	0.0-0.21	0.21-0.7	0.7-1.0	1.0-2.4*	NE				
TP21-P	0.0-0.18	0.18-0.6	0.6-0.8	NE	0.8-3.2*				
TP22-P	0.0-0.15	0.15-0.4	0.4-0.7	0.7-3.2*	NE				
TP23-L	0.0-0.16	0.16-0.8	0.8-1.6	1.6-3.0*	NE				
TP24-P	0.0-0.16	0.16-0.9	0.9-1.1	1.1-3.2*	NE				
TP25-P	0.0-0.15	0.15-0.6	0.6-1.0	NE	1.0-3.0*				
TP26-P	0.0-0.22	NE	0.22-0.7	NE	0.7-3.0*				
TP27-L	0.0-0.12	NE	0.12-0.7	NE	0.7-1.6*				
TP28-P	0.0-0.22	NE	0.22-0.5	NE	0.5-1.3*				
TP29-P	0.0-0.12	NE	0.12-0.5	0.5-2.7*	NE				
TP30-P	0.0-0.12	NE	0.12-0.4	0.4-3.2*	NE				
TP31-L	0.0-0.13	NE	0.13-0.4	NE	0.4-3.2*				
TP32-P	0.0-0.1	NE	0.1-0.4	NE	0.4-1.2*				
ТРЗЗ-Р	0.0-0.15	NE	0.15-0.4	NE	0.4-1.8*				
TP34-L	0.0-0.16	NE	0.16-0.6	0.6-3.0*	NE				
TP35-P	0.0-0.13	NE	0.13-0.6	NE	0.6-3.0*				
TP36-L	0.0-0.18	NE	0.18-0.8	0.8-3.0*	NE				
TP37-P	0.0-0.14	NE	0.14-0.5	1.7-3.2*	0.5-1.7				
TP38-P	0.0-0.15	0.15-0.4	0.4-0.7	NE	0.7-3.0*				
TP39-L	0.0-0.12	0.12-0.5	0.5-0.8	NE	0.8-3.0*				
TP40-P	0.0-0.21	NE	0.21-0.6	NE	0.6-3.0				

4.3 Groundwater

Groundwater was not encountered during the investigation. It should be noted that the groundwater conditions will vary with seasonal and weather conditions along with construction related Site conditions.



4.4 Laboratory Test Results

Geotechnical laboratory testing was carried out on selected bulk, disturbed and undisturbed samples collected during the site investigation. All testing was performed by Australian Soil and Concrete Testing (Newcastle) and Eurofins - NATA accredited laboratories in accordance with the relevant Australian Standards and technical procedures. The detailed results of laboratory testing are presented in **Appendix E – Laboratory Test Results** and are summarised in the following sections.

4.4.1 Atterberg Limits

A summary of Atterberg Limits and Linear Shrinkage test results are presented in Table 3 and are plotted graphically in Figure 4. Testing indicates that clayey materials are medium to high plasticity.

Table 3.	Table 3. Atterberg Limits Test Results												
Test Pit	Depth	Co.il	Classification	Att	erberg Lin	Linear							
ID	(m BGL)	Soil	Classification	LL (%)	PL (%)	PI (%)	Shrinkage (%)						
TP01-L	1.5-2.5	Sandy CLAY	CI	40	17	23	10.5						
ТРО7-Р	1.0-1.5	Clayey Gravelly SAND	CI-CH	39	17	22	8.5						
TP18-L	0.2-0.5	Silty CLAY	CI-CH	64	17	47	16.0						
TP25-P	1.5-2.5	Clayey Sandy GRAVEL	CI-CH	42	17	25	11.0						
TP35-P 1.5-2.0 Clayey Gravelly SAND CL-Cl 38 20 18 6.5													
LL – Liquid I	imit		•	•	•								

PL - Plastic Limit

PI – Plasticity Index

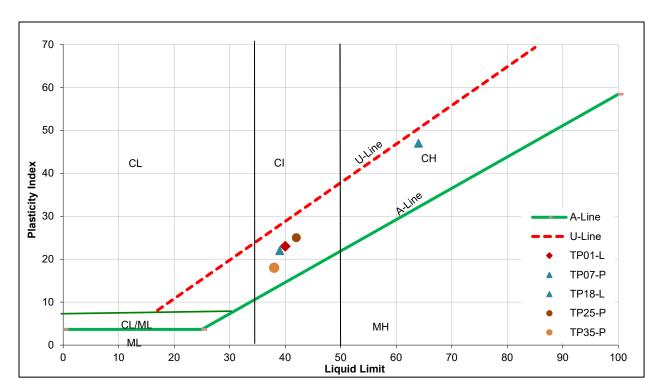


Figure 4. Atterberg Limit Plot



4.4.2 Particle Size Distribution

Particle Size Distribution (PSD) test results undertaken on samples of soil are presented in Table 4 and confirms the material description on the test pit logs.

Table 4. Particle Size Distribution Test Results											
Test Pit ID Depth (m BGL)		% passing 2.36 mm sieve	% passing 75 μm sieve	Sample Description							
TP01-L	1.5-2.5	74	44	Sandy CLAY with gravel							
TP07-P	1.0-1.5	51	15	Clayey Sandy GRAVEL							
TP18-L	0.2-0.5	100	87	Silty CLAY							
TP25-P	1.5-2.5	47	14	Clayey Sandy GRAVEL							
TP35-P	1.5-2.0	66	18	Clayey Gravelly SAND							

4.4.3 California Bearing Ratio (CBR)

CBR tests were undertaken on eight soil samples to inform the design CBR for the proposed road within the proposed development and the results are summarised in Table 6.

Table 5. Cali	Table 5. California Bearing Ratio Test Results											
Test ID	Depth (m BGL)	Sample Description	W¹(%)	SOMC ² (%)	SMDD³ (t/m³)	Swell (%)	CBR (%)					
TP02-P	1.5-2.1	XW Sandstone-Sandy CLAY	31.8	32.0	1.38	3.0	2.05					
TP09-P	1.1-1.5	Residual Soil-Silty CLAY	26.3	26.5	1.54	2.0	3.0 ⁵					
TP15-P	0.2-0.6	Residual Soil-Silty CLAY	33.2	29.0	1.46	3.0	2.05					
TP20-P	0.3-0.8	Slopewash-Silty CLAY	30.1	30.5	1.44	1.5	3.5 ⁵					
TP24-P	0.5-1.0	Slopewash-Silty CLAY	33.2	33.0	1.38	3.0	1.5 ⁴					
TP29-P	1.5-2.0	XW Sandstone-Sandy CLAY	12.5	15.0	1.87	0.5	25 ⁴					
TP37-P	1.7-2.5	XW Mudstone-Sandy CLAY	31.8	33.5	1.34	1.5	3.0 ⁵					
TP38-P	1.0-1.75	XW Sandstone-Clayey SAND	12.5	14.5	1.80	0.5	15.0 ⁴					

¹ Field Moisture Content

² Standard Optimum Moisture Content

³ Standard Maximum Dry Density

⁴ CBR at 2.5mm (%)

⁵CBR at 5mm (%)

^{*}XW-extremely weathered



4.4.4 Shrink-Swell

Undisturbed soil samples have been collected during field investigation and the results are shown in Table 5.

Table 6.	Table 6. Shrink-Swell Index Test Results											
			Shrinkage									
Test Pit ID	Soil Type	Depth (m BGL)	Shrinkage Field Moisture Content (%)	Dried Shrinkage (%)	Field Moisture Content (%)	Inundated Moisture Content (%)	Swell Strain (%)	Shrink – Swell Index (Iss%)				
TP01-L	Silty CLAY	0.7-1.2	26.0	-7.89	29.5	31.9	1.64	4.8				
TP19-L	Silty CLAY	0.3-0.8	27.1	-7.56	25.4	29.4	2.59	4.9				
TP23-L	Silty CLAY	0.3-0.8	26.8	-7.7	25.1	28.5	2.04	4.8				

4.4.5 Point Load Testing

It is noted the rock samples collected from test pits are competent bedrock fragments as the lower strength bedrock was broken down into soil during excavation. All the rock samples were collected dry and were tested dry which could potentially contribute to a higher strength rock interpretation. Point load testing has been conducted on selected rock samples collected from test pits and the test results are shown in Table 7.

Table 7. Po	Table 7. Point Load Test Results										
TP ID	Rock	Depth (m BGL)	Moisture condition	Is (MPa)	Is (50) MPa	Rock strength					
TP05-P	Mudstone	2.5-3.0	Moist	0.22	0.28	Low Strength					
TP05-P	Mudstone	2.5-3.0	Moist	0.19	0.23	Low Strength					
TP05-P	Mudstone	2.5-3.0	Moist	0.19	0.24	Low Strength					
TP05-P	Mudstone	2.5-3.0	Moist	0.15	0.2	Low Strength					
TP05-P	Mudstone	2.5-3.0	Moist	0.25	0.31	Medium Strength					
TP05-P	Mudstone	2.5-3.0	Moist	0.26	0.32	Medium Strength					
TP05-P	Mudstone	2.5-3.0	Moist	0.29	0.32	Medium Strength					
TP05-P	Mudstone	2.5-3.0	Moist	0.24	0.32	Medium Strength					
TP05-P	Mudstone	2.5-3.0	Moist	0.23	0.26	Low Strength					
TP05-P	Mudstone	2.5-3.0	Moist	0.42	0.44	Medium Strength					
TP05-P	Mudstone	2.5-3.0	Moist	0.24	0.3	Medium Strength					
TP05-P	Mudstone	2.5-3.0	Moist	0.23	0.28	Low Strength					
TP28-P	Sandstone	1.0-1.3	Moist	0.066	0.075	Very Low Strength					
TP28-P	Sandstone	1.0-1.3	Moist	0.2	0.27	Low Strength					
TP28-P	Sandstone	1.0-1.3	Moist	0.38	0.48	Medium Strength					
TP28-P	Sandstone	1.0-1.3	Moist	0.16	0.2	Low Strength					
TP28-P	Sandstone	1.0-1.3	Moist	0.61	0.69	Medium Strength					
TP28-P	Sandstone	1.0-1.3	Moist	0.51	0.58	Medium Strength					
TP28-P	Sandstone	1.0-1.3	Moist	0.61	0.75	Medium Strength					
TP28-P	Sandstone	1.0-1.3	Moist	0.88	1.0	High Strength					



Table 7. Point Load Test Results						
TP ID	Rock	Depth (m BGL)	Moisture condition	Is (MPa)	Is (50) MPa	Rock strength
TP28-P	Sandstone	1.0-1.3	Moist	0.67	0.86	Medium Strength
TP28-P	Sandstone	1.0-1.3	Moist	0.63	0.83	Medium Strength
TP28-P	Sandstone	1.0-1.3	Moist	0.24	0.3	Medium Strength
TP28-P	Sandstone	1.0-1.3	Moist	0.64	0.84	Medium Strength
TP32-P	Sandstone	0.5-1.2	Moist	0.42	0.52	Medium Strength
TP32-P	Sandstone	0.5-1.2	Moist	0.24	0.28	Low Strength
TP32-P	Sandstone	0.5-1.2	Moist	0.14	0.17	Low Strength
TP32-P	Sandstone	0.5-1.2	Moist	0.17	0.22	Low Strength
TP32-P	Sandstone	0.5-1.2	Moist	0.74	0.8	Medium Strength
TP32-P	Sandstone	0.5-1.2	Moist	0.3	0.6	Medium Strength
TP32-P	Sandstone	0.5-1.2	Moist	0.22	0.26	Low Strength
TP32-P	Sandstone	0.5-1.2	Moist	0.28	0.35	Medium Strength
TP32-P	Sandstone	0.5-1.2	Moist	0.34	0.43	Medium Strength
TP32-P	Sandstone	0.5-1.2	Moist	0.29	0.37	Medium Strength
TP32-P	Sandstone	0.5-1.2	Moist	0.47	0.6	Medium Strength
TP32-P	Sandstone	0.5-1.2	Moist	1.2	1.5	High Strength
ТРЗЗ-Р	Sandstone	1.0-1.8	Moist	0.033	0.039	Very Low Strength
TP33-P	Sandstone	1.0-1.8	Moist	0.48	0.57	Medium Strength
TP33-P	Sandstone	1.0-1.8	Moist	0.29	0.29	Low Strength
TP33-P	Sandstone	1.0-1.8	Moist	0.085	0.1	Very Low Strength
TP33-P	Sandstone	1.0-1.8	Moist	0.019	0.023	-
TP33-P	Sandstone	1.0-1.8	Moist	0.2	0.24	Low Strength
TP33-P	Sandstone	1.0-1.8	Moist	0.31	0.35	Medium Strength
TP33-P	Sandstone	1.0-1.8	Moist	0.25	0.29	Low Strength
ТРЗЗ-Р	Sandstone	1.0-1.8	Moist	0.3	0.36	Medium Strength
ТРЗЗ-Р	Sandstone	1.0-1.8	Moist	0.8	0.9	Medium Strength
ТРЗЗ-Р	Sandstone	1.0-1.8	Moist	0.21	0.22	Low Strength
ТРЗЗ-Р	Sandstone	1.0-1.8	Moist	0.13	0.17	Low Strength
-) below the n	ninimum rock strength of	very low				



4.4.6 Aggressivity

The Australian Standard AS2159-2009 provides criteria for assessment of the level of exposure classification for steel and concrete to enable the designers to incorporate protective measures for each element into the design. The assessment criteria are based upon the pH, concentrations of Sulphate and Chloride in soil, the soil permeability, and the groundwater level.

Soil aggressivity testing was undertaken on three (3) sample recovered from boreholes. An assessment of the exposure classification for the soil sample tested based on the above criteria is presented in Table 8.

Table 8. Aggressivity Test Results								
		Sulphates		Chlorides in		Exposure classification		
Test Pit ID	Soil type	(SO ₄) in soil (mg/kg - ppm)	рН	groundwater (mg/kg- ppm)	Resistivity ohm.cm	Aggressive to steel	Aggressive to concrete	
TP11-L	Sandy CLAY	<25	9.0	100	7500	Non-Aggressive	Non-Aggressive	
TP36-L	Sandy CLAY	<25	8.7	100	6800	Non-Aggressive	Non-Aggressive	
TP40-P	Clayey SAND	<25	9.5	220	3200	Mild	Mild	



5 Pavement Design

5.1 Design Traffic Loadings

Design traffic loadings have been selected and pavement thickness design calculations have been undertaken by EP Risk in accordance with *Maitland City Council - Manual of Engineering Standards*.

The design traffic data has been determined based on the following assumptions in Table 9.

Table 9. Recommended Road Type and Design ESA's				
Road Type	Roads Identification	Design ESA's		
Local - Secondary	TBC	2 x 10 ⁵		
Local - Primary	TBC	5 x 10 ⁵		
Collector - Secondary	TBC	1 x 10 ⁶		
Collector - Primary	TBC	1.5 x 10 ⁶		
Distributor – Secondary (Bus Route)	TBC	2 x 10 ⁶		

Where traffic data varies from the above assumptions a review of pavement design will be required particularly considering connectivity with adjacent developments.

5.2 Design Parameters

Pavement thickness has been undertaken in accordance with Austroads AGPT02-17 Guide to Pavement Technology, Part 2: Pavement Structural Design based on the following parameters:

- Design subgrade CBR of 2% for Silty CLAY (TP02-P and TP15-P).
- Design CBR of 3% for extremely weathered Mudstone/Sandstone-Sandy CLAY and residual soil.
- Design CBR of 6% for extremely weathered Sandstone Clayey SAND.
- CBR of 10% for distinctly weathered Mudstone/Sandstone. CBR 10% is likely to be appropriate for the areas of deeper cut in the north-western part of the site.
- Design traffic as per Table 9.

The design subgrade has been determined in accordance with Section 5 of Austroads 2017 based on laboratory testing results and field interpretation.

The CBR Swell results when compared to Table 5.2 in Austroads Guide to pavement Technology Part 2: Pavement Structural Design indicate that the soils tested have generally a moderate to high expansive nature and specific strategies are likely required to address potential volume change due to moisture variation in the subgrade. This will largely be dependent on the vertical alignment of roads and the material present within 0.5 m of design subgrade level (DSL).

Where filling is undertaken within the road alignments, the CBR of the fill material should be considered specifically regarding the final pavement design subgrade CBR. All fill materials should generally be a minimum of CBR 3% based on 4-day soak when compacted to 100% standard relative density and SOMC except where the final pavement design is based on a subgrade design CBR of 10%. Subgrade replacement with suitable site won materials is recommended for isolated areas of lower strength subgrade (TP24-P).



5.3 Pavement Design – Flexible Unbound Pavement

The option of pavement construction utilising flexible unbound pavement materials for Silty/Sandy CLAY, XW Mudstone/ Sandstone and slightly weathered/fresh Mudstone/Sandstone are detailed in Table 11, Table 12, Table 13 and Table 14.

In accordance with latest Council directive any subgrade with CBR <3 or with CBR swell ≥2.5% will require a minimum 300mm select layer. The select layer could be sourced from the areas of cut across the site subject to laboratory testing and Council approval. It is noted the *Maitland City Council - Manual of Engineering Standards (MoES)* requires 100 mm minimum base thickness and 125 mm minimum sub-base thickness with overall pavement thickness being a minimum of 300mm. Due to the profile of standard SA kerb and roll kerb and gutter. Basecourse is normally specified as a minimum of 150mm for construction practicality.

Table 10. Recommended	Flexible Pavement	Composition – CBR 2%
Table to vecommenden	riexible raveillelli	. CUITIDUSTLIUTT — CBR 2/6

Road Type	Distributor - Bus Route	Collector Primary	Collector Secondary	Local - Primary	Local Secondary
Wearing Course (mm)	45 AC14 HD*	45 AC14 HD*	45 AC14 HD*	30 AC10*	30 AC10*
Basecourse (mm)	150	150	150	160**	160**
Subbase (mm)	185	165	140	125	125
Select (mm)	300	300	300	300	300
Total Thickness (mm)	680	660	635	615	615
Subgrade CBR	min 2%	min 2%	min 2%	min 2%	min 2%
Design ESA	2.0 × 10 ⁶	1.5 x 10 ⁶	1.0 × 10 ⁶	5.0 × 10 ⁵	2.0 x 10 ⁵

^{*}AC14/AC10* with 10mm primer seal placed under the asphaltic concrete wearing surface

Table 11. Recommended Flexible Pavement Composition - CBR 3%

Road Type	Distributor - Bus Route	Collector Primary	Collector Secondary	Local - Primary	Local Secondary
Wearing Course (mm)	45 AC14 HD*	45 AC14 HD*	45 AC14 HD*	30 AC10*	30 AC10*
Basecourse (mm)	150	150	150	160**	160**
Subbase (mm)	125	125	125	290 (125)	250 (125)
Select (mm)***	300	220	200	(300)	(300)
Total Thickness (mm)	620	540	520	480 (615)	425 (615)
Subgrade CBR	min 3%	min 3%	min 3%	min 3%	min 3%
Design ESA	2.0 × 10 ⁶	1.5 x 10 ⁶	1.0 × 10 ⁶	5.0 × 10 ⁵	2.0 x 10 ⁵

^{*}AC14/AC10* with 10mm primer seal placed under the asphaltic concrete wearing surface

^{**} Basecourse layer will be 160mm to suit standard kerb & gutter (modified SA) or roll kerb.

^{**} Basecourse layer will be 160mm to suit standard kerb & gutter (modified SA) or roll kerb.

^{***} Minimum CBR 30% required for the CBR 3% option. Where CBR swell is ≥2.5% select should be increased to 300mm with subbase thickness reduced accordingly as per bracketed values.



Road Type	Distributor - Bus Route	Collector Primary	Collector Secondary	Local - Primary	Local Secondary
Wearing Course (mm)	45 AC14 HD*	45 AC14 HD*	45 AC14 HD*	30 AC10*	30 AC10*
Basecourse (mm)	150	150	150	160**	160**
Subbase (mm)	250	205	180	140	140
Total Thickness (mm)	445	400	375	330	330
Subgrade CBR	min 6%	min 6%	min 6%	min 6%	min 6%
Design ESA	2.0 × 10 ⁶	1.5 x 10 ⁶	1.0 × 10 ⁶	5.0 × 10 ⁵	2.0 x 10 ⁵

^{*}AC14/AC10* with 10mm primer seal placed under the asphaltic concrete wearing surface

Table 13. Recommended Flexible Pavement Composition – CBR 10%

Road Type	Distributor - Bus Route	Collector Primary	Collector Secondary	Local - Primary	Local Secondary
Wearing Course (mm)	45 AC14 HD*	45 AC14 HD*	45 AC14 HD*	30 AC10*	30 AC10*
Basecourse (mm)	150	150	150	160**	160**
Subbase (mm)	150	150	150	125	125
Total Thickness (mm)	345	445	345	315	315
Subgrade CBR	min 10%	min 10%	min 10%	min 10%	min 10%
Design ESA	2.0 × 10 ⁶	1.5 x 10 ⁶	1.0 × 10 ⁶	5.0 × 10 ⁵	2.0 x 10 ⁵

^{*}AC14/AC10* with 10mm primer seal placed under the asphaltic concrete wearing surface

A minimum of fourteen days duration shall apply prior to application of asphalt layer. That period may be extended or shortened subject to approval by Council. It is noted Maitland City Council requires minimum 40mm AC (14) "Heavy Duty" for Classified Roads a 45mm AC14 wearing course has been specified to comply with 3-time nominal size of aggregate and provide improved durability.

For areas where the clay subgrade has a CBR <3 or swell ≥2.5%, the pavement design incorporate a 300mm select layer with minimum CBR of 15% or other measures detailed in Austroads Guidelines for managing soils with a swell potential. Select with CBR of 30% is specified for the design Subgrade of 2% and 3%. The design CBR needs to be confirmed on road alignment following the regrade activities on site. Where subgrade is at elevated moisture content at the time of construction a select layer will be likely be required and should be provisioned for particularly in lower lying areas in the southern section of the site.

5.4 Subgrade Preparation

Where construction of a new pavement is proposed, subgrade preparation should be in general accordance with the following procedures.

- Remove topsoil and excavated to design subgrade level.
- Ripping the encountered weathered Mudstone/Sandstone to 300-350mm below DSL and recompact to a minimum 100% of SMDD. Moisture contents should be within 70% to 90% of SOMC for weathered

^{**} Basecourse layer will be 160mm to suit standard kerb & gutter (modified SA) or roll kerb.

 $^{^{**}}$ Basecourse layer will be 160mm to suit standard kerb & gutter (modified SA) or roll kerb.



bedrock and closer to SOMC where highly expansive subgrade materials are encountered or used as fill

- Static proof-rolling of the exposed subgrade using a heavy (minimum 10 tonne) roller under the direction of an experienced geotechnical consultant.
- Loose or yielding areas should be excavated and replaced with compacted select fill or suitable subgrade replacement comprising material of similar consistency to the subgrade.
- Confirmation of design subgrade parameters by geotechnical consultant.
- Where filling or subgrade replacement is required, the materials employed should be free of organics
 or other deleterious material. The material should also have a maximum particle size of 100mm or one
 third of the layer thickness, with a minimum soaked CBR >3%. Low to moderate expansive/reactive
 material should be used as subgrade and general fill where possible in the top 1m to design levels.

Following satisfactory preparation of the subgrade, the pavement should be constructed in accordance with the recommendations or this report and *Maitland City Council – Manual of Engineering Standards Construction*. In case of discrepancy clarification should be obtained from Council.

5.5 Drainage

The moisture regime associated with a pavement has a major influence on the performance considering the stiffness/strength of the pavement materials is dependent on the moisture content of the material used. Accordingly, to protect the pavement materials from wetting up and softening, particular care would be required to provide a waterproof seal for the pavement materials, together with adequate surface and sub-surface drainage of the pavement and adjacent areas.

It is recommended that subsoil drainage be installed along both side of all roads within the development in accordance with Council requirements, with subsoil installed at subgrade level in highly expansive subgrade. CBR swell results from the preliminary investigation range from moderate to highly expansive. Design measures and subsurface drainage measures to control subgrade swell are provided in Austroads Pavement Guide to Pavement Technology and the relevant Transport for New South Wales Supplement(s). Preferred measures shall also be discussed with Council's Representative prior to adoption in any pavement construction. Designs utilising a 300mm select layer are provided in Tables 11 and 12.

The pavement thickness designs presented above assume drained pavement conditions. The selection, construction and maintenance of appropriate drainage infrastructure would be required for adequate performance. The selection of appropriate construction materials that are relatively insensitive to moisture change is also essential in area subject to periodic inundation, even if for a relatively short period of time.

5.6 Materials

5.6.1 Specifications and Compaction Requirements

Pavement materials and compaction requirements for new pavement construction should conform to Council requirements outlined in MoES and the following requirements outlined in Table 15.



Table 14. Material Specification and Compaction Requirements					
Pavement Course	Material Specification	Compaction Requirements			
Base Course DGB20 (Class 1 &2) & NGB20** MoES (Cl 9.1.2)	Material complying with Council MoES Table 242.3 for the appropriate traffic category	Min 98% Modified (AS 1289 5.2.1)			
Subbase Subbase quality crushed rock (DGS20, DGS40, GMS40, NGS20, NGS40) MoES (CI 9.1.2)	Material complying with Council MoES	Min 95% Modified (AS 1289 5.2.1)			
Select Granular material	Minimum CBR 15%, (min 30% for Design CBR of ≤3%) and PI ≤15% conforming to Council MoES	Min 100% Standard (AS 1289 5.1.1)			
Subgrade or replacement	Minimum CBR as appropriate for the design option.	Min 100% Standard (AS 1289 5.1.1)			

^{*) -} Class 1 material should be used on sub-arterial category roads

Minimum testing on all potential imported pavement materials should be in accordance with TfNSW 3051 Ed 7. Pre-treatment of material prior to testing would be advisable for materials subject to breakdown.

5.6.2 Wearing Course

Wearing courses should be in accordance with Council's specifications with reference to TfNSW QA Specifications R116 for Dense Graded Asphalt. It is noted that a minimum of 40mm AC14 (Heavy Duty) wearing course is utilised for classified roads in accordance with Council Specifications. 45mm of AC14 heavy duty has been specified to meet the minimum 3 time the nominal size of aggregate. Recent trials have also shown that 48mm of AC14 is the optimal thickness for durability.

The design and construction of wearing courses should be in in consultation with the preferred supplier considering traffic volume and type. All pavement surfaces should be primer sealed prior to the application of the AC wearing course. A minimum delay of 14 days is required after the primer seal before placement of the AC wearing course.

5.6.3 Inspections

The subgrade will require inspection by an experienced geotechnical consultant after boxing out or filling to design subgrade level. The purpose of inspections is to confirm design parameters, assess the suitability of the subgrade to support the pavement, and delineate areas which may require subgrade replacement or remedial treatment prior to construction.

^{**)} NGB and NGS material cannot be used on collector category road or higher due to higher design traffic. Material should comply with Council MoES Appendix D – Pavement Material Properties for the appropriate traffic category



6 Preliminary Site Classification

Australian Standard AS 2870-2011 establishes performance requirements and specific designs for common foundation conditions as well as providing guidance on the design of footing systems using engineering principles. Site classes as defined on Table 2.1 and 2.3 of AS 2870 are presented in Table 16.

Table 15. G	Table 15. General Definition of Site Classes				
Site Class	Foundation Characteristic Surfa				
А	Most sand and rock sites with little or no ground movement from moisture changes	-			
S	Slightly reactive clay sites, which may experience only slight ground movement from moisture changes	0 – 20 mm			
М	Moderately reactive clay or silt sites, which may experience moderate ground movement from moisture changes	20 – 40 mm			
H1	Highly reactive clay sites, which may experience high ground movement from moisture changes	40 – 60 mm			
H2	Highly reactive clay sites, which may experience very high ground movement from moisture changes	60 – 75 mm			
Е	Extremely reactive sites, which may experience extreme ground movement from moisture changes > 75 mm				
A to P	Filled sites (refer to clause 2.4.6 of AS 2870)				
Р	Sites which include soft soils, such as soft clay or silt or loose sands; landslip; mine subsidence; collapsing soils; soils subject to erosion; reactive sites subject to abnormal moisture conditions or sites which cannot be classified otherwise.				

Reactive sites are sites consisting of clay soils that swell on wetting and shrink on drying, resulting in ground movements that can damage lightly loaded structures. The amount of ground movement is related to the physical properties of the clay and environmental factors such as climate, vegetation, and watering. A higher probability of damage can occur on reactive sites where abnormal moisture conditions occur, as defined in AS 2870, due to factors such as:

- Presence of trees on the building site or adjacent site, removal of trees prior to or after construction, and the growth of trees too close to a footing. The proximity of mature trees and their effect on foundations should be considered when determining building areas within each allotment (refer to AS 2870).
- Failure to provide adequate site drainage or lack of maintenance of site drainage, failure to repair plumbing leaks and excessive or irregular watering of gardens.
- Unusual moisture conditions caused by removal of structures, ground covers (such as pavements), drains, dams, swimming pools, tanks etc.

Regarding the performance of footings systems, AS 2870 states "footing systems designed and constructed in accordance with this Standard on a normal site (see Clause 1.3.2) that is:

- a) not subject to abnormal moisture conditions; and
- b) maintained, such that the original site classification remains valid and abnormal moisture conditions do not develop, are expected to usually experience no damage, a low incidence of damage category 1 and an occasional incidence of damage category 2."

Damage categories are defined in Appendix C of AS 2870, which is reproduced in CSIRO Information Sheet BTF 18, Foundation Maintenance and Footing Performance: A Homeowner's Guide attached as **Appendix F** – **Foundation Maintenance and Footing Performance**.



The laboratory Shrink Swell test results summarised in Table 5 indicate that the tested Silty CLAY soil returned an I_{ss} value of 4.8% in TP01-L and TP23-L and an Iss value of 4.9% for TP19-L. Atterberg limit testing is also indicative of highly reactive material in the residual clay materials.

The classification of sites with controlled fill of depths greater than 0.4m (deep fill) comprising of material other than sand would be Class P. An alternative classification may however be given to sites with controlled fill where consideration is made to the potential for movement of the fill and underlying soil based on the moisture conditions at the time of construction and the long-term equilibrium moisture conditions.

Based on the subsurface profiles encountered during the Site inspection and in accordance with the AS 2870-2011; the Site in its existing condition and in the absence of abnormal moisture conditions would likely be classified as detailed in Table 17.

Table 16. Anticipated Site Classifications		
Gosforth - Anambah Road	Site Classification	
In Existing Condition prior to regrade	Class H1 and Class H2, highly reactive	
Following regrade activities	Class H1 and Class H2, highly reactive	

A characteristic surface movement (y_s) of 45mm to 65mm has been calculated for the site dependent on the soil profile in its existing state prior to regrade, using a depth of design suction (Hs) change of 2.3m. Following regrade characteristic surface movement (y_s) in the order of 93mm to 109mm have been calculated using worst case scenarios as the depth of the cracked zone is considered zero as per AS2870-2011 Clause 2.3.2. Actual site classifications will be dependent on regrade activities including depth to rock and filling depth along with the materials utilised as fill.

NB: Careful material management will be required to avoid Class E classifications and ensure best outcomes for site classifications and pavements design especially in the southern part of the site. Reactive fill material should be placed below 1.5m of finished design levels.

The above site classifications and footing recommendations are for the site conditions present at the time of fieldwork and consequently the site classification may need to be reviewed with consideration of any site works that may be undertaken after the investigation and this report.

Site works may include:

- Changes to the existing soil profile by cutting and filling.
- Landscaping, including trees removed or planted in the general building area; and
- Drainage and watering systems.

Designs and design methods presented in AS 2870-2011 are based on the performance requirement that significant damage can be avoided if site conditions are properly maintained. Performance requirements and foundation maintenance are outlined in Appendix B of AS 2870. The above site classification assumes that the performance requirements as set out in Appendix B of AS 2870 are acceptable and that site foundation maintenance is undertaken to avoid extremes of wetting and drying.

Details on appropriate site and foundation maintenance practices are presented in Appendix B of AS 2870-2011 and in CSIRO Information Sheet BTF 18, Foundation Maintenance and Footing Performance: A Homeowner's Guide. Adherence to the detailing requirement outlined in Section 5 of AS 2870-2011 is essential, Section 5.6. Additional requirements for Classes M, H1, H2 and E sites, including architectural restrictions, plumbing and drainage requirements.



7 General Construction Considerations

7.1 Excavatability Assessment

Practical machine refusal for the 24-tonne excavator was encountered on a combination of mudstone and sandstone in seven (7) test pits out of the forty (40) excavated test pits. Refusal depths ranged from 1.2m BGL to 2.5m BGL. The strength of bedrock encountered in test pits assessed by point load testing ranges from very low to high strength. To assess the excavatability of the bedrock, the strength range is plotted on the graph in Figure 6 for excavatability as per the suggested method by Pettifer and Fookes. The area of the chart covered indicates that hard to very hard ripping by a D9 will be typically the excavation method for the type of rock encountered within the Site area.

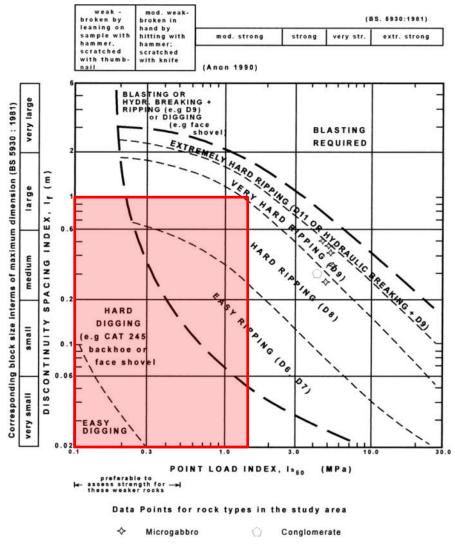


Figure 5. Excavatability Assessment (Pettifer and Fookes)

Excavations to depths of 1.5m-1.8 m BGL in weathered bedrock are expected to be readily achievable using larger (>25T) conventional earthmoving equipment. Excavations below 2m deep (especially in confined space like trenches) in slightly weathered/fresh bedrock may require excavators fitted with tiger teeth buckets or single ripper attachment and potential hydraulic hammering in isolated confined areas where high strength rock is encountered.

Excavatability conditions have not been assessed beyond the depths to which the test pits were excavated; however, the following general comments regarding rock mass excavatability conditions can be made:



- Rock strength as well as rock mass defect (joint) spacing could be expected to control rock mass excavatability. Rock strength is likely to be variable and layers of weaker rock can underlie stronger bedrock.
- Excavatability could be expected to be dependent on the plant used, the experience of the operator and the degree of confinement within the excavation.

It is recommended that long-term excavations are either battered at 2H:1V or flatter and protected against erosion or be supported by engineer designed and suitably constructed retaining walls. Excavations may be battered steeper than 2H:1V in rock materials, subject to specific geotechnical Investigation.

Excavations or trenches in the Silty/Sandy CLAY and extremely weathered material could be expected to stand close to vertical in the short-term. Where personnel are to enter excavations, options for short-term excavations stability include benching or battering back of the excavations to 1H:1V or the support of excavations within the residual soil and extremely weathered rock profile.

The excavation recommendations provided above should be considered with reference to the Safe Work Australia Code of Practice 'Excavation Work', dated January 2020.

7.2 Retaining Structures

All retaining structures should be designed by an engineer. Design of retaining walls should:

- Count surcharge loading from slopes and structures above the wall.
- Consider loading from any proposed compaction of fill behind the wall.
- Provide adequate surface and subsurface drainage behind all retaining walls, including a free draining granular backfill to prevent the build-up of hydrostatic pressures behind the wall.
- Utilise materials that are not susceptible to deterioration.
- Ensure walls are founded in materials appropriate for the loading conditions.

Footings for proposed retaining walls should be founded below any topsoil or slopewash within stiff or better consistency clay or weathered rock.

7.3 Filling and Material Management

Fill should be placed and compacted in accordance with AS 3798-2007. It is expected that construction of a suitable fill platform to support structural loads, such as pavements, ground slabs, footing and stiffened raft slabs, would include the following:

- Stripping of topsoil.
- Removal of any unsuitable soil (if applicable).
- Wet material where encountered (along the drainage lines across the site and in the southern part of
 the site) will likely require treatment or moisture re-conditioning (drying and blending with dryer fill
 material) prior to placement and compaction.
- Proof rolling of the exposed subgrade to detect any weak or deforming areas of subgrade that should be excavated and replaced with controlled fill.



- Placement of fill in horizontal layers with compaction of each layer to a minimum dry density ratio of 95% Standard Relative Density (SRD) as per Australian Standard AS 1289 Clause 5.1.) at moisture contents of 85- 115% of SOMC and 98% SRD for fill ≥1m depth. Fill within 0.5m of design subgrade in road alignments is to be compacted to 100% standard relative density at a 70-100% of SOMC.
- All fill materials should be supported by properly designed and constructed retaining walls or else battered at a slope of 2H:1V or flatter and protected against erosion by vegetation or similar and the provision of adequate drainage.

7.3.1 Material Management

The material management during regrade for this site will be critical due to the presence of highly reactive cohesive soils ($I_{ss} \ge 4.8\%$) and depth to the rock 1.6m BGL in some areas of the site.

Good material management practices should be employed for this site to avoid lot classification with Class E. Reactive / Expansive clay materials should be placed as close to SOMC as practical to minimise their swell potential and preferentially placed in lower layers of the deeper fill areas (≥1.15m BGSL). It will also be critical not to over compact material dry of SOMC.

Materials excavated on Site apart from topsoil and slopewash are considered suitable for re-use as engineering fill. Some materials such as slopewash will likely require treatment such as blending and moisture reconditioning to produce suitable structural fill, subject to further assessment and weather conditions prior to and during construction. Material should be managed during regrade to allow use of required design CBR and lower reactivity material in the top 1m of filling and subgrade preparation to provide better outcome for pavement construction and site classification. Higher CBR material used in the upper 0.3-0.5m of subgrade will influence the design CBR which can be adopted.

7.4 Geotechnical Design Parameters

The geotechnical parameters for the proposed development have been assessed based on results of the site and laboratory tests of the ground investigation. These are provided for the different geological units: soils in Table 18 and for bedrock in Table 16. The design parameters for bedrock have been assumed based on the observations during site investigation.

The low consistency topsoil layer has been considered unsuitable for shallow foundations and no design parameters have been calculated for these units.

Table 17. Geotechnical Design Parameters-soil								
Geotechnical Units	Bulk Unit Weight (kN/m3)	Undrained Cohesion Cu (kPa)	Drained Cohesion c' (kPa)	Drained friction angle φ' (°)	Poisson's Ratio (-)	Elastic Modulus E' (MPa)	Earth Pressure coefficient ka	Earth pressure coefficient kp
RESIDUAL SOIL/ SLOPEWASH Silty/Sandy CLAY (stiff or better)	19	50-75	3-5	26	0.3	10	0.39	2.56

The allowable bearing capacity for the stiff or better residual soil is estimated to 100kPa.



Table 18 - Geotechnical	Design Parameters-Rock

Geotechnical Unit (strength)	Bulk Unit Weight (kN/m3)	Allowable Bearing Pressure (MPa)*	Ultimate shaft adhesion (kPa)**	Poisson's Ratio (-)	Elastic Modulus E' (MPa)	
MUDSTONE	20	0.7	50	0.3	50	
very low strength (Class V)	20	0.7	30	0.5		
SANDSTONE very low strength (Class V)	20	0.8	150	0.35	50	
SANDSTONE low strength (Class IV)	21	2	250	0.3	100	
SANDSTONE medium strength (Class III)	22	3.5	800	0.25	350	

^{*)} Bearing pressure to limit the settlement to <1% of minimum footing size
**) clean socket of roughness category R2 or better



8 References

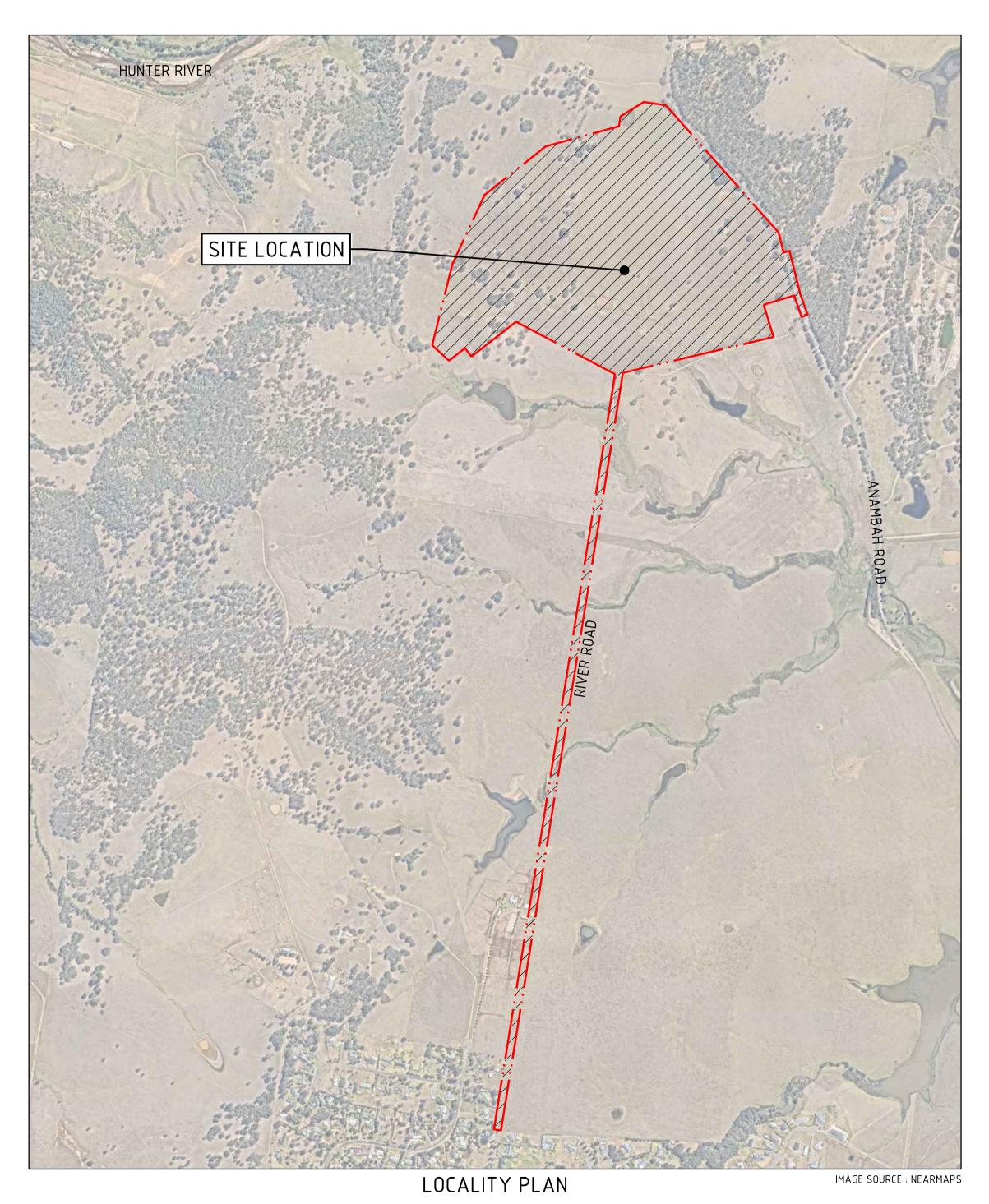
- Austroads AGPT05-19, "Guide to Pavement Technology Part 5: Pavement Evaluation and Treatment Design," Austroads Ltd, October 2019
- Austroads AGPT02-17, "Guide to Pavement Technology Part 2: Pavement Structural Design," Austroads Ltd, 2017.
- Australian Standard AS2870-2011 "Residential slabs and footing"
- Australian Standard AS3798-2007 "Guideline on earthworks for commercial and residential developments".
- Australian Standard AS2159-2009, "Piling Design & Installation," Standards Australia, 2009
- eSPADE, Online website of NSW Office of Environment and heritage (www.environment.nsw.gov.au)
- NSW Department of Planning and Environment, Resources and Geoscience (www.resourcesandgeoscience.nsw.gov.au)
- Maitland City Council Manual of Engineering Standards April 2023.
- TfNSW QA Specification 3051 (Ed 7 Rev 0), "Granular Base and Subbase Materials for Surfaced Road Pavements," Roads and Maritime Services, April 2011
- TfNSW QA Specification 3051 (Ed 7 Rev 0), "Granular Base and Subbase Materials for Surfaced Road Pavements," Roads and Maritime Services, August 2018.

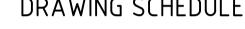


Appendix A MASTERPLANNING DEVELOPMENT APPLICATION – CIVIL ENGINEERING PACKAGE

PROPOSED SUBDIVISION, 559 ANAMBAH ROAD GOSFORTH NSW 2320

CIVIL ENGINEERING PACKAGE





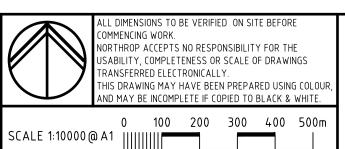
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						COMMUNITIES
						DRAWING NOT TO BE USED FOR CONSTRUCTION







Level 1, 215 Pacific Hwy, Charlestown NSW 2290 Ph (02) 4943 1777 Email newcastle@northrop.com.au ABN 81 094 433 100

MP-C05.43 ROAD LONGITUDINAL SECTIONS - SHEET 13

MP-C05.44 ROAD LONGITUDINAL SECTIONS - SHEET 14

MP-C05.45 ROAD LONGITUDINAL SECTIONS - SHEET 15

PROPOSED SUBDIVISION **559 ANAMBAH ROAD GOSFORTH NSW 2320**

MASTERPLANNING DA

CIVIL ENGINEERING PACKAGE

MP-C08.33 ROAD LONGITUDINAL SECTIONS RIVER ROAD - SHEET 3

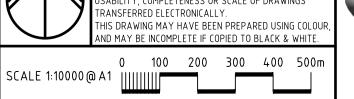
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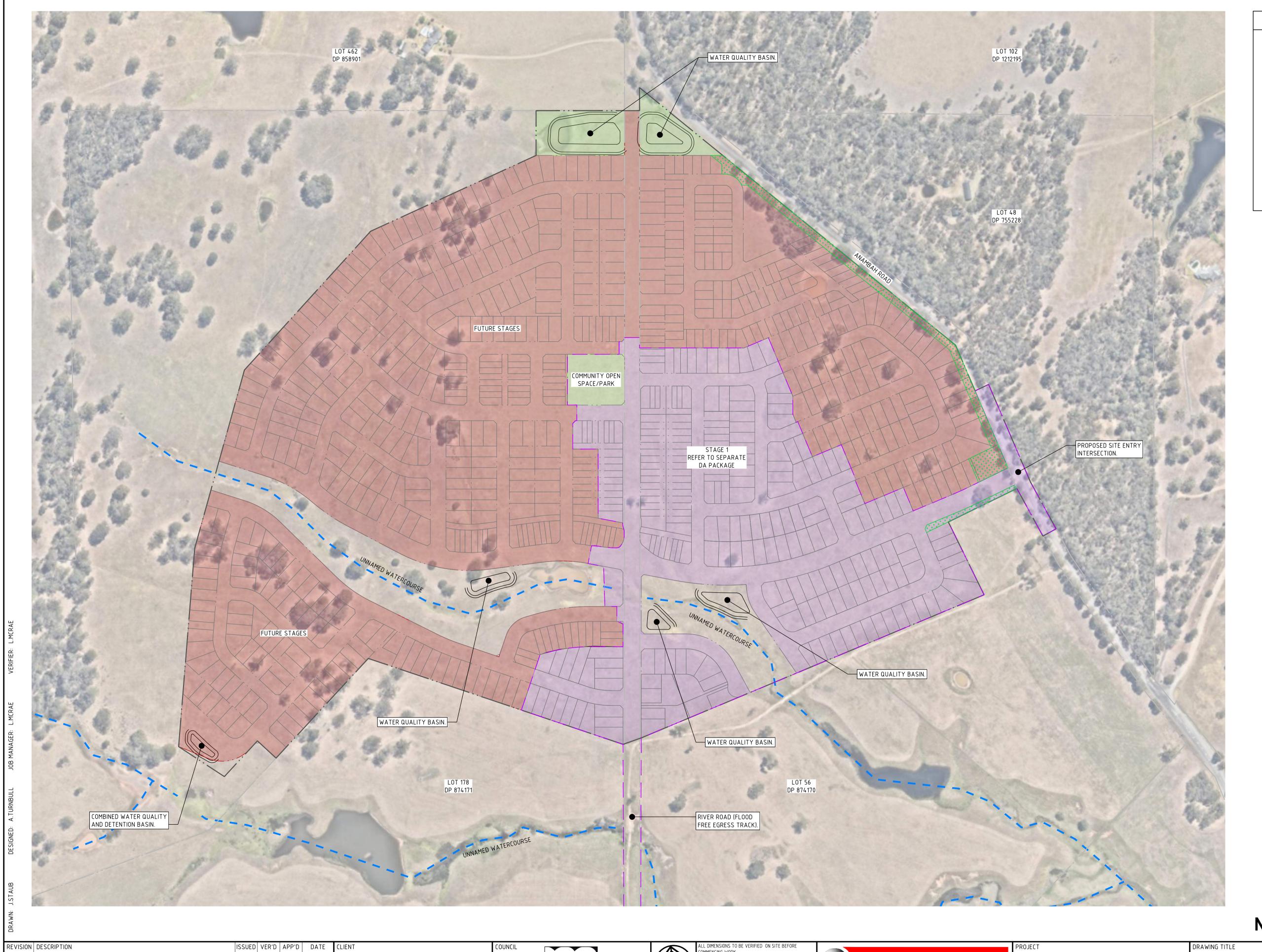
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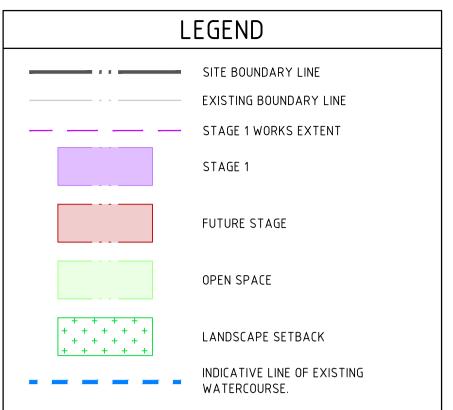
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MASTERPLANNING DEVELOPMENT APPLICATION





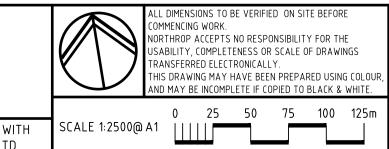


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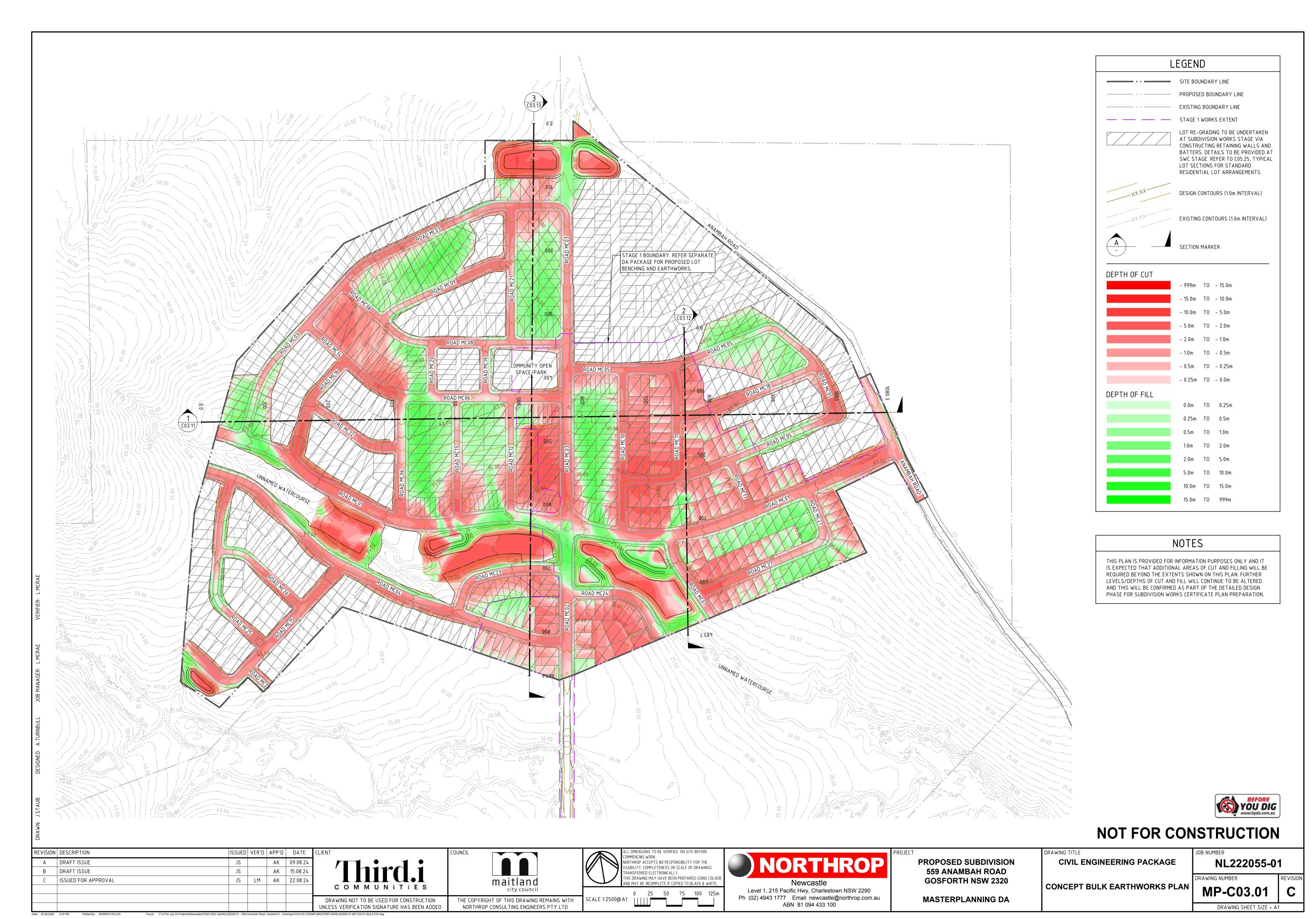
PROPOSED SUBDIVISION 559 ANAMBAH ROAD **GOSFORTH NSW 2320**

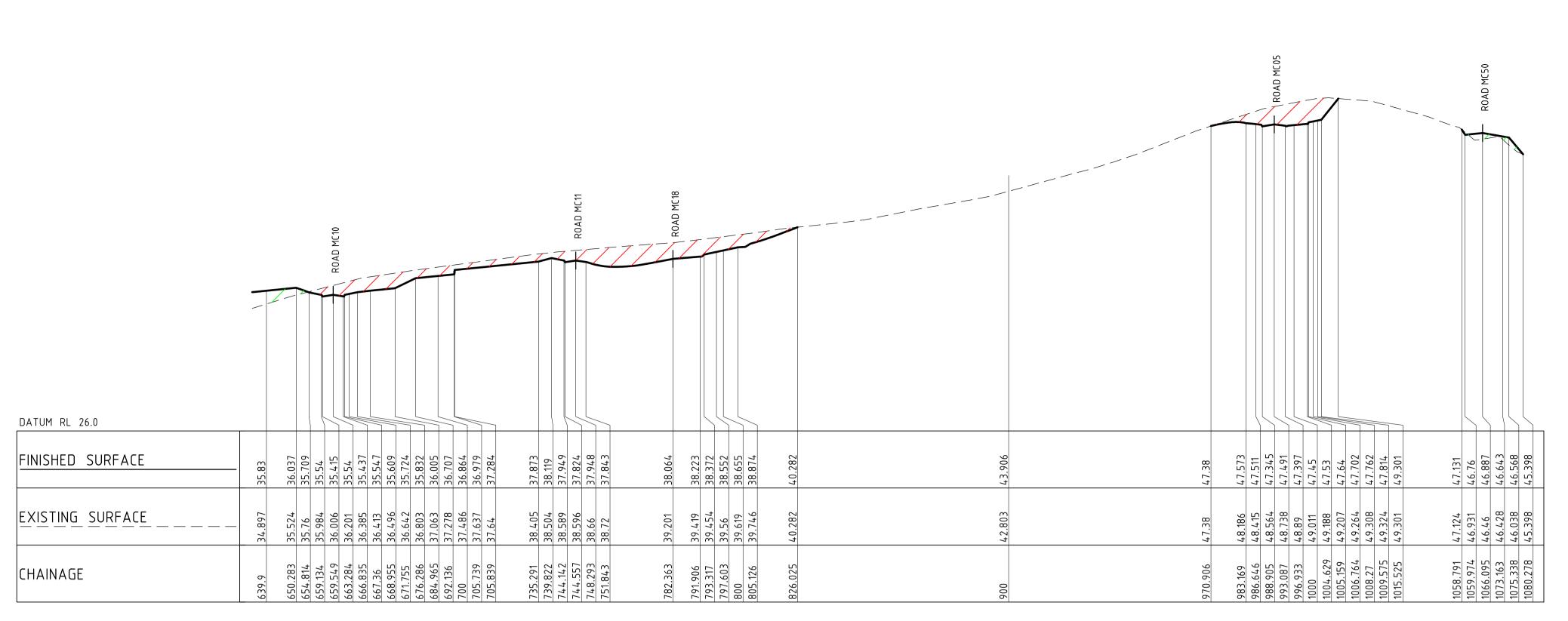
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CIVIL ENGINEERING PACKAGE STAGING PLAN

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	MP-C02.01	

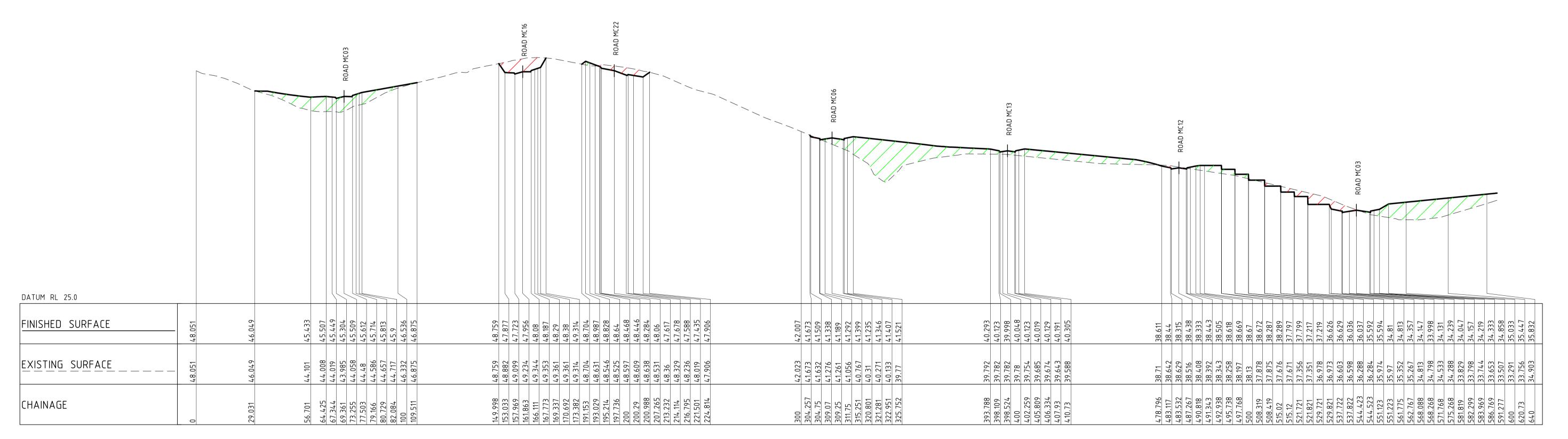
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LONGITUDINAL SECTION ALONG 1
HORIZONTAL SCALE 1:1000@A1

VERTICAL SCALE 1:200@A1

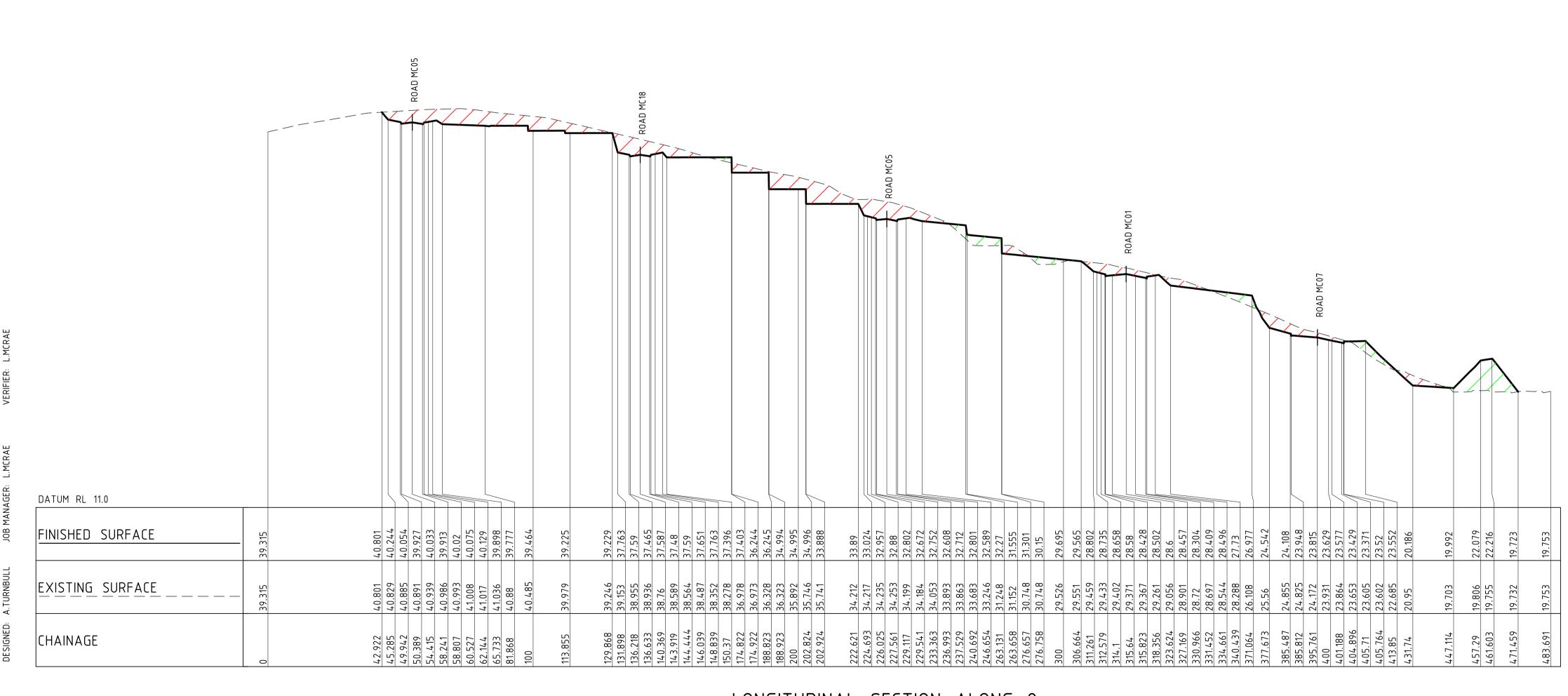


LONGITUDINAL SECTION ALONG 1 HORIZONTAL SCALE 1:1000@A1 VERTICAL SCALE 1:200@A1



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					maitland	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR, AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE	Newcastle	GOSFORTH NSW 2320		DRAWING NUMBER REVISION
				COMMUNITIES	city council	CCALE 44000 @ A4 0 10 20 30 40 50m	Level 1, 215 Pacific Hwy, Charlestown NSW 2290		BULK EARTHWORKS SITE SECTIONS	MP-C03.11 B
				DRAWING NOT TO BE USED FOR CONSTRUCTION	THE COPYRIGHT OF THIS DRAWING REMAINS WITH	SCALE 1:1000 @ A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au	MASTERPLANNING DA	- SHEET 1	WII -000.11
				UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED	NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:200@ A1	ABN 81 094 433 100			DRAWING SHEET SIZE = A1
Date: 22.08.2024	22.08.2024 4:53 PM Plotted By: ANDREW KILLEN Found: O/15 Pre-July 24 Projects\Newcastle\YEAR 2022 Jobs\N1222055-01 - 559 Anambah Road, Gosforth\O - Drawings\CIVIL\03-CAD\MP-MASTERPLAN\N1222055-01-MP-C03.01-BULK EW.dwg									



LONGITUDINAL SECTION ALONG 2
HORIZONTAL SCALE 1:1000@A1 VERTICAL SCALE 1:200@A1



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ABN 81 094 433 100

PROPOSED SUBDIVISION

559 ANAMBAH ROAD GOSFORTH NSW 2320

MASTERPLANNING DA

BULK EARTHWORKS SITE SECTIONS

- SHEET 2

NL222055-01 CIVIL ENGINEERING PACKAGE DRAWING NUMBER

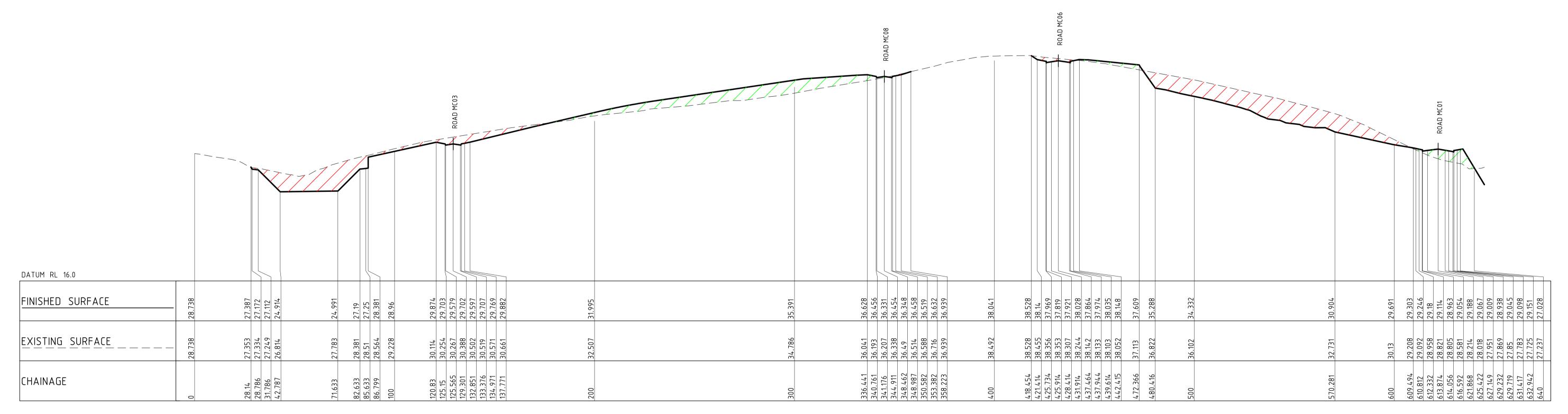
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LONGITUDINAL SECTION ALONG 3

HORIZONTAL SCALE 1:1000@A1

VERTICAL SCALE 1:200@A1



LONGITUDINAL SECTION ALONG 3

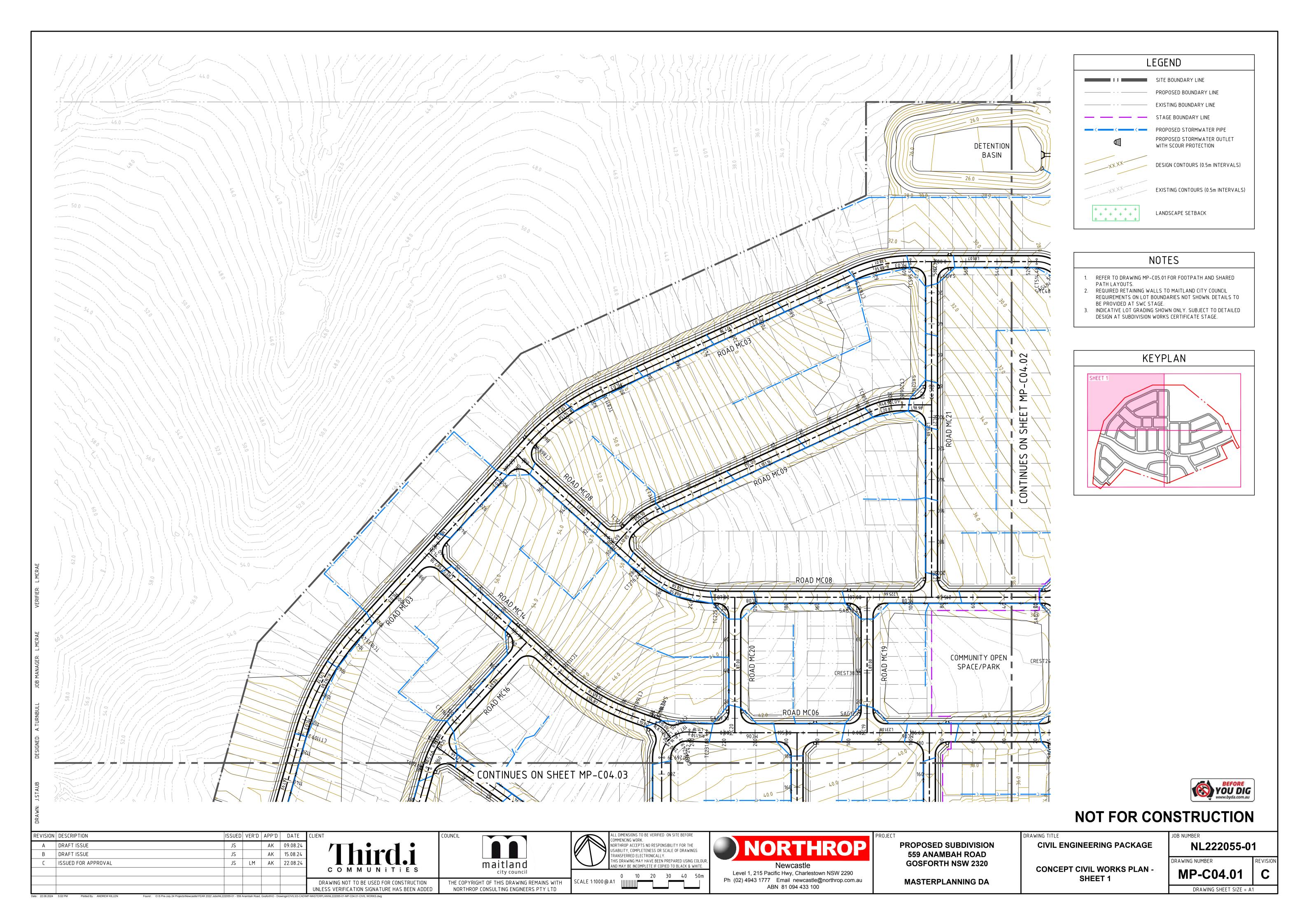
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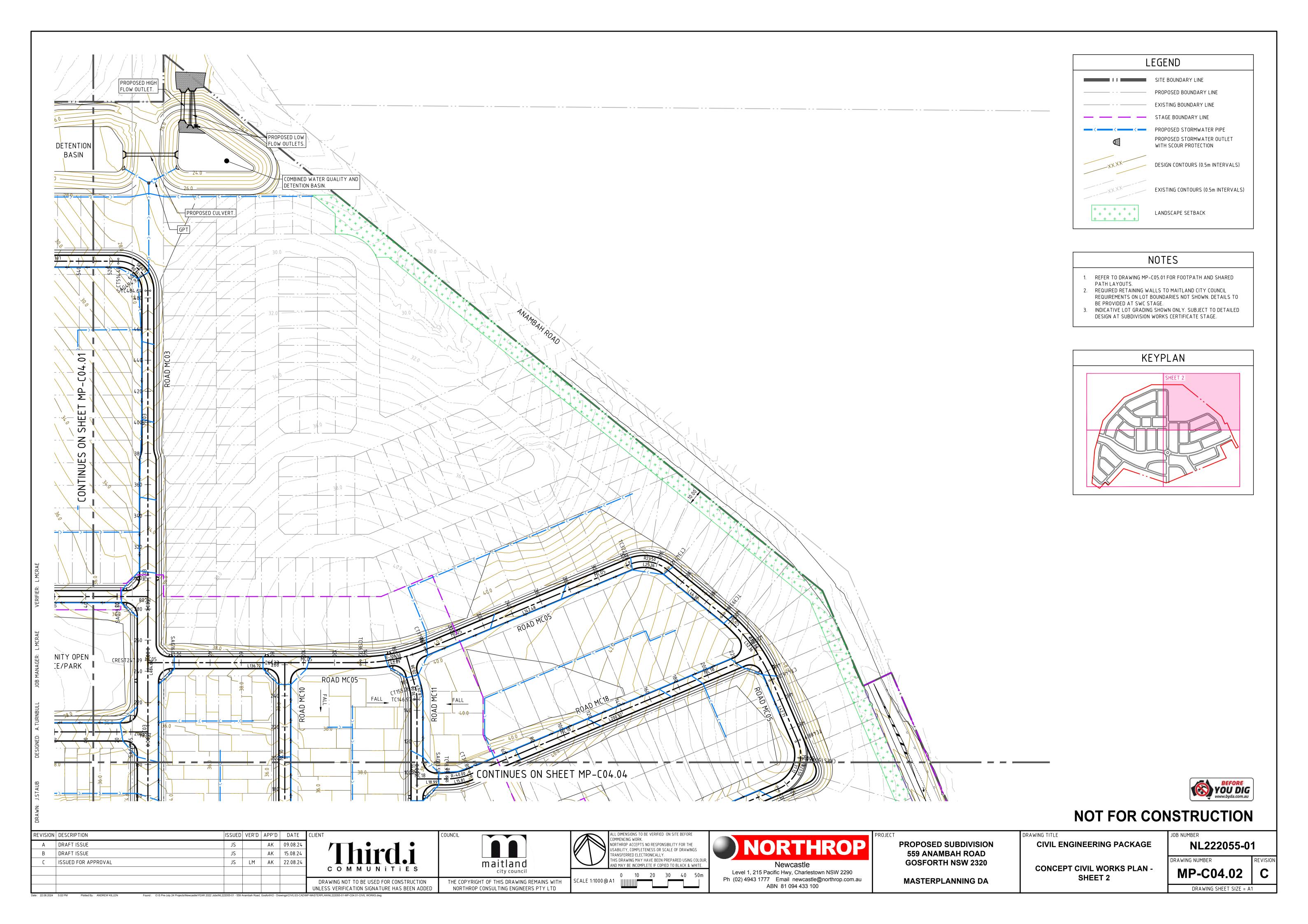
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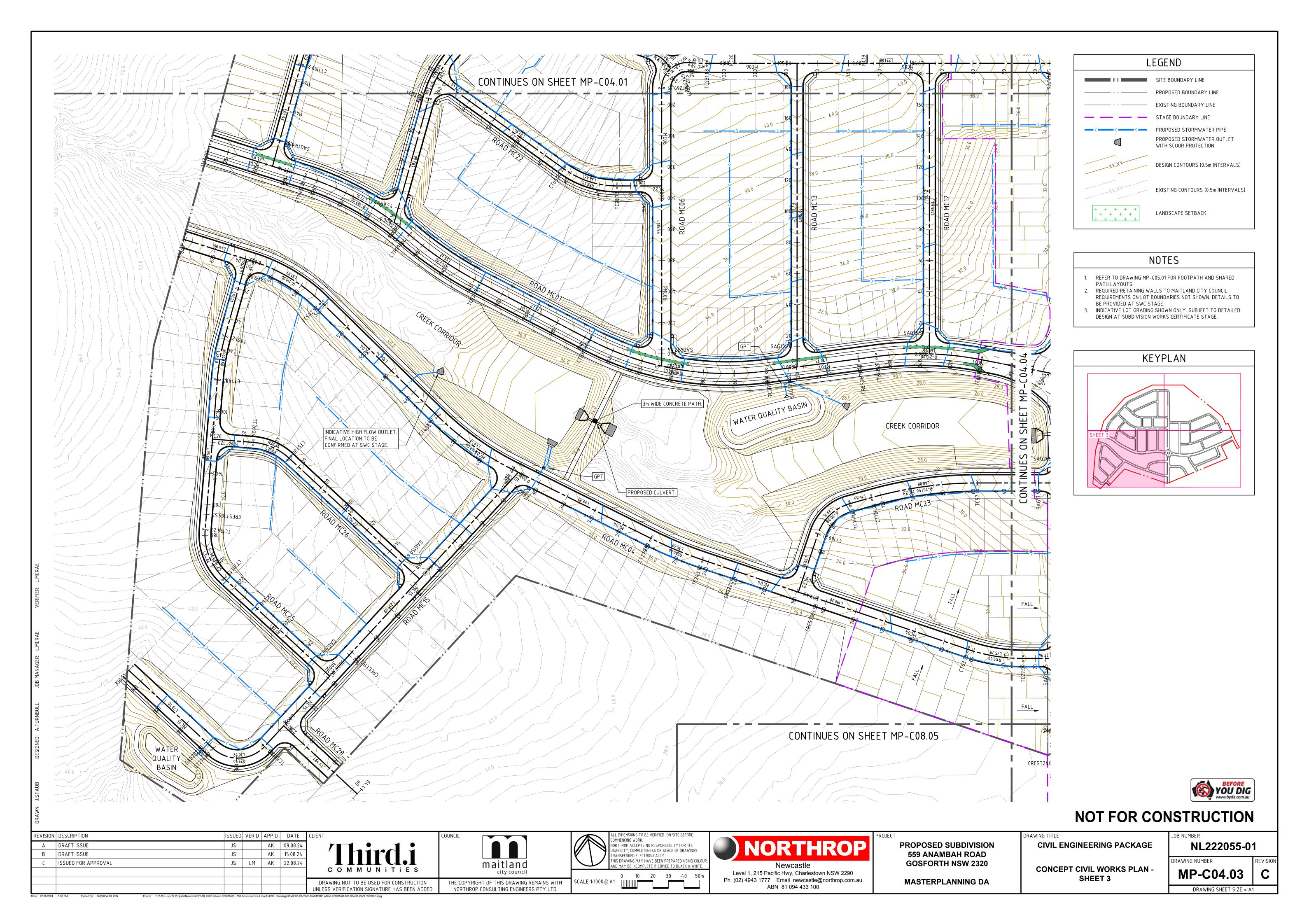


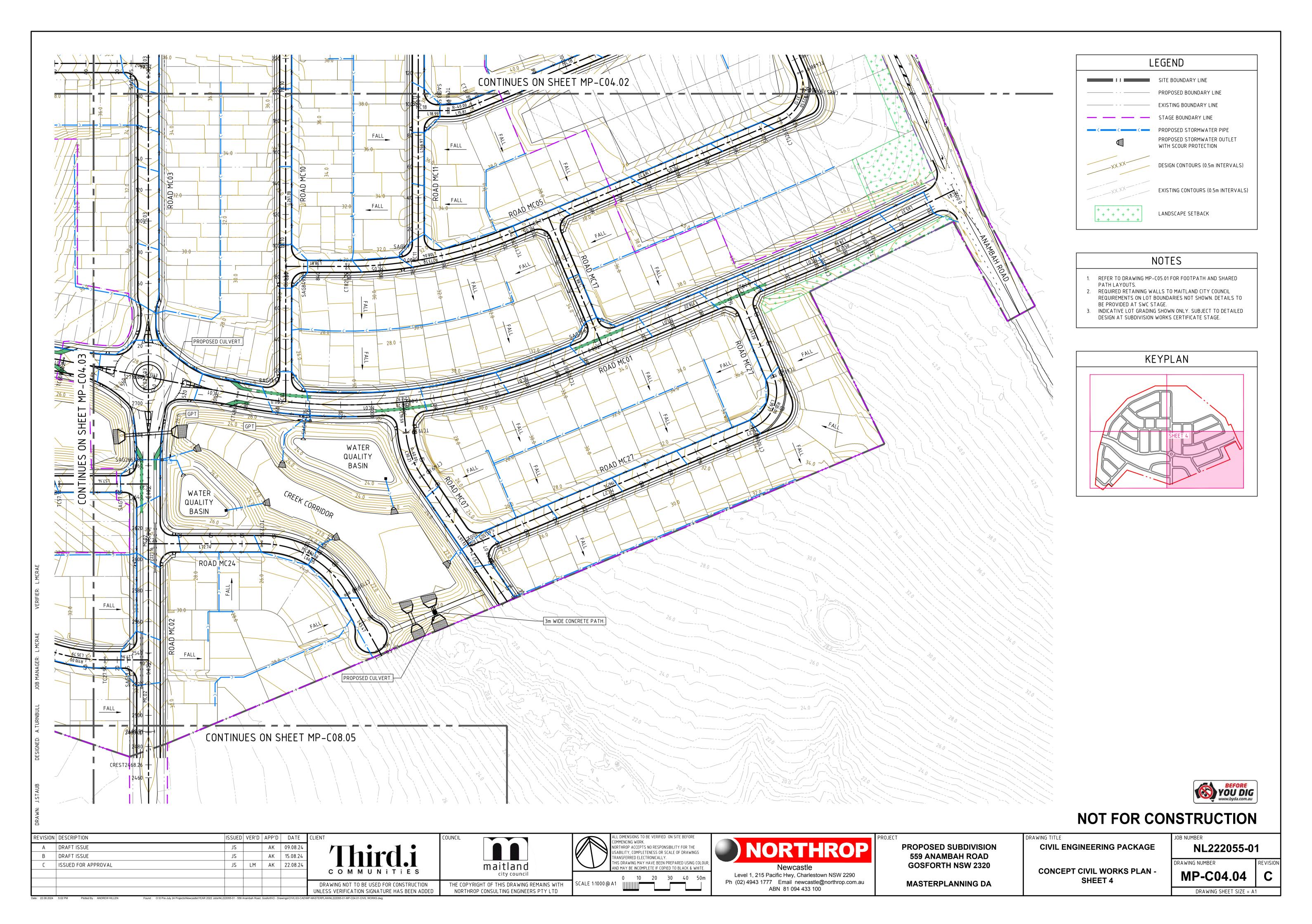
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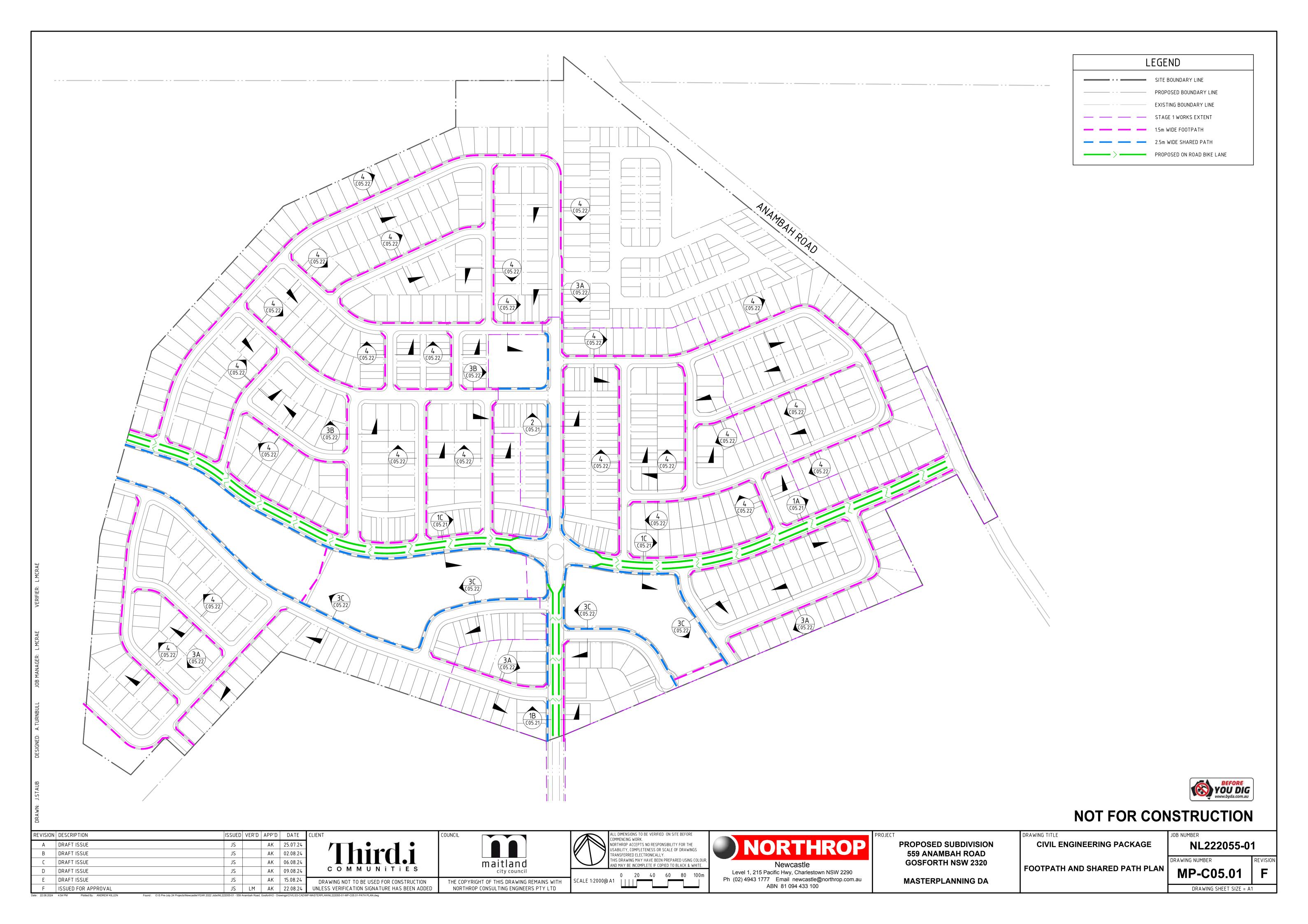
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		COMMUNITIES	maitland city council	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR, AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE. 0 10 20 30 40 50m	Newcastle Level 1, 215 Pacific Hwy, Charlestown NSW 2290	GOSFORTH NSW 2320	BULK EARTHWORKS SITE SECTIONS	MP-C03.13	REVISION REVISION
		DRAWING NOT TO BE USED FOR CONSTRUCTION UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED	THE COPYRIGHT OF THIS DRAWING REMAINS WITH NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:200@ A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au ABN 81 094 433 100	MASTERPLANNING DA	- SHEET 3	DRAWING SHEET SIZE = A1	1

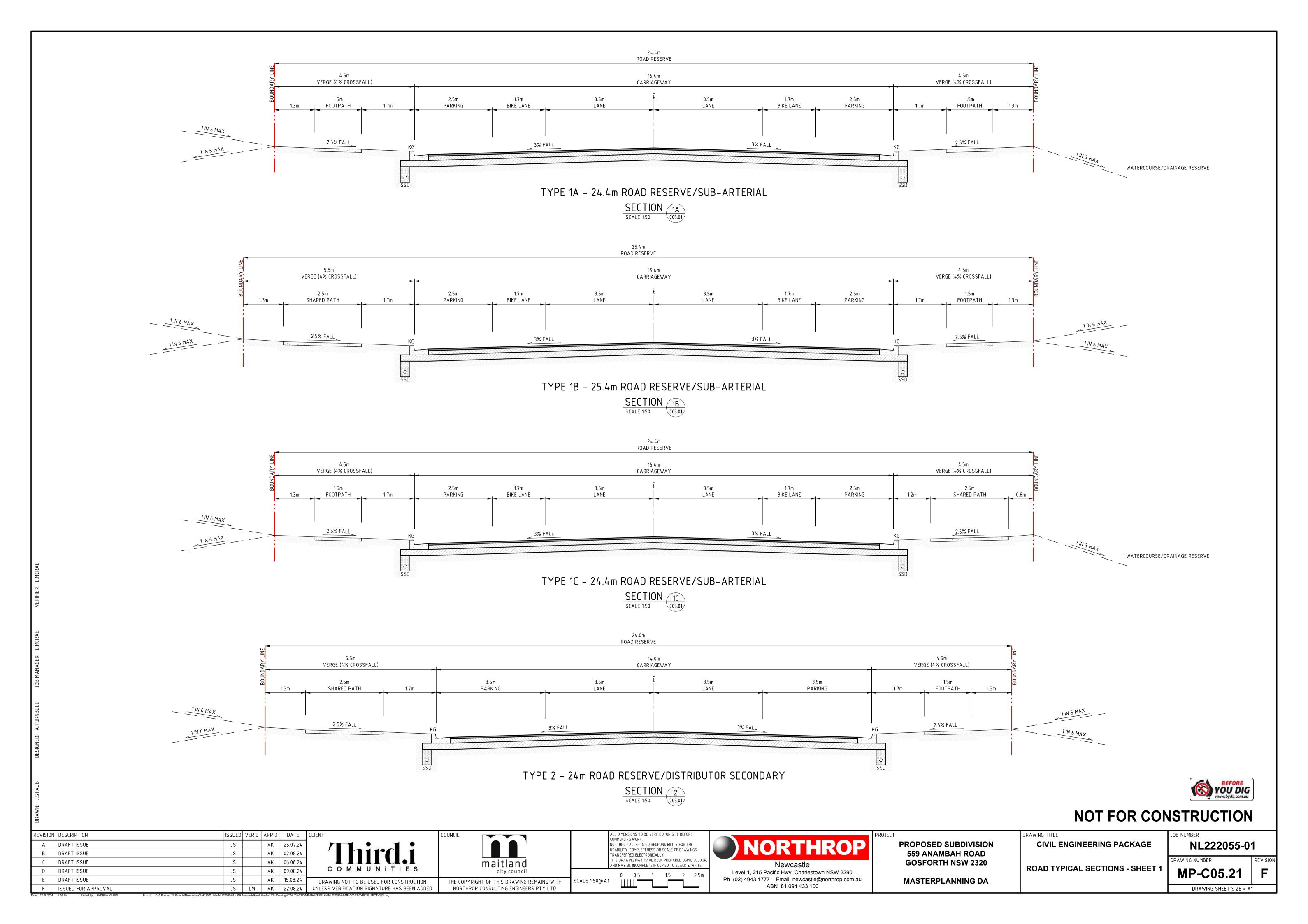












SCALE 1:50@ A1

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D DRAFT ISSUE

E DRAFT ISSUE

F ISSUED FOR APPROVAL

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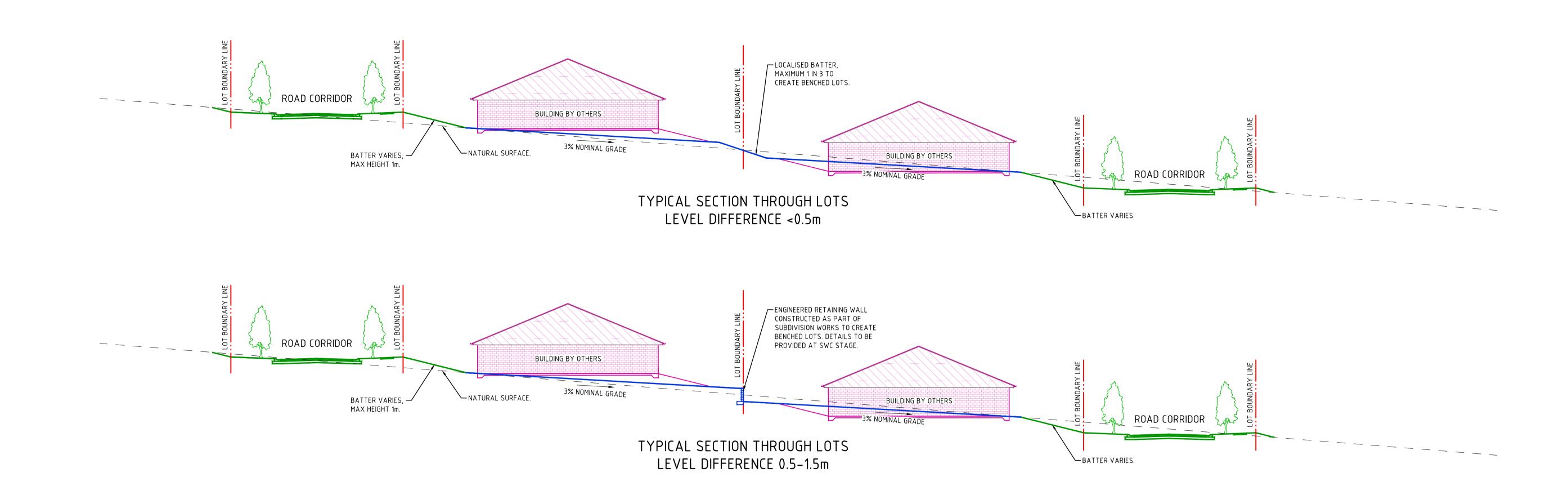
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MP-C05.22

ROAD TYPICAL SECTIONS - SHEET 2

MASTERPLANNING DA





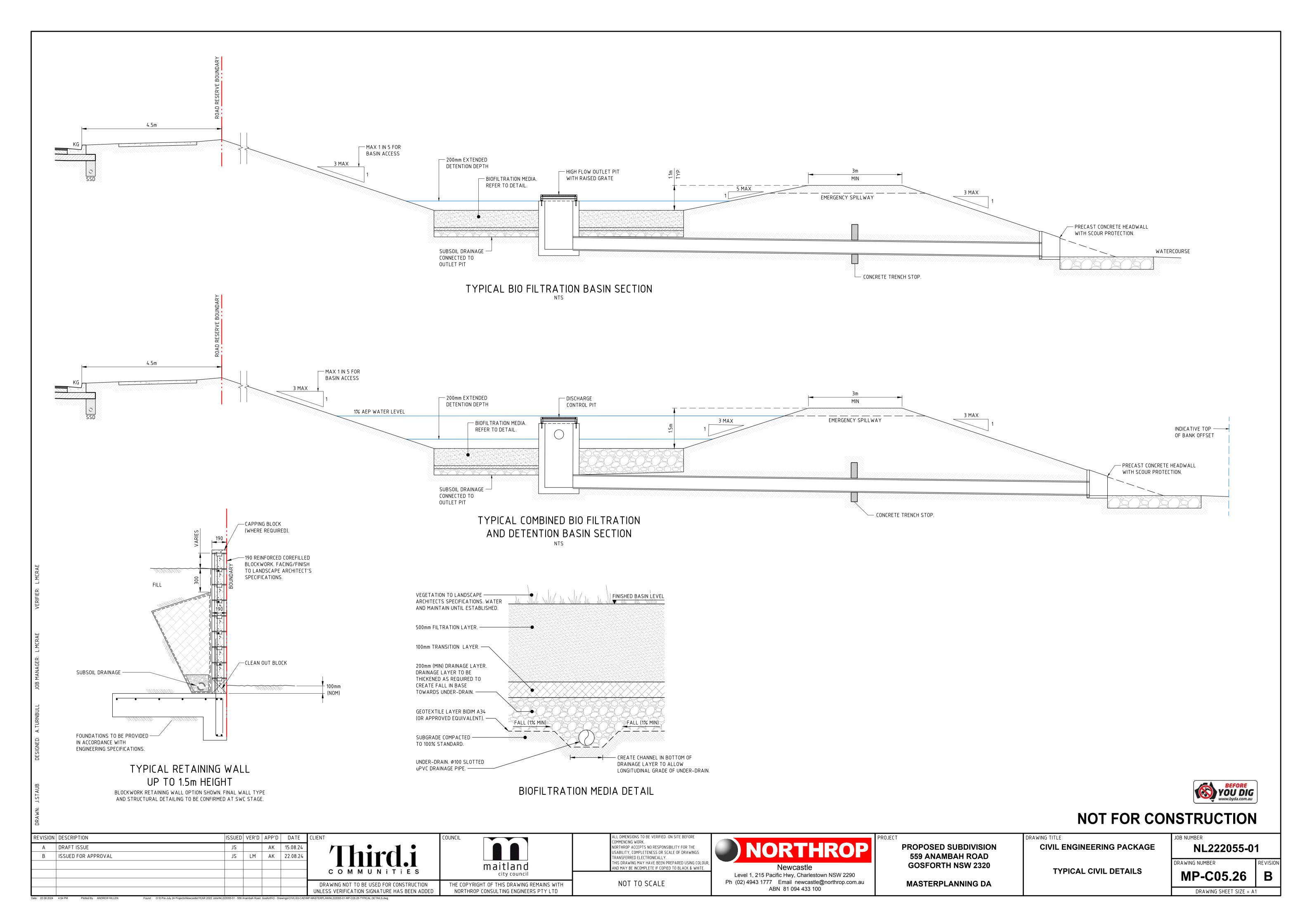
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MP-C05.25

DRAWING NUMBER

NL222055-01



REVISION DESCRIPTION

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ISSUED VER'D APP'D DATE

JS LM AK 22.08.24

JS

AK 09.08.24

AK 15.08.24

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VERTICAL SCALE 1:100@A1

Newcastle

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NL222055-01

DRAWING SHEET SIZE = A1

MP-C05.31

DRAWING NUMBER

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CIVIL ENGINEERING PACKAGE

ROAD LONGITUDINAL SECTIONS -

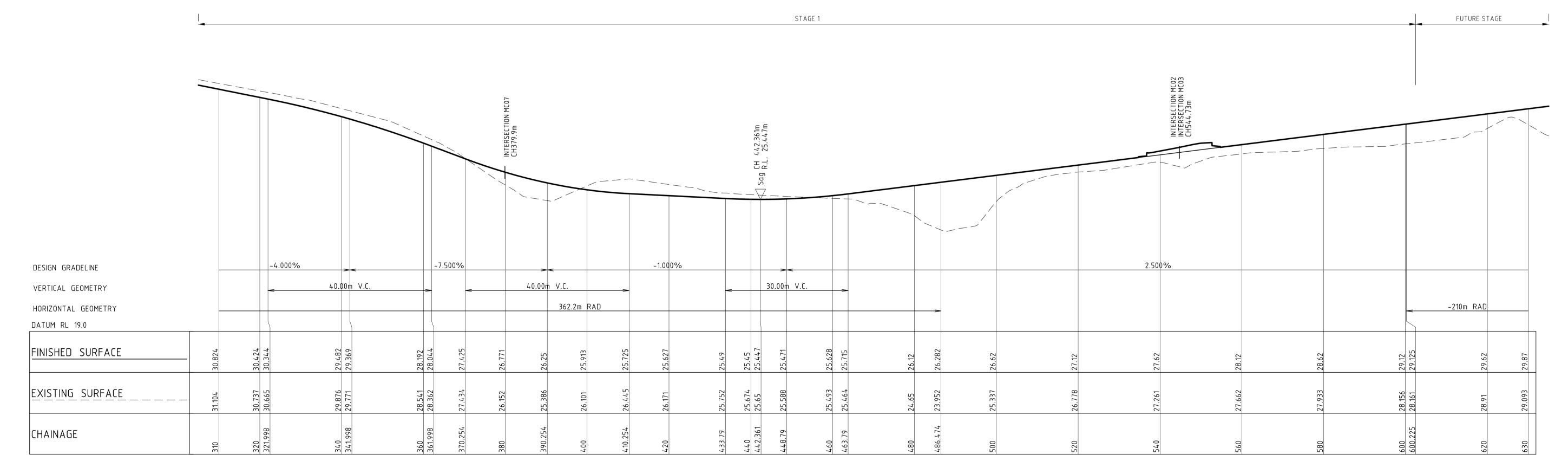
SHEET 1

PROPOSED SUBDIVISION

559 ANAMBAH ROAD

GOSFORTH NSW 2320

MASTERPLANNING DA



LONGITUDINAL SECTION ALONG MC01

HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1

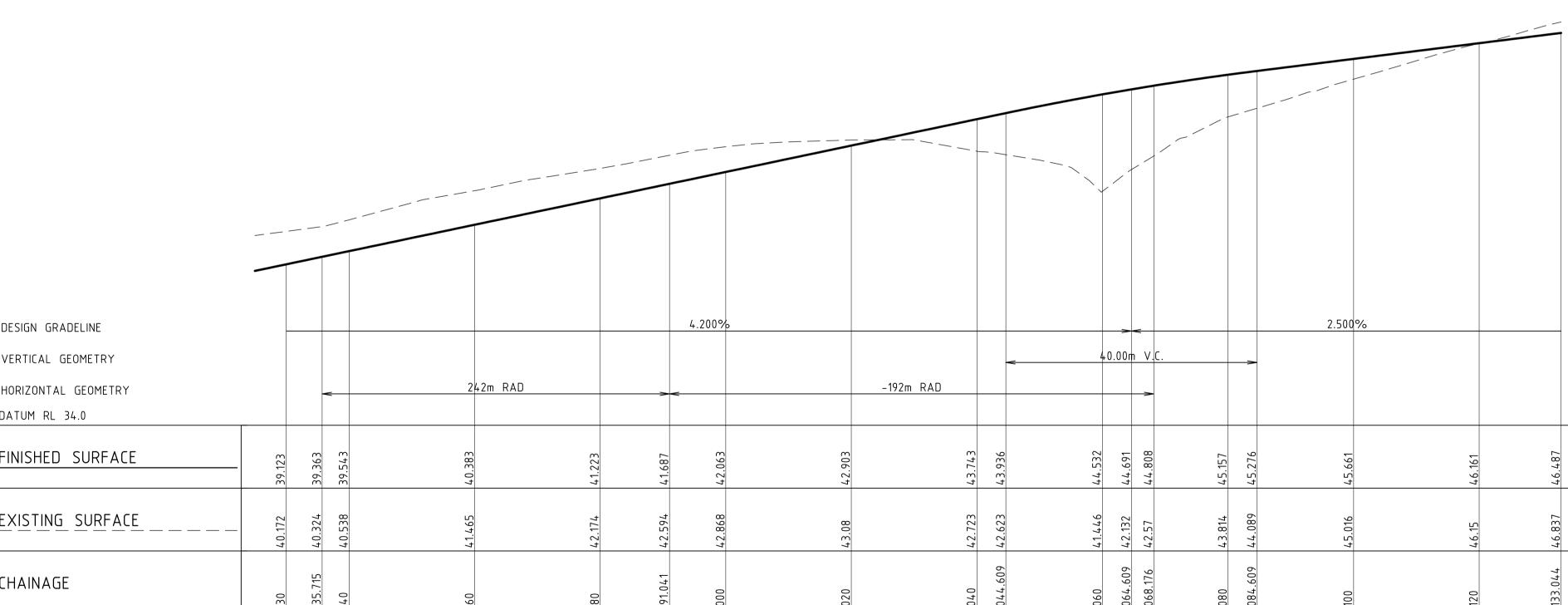


REVISION DESCRIPTION	ISSUED VER'D APP'D DATE CLIENT	COUNCIL	ALL DIMENSIONS TO BE VERIFIED ON SITE BEFORE		PROJECT	DRAWING TITLE	JOB NUMBER	
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C ISSUED FOR APPROVAL	JS LM AK 22.08.24	maitland	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR,	Newcastle	GOSFORTH NSW 2320		DRAWING NUMBER REV	√ISI0N
	COMMUNITIES	city council	0 5 10 15 20 25m	Level 1, 215 Pacific Hwy, Charlestown NSW 2290		ROAD LONGITUDINAL SECTIONS -	MP-C05.32 (C
	DRAWING NOT TO BE USED FOR CONSTRUCTION	THE COPYRIGHT OF THIS DRAWING REMAINS WITH	SCALE 1:500@ A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au	MASTERPLANNING DA	SHEET 2	WIF-CU3.32 C	
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Date: 22.08.2024 4:55 PM Plotted By: ANDREW KILLEN Found: 0:\5	Pre-July 24 Projects\Newcastle\YEAR 2022 Jobs\NL222055-01 - 559 Anambah Road, Gosforth\O - Drawings\CIVIL\03-CAD\MP-MASTERPLAN\NL222055-01-MP-C05.31-LONG SECTIONS.dwg	•						

LONGITUDINAL SECTION ALONG MC01 HORIZONTAL SCALE 1:500@A1 VERTICAL SCALE 1:100@A1



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С	ISSUED FOR APPROVAL	JS LM AK 22.08.24	COMMUNITIES	maitland city council	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR, AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE. 0 5 10 15 20 25m SCALE 1:500@ A1	Newcastle Level 1, 215 Pacific Hwy, Charlestown NSW 2290	GOSFORTH NSW 2320	ROAD LONGITUDINAL SECTIONS -	MP-C05.33	REVISION
			DRAWING NOT TO BE USED FOR CONSTRUCTION UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED	THE COPYRIGHT OF THIS DRAWING REMAINS WITH NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:100 @ A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au ABN 81 094 433 100	MASTERPLANNING DA	SHEET 3	DRAWING SHEET SIZE = A	



LONGITUDINAL SECTION ALONG MC01 HORIZONTAL SCALE 1:500@A1

FUTURE STAGE

VERTICAL SCALE 1:100@A1



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AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE. SCALE 1:100 @ A1



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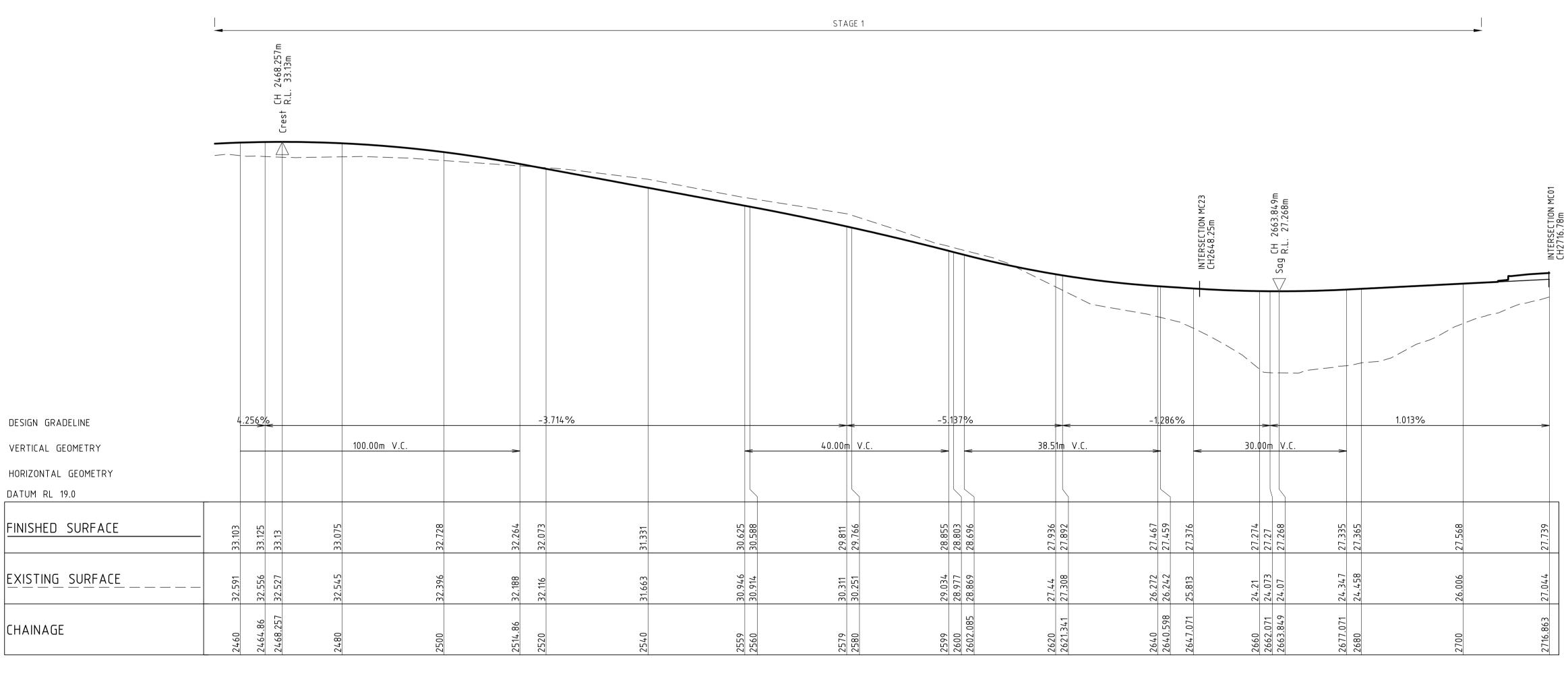
PROPOSED SUBDIVISION 559 ANAMBAH ROAD **GOSFORTH NSW 2320**

MASTERPLANNING DA

CIVIL ENGINEERING PACKAGE

ROAD LONGITUDINAL SECTIONS -SHEET 4

JOB NUMBER NL222055-0 °	 1
DRAWING NUMBER	REVI
MP-C05.34	(



LONGITUDINAL SECTION ALONG MC02
HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1



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REVISION	DESCRIPTION	ISSUED	VER'D	APP'D	DATE	CLI
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ABN 81 094 433 100

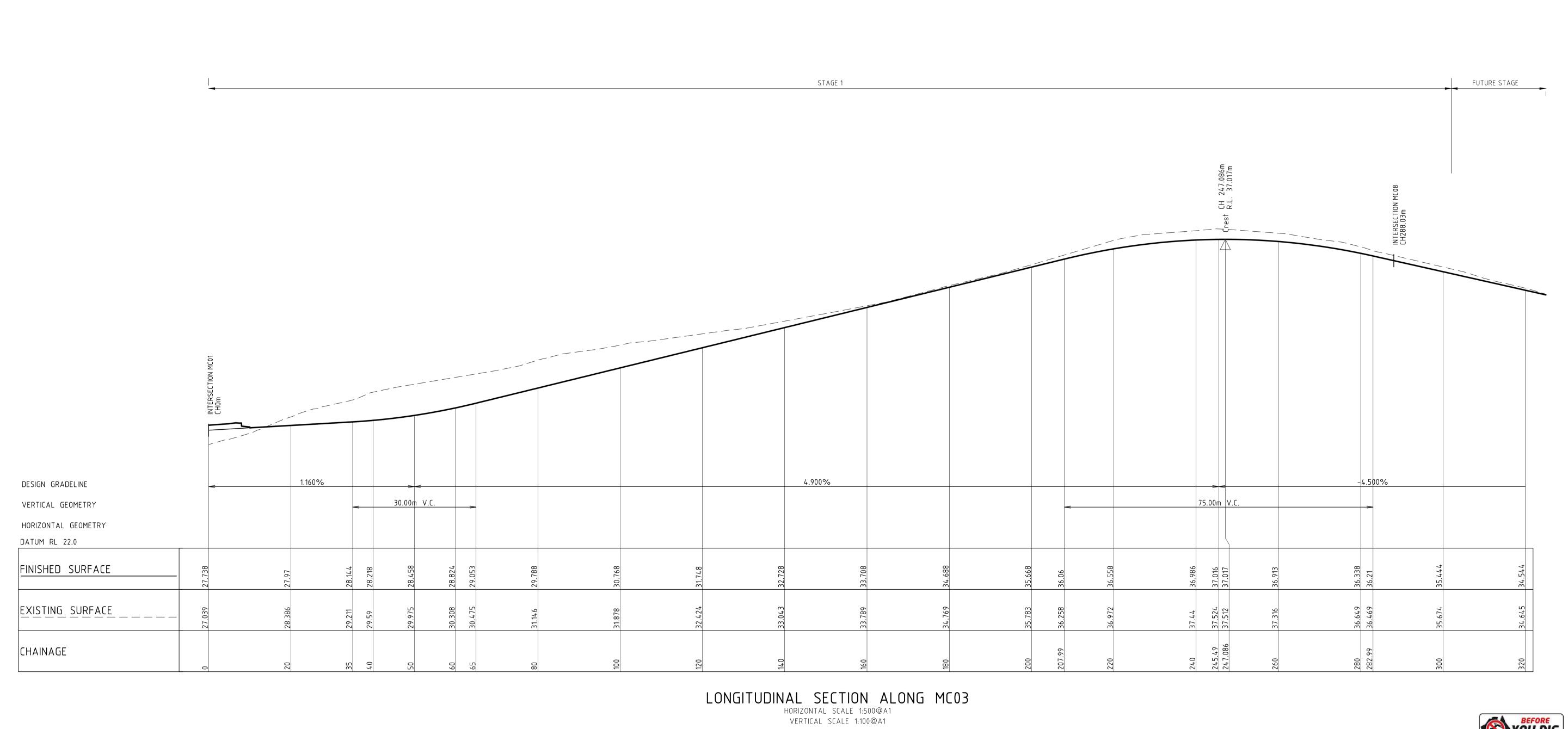
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PROPOSED SUBDIVISION 559 ANAMBAH ROAD **GOSFORTH NSW 2320**

CIVIL ENGINEERING PACKAGE

ROAD LONGITUDINAL SECTIONS -SHEET 5

NL222055-01 DRAWING NUMBER MP-C05.35 DRAWING SHEET SIZE = A1





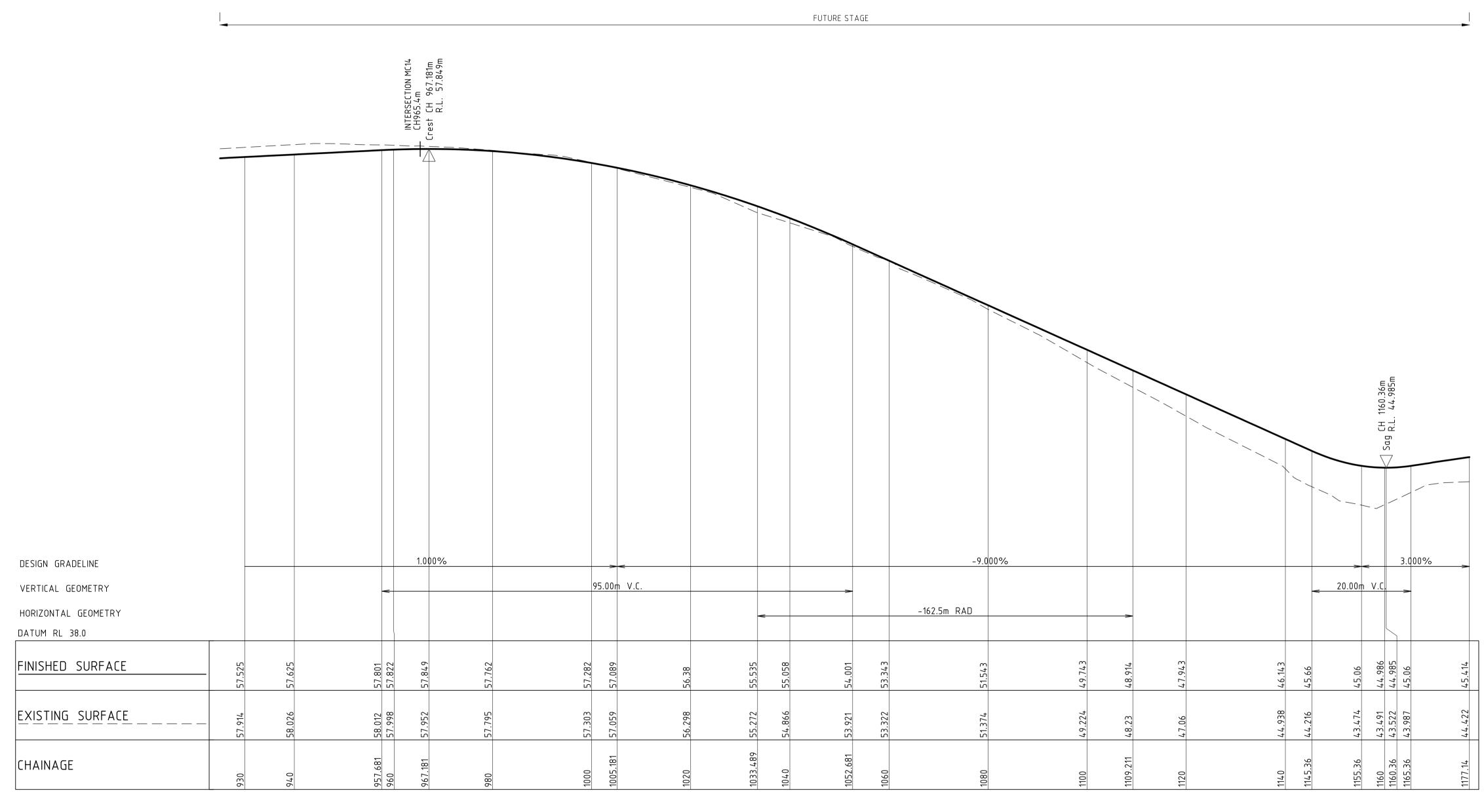
RE\	VISION DESCRIPTION ISSUED VER'D APP'D DATE	CLIENT	COUNCIL	ALL DIMENSIONS TO BE VERIFIED ON SITE BEFORE		PROJECT	DRAWING TITLE	JOB NUMBER
	A DRAFT ISSUE JS AK 09.08.2			COMMENCING WORK. NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE	NORTHROD	PROPOSED SUBDIVISION	CIVIL ENGINEERING PACKAGE	NL222055-01
	B DRAFT ISSUE JS AK 15.08.2	o in the second		TRANSFERRED ELECTRONICALLY.	MONTHINO	559 ANAMBAH ROAD		
	C ISSUED FOR APPROVAL JS LM AK 22.08.2		maitland	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR, AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE.	Newcastle	GOSFORTH NSW 2320	DOAD LONGITUDINAL OF OTIONS	DRAWING NUMBER REVISION
		COMMUNITIES	city council	SCALE 1.500@ A1 0 5 10 15 20 25m	Level 1, 215 Pacific Hwy, Charlestown NSW 2290		ROAD LONGITUDINAL SECTIONS -	MP-C05.36 C
		DRAWING NOT TO BE USED FOR CONSTRUCTION	THE COPYRIGHT OF THIS DRAWING REMAINS WITH	- SCALE 1:000@A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au	MASTERPLANNING DA	SHEET 6	1111 333.33
		UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED	NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:100 @ A1 0 1 2 3 4 5m	ABN 81 094 433 100			DRAWING SHEET SIZE = A1

LONGITUDINAL SECTION ALONG MC03 HORIZONTAL SCALE 1:500@A1 VERTICAL SCALE 1:100@A1



REVISION DESCRIPTION	ISSUED VER'D APP'D DATE CLIENT		COUNCIL	ALL DIMENSIONS TO BE VERIFIED ON SITE BEFORE		PROJECT	DRAWING TITLE	JOB NUMBER	
A DRAFT ISSUE	JS AK 09.08.24			COMMENCING WORK. NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE	NOPTHROD	PROPOSED SUBDIVISION	CIVIL ENGINEERING PACKAGE	NL222055-0 ²	1
B DRAFT ISSUE	JS AK 15.08.24	' I M1rA 1		TRANSFERRED ELECTRONICALLY.	NONTINOF	559 ANAMBAH ROAD			
C ISSUED FOR APPROVAL	JS LM AK 22.08.24		maitland	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR,	Newcastle	GOSFORTH NSW 2320		DRAWING NUMBER	REVISION
		COMMUNITIES	city council	0 5 10 15 20 25m	Level 1, 215 Pacific Hwy, Charlestown NSW 2290		ROAD LONGITUDINAL SECTIONS -	MP-C05.37	
	DR.	AWING NOT TO BE USED FOR CONSTRUCTION	THE COPYRIGHT OF THIS DRAWING REMAINS WITH	SCALE 1:500@ A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au	MASTERPLANNING DA	SHEET 7		
		SS VERIFICATION SIGNATURE HAS BEEN ADDED	NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:100 @ A1 0 1 2 3 4 5m	ABN 81 094 433 100			DRAWING SHEET SIZE = A1	,1
Date: 22.08.2024 4:55 PM Plotted By: ANDREW KILLEN Found: 0:15 Pre-July 2	y 24 Projects\Newcastle\YEAR 2022 Jobs\NL222055-01 - 559 Anambah Road, Gosforth\O - Drawings\CIVIL\03-CAD\MP-MASTERPLAT	ANINL222055-01-MP-C05.31-LONG SECTIONS.dwg		-					

REVISI0	DESCRIPTION ISSUED VER'D APP'D DATE CLIENT	COUNCIL	ALL DIMENSIONS TO BE VERIFIED ON SITE BEFORE		PROJECT	DRAWING TITLE	JOB NUMBER
Α	DRAFT ISSUE JS AK 09.08.24		NORTHEN ACCEPTS NO RESPONSIBILITY FOR THE	NORTHROD	PROPOSED SUBDIVISION	CIVIL ENGINEERING PACKAGE	NL222055-01
В	DRAFT ISSUE JS AK 15.08.24		TRANSFERRED ELECTRONICALLY.		559 ANAMBAH ROAD		
С	ISSUED FOR APPROVAL JS LM AK 22.08.24	maitland	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR, AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE.	Newcastle	GOSFORTH NSW 2320	BOAR LONGITURINAL SECTIONS	DRAWING NUMBER REVISION
	COMMUNITIES	city council	SCALE 1500@ A1 0 5 10 15 20 25m	Level 1, 215 Pacific Hwy, Charlestown NSW 2290		ROAD LONGITUDINAL SECTIONS -	MP-C05.38 C
	DRAWING NOT TO BE USED FOR CONSTRUCTION	THE COPYRIGHT OF THIS DRAWING REMAINS WITH	SCALE 1.500@ A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au	MASTERPLANNING DA	SHEET 8	333.00
	UNLESS VERIFICATION SIGNATURE HAS BEEN AN	DED NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:100 @ A1 0 1 2 3 4 5m	ABN 81 094 433 100			DRAWING SHEET SIZE = A1



LONGITUDINAL SECTION ALONG MC03
HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1



NOT FOR CONSTRUCTION

REVISION	DESCRIPTION	IZZOFD	AFK,D	APP'U	DATE	LL
Α	DRAFT ISSUE	JS		AK	09.08.24	
В	DRAFT ISSUE	JS		AK	15.08.24	
С	ISSUED FOR APPROVAL	JS	LM	AK	22.08.24	

DRAWING NOT TO BE USED FOR CONSTRUCTION UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED





ABN 81 094 433 100

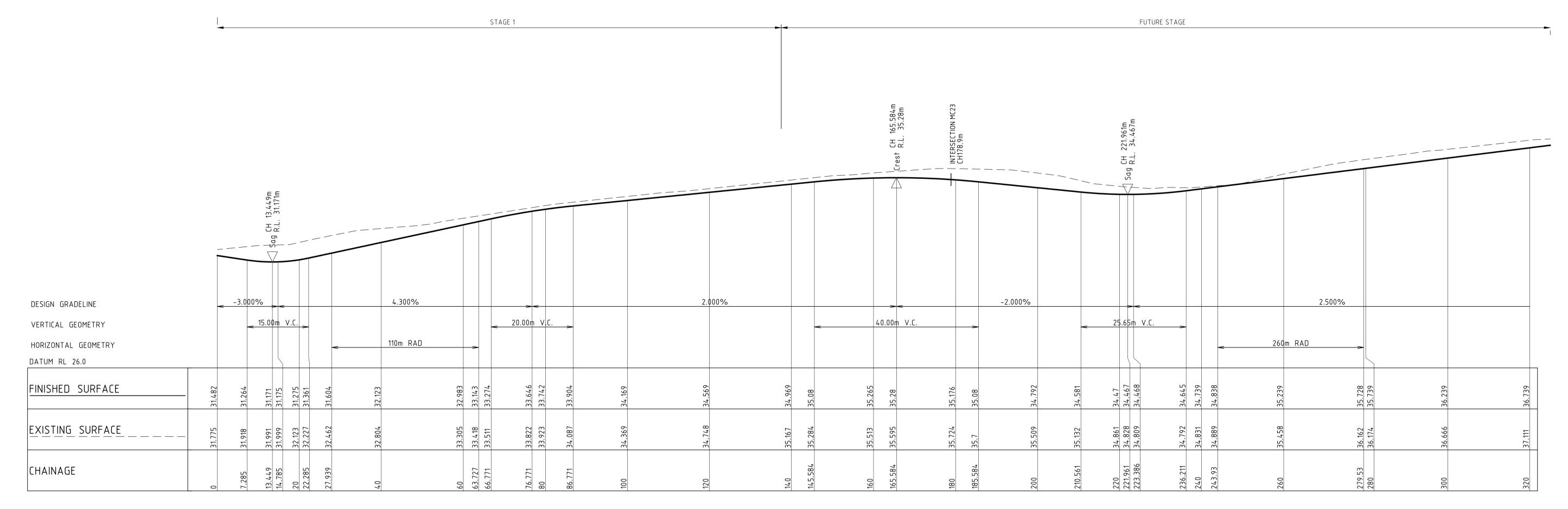
PROPOSED SUBDIVISION 559 ANAMBAH ROAD GOSFORTH NSW 2320

MASTERPLANNING DA

CIVIL ENGINEERING PACKAGE

ROAD LONGITUDINAL SECTIONS -SHEET 9

JOB NUMBER	
NL222055-0 ⁻	1
DRAWING NUMBER	REVI
MP-C05.39	



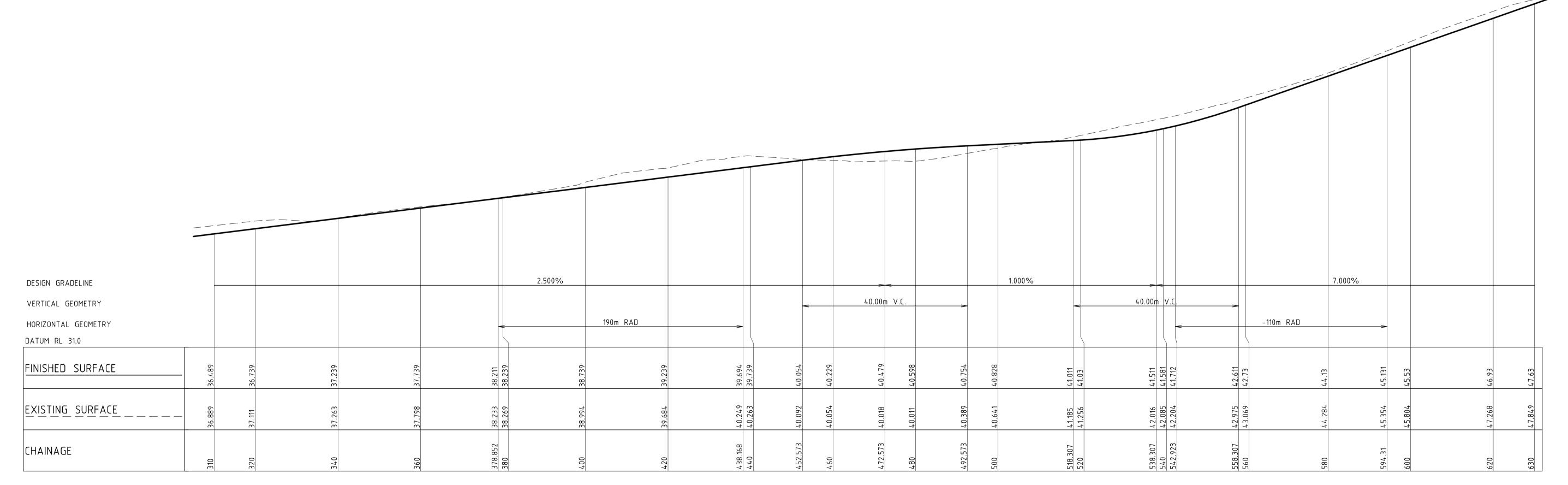
LONGITUDINAL SECTION ALONG MC04 HORIZONTAL SCALE 1:500@A1 VERTICAL SCALE 1:100@A1



REVISI	N DESCRIPTION	ISSUED	VER'D APP'D DATE	CLIENT	COUNCIL	ALL DIMENSIONS TO BE VERIFIED ON SITE BEFORE		PROJECT	DRAWING TITLE	JOB NUMBER	
А	DRAFT ISSUE	JS	AK 09.08.24			NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE	NOPTHROP	PROPOSED SUBDIVISION	CIVIL ENGINEERING PACKAGE	NL222055-01	1
В	DRAFT ISSUE	JS	AK 15.08.24	'		TRANSFERRED ELECTRONICALLY.	NONTINOF	559 ANAMBAH ROAD			
С	ISSUED FOR APPROVAL	JS	LM AK 22.08.24	111114.1	maitland	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR, AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE.	Newcastle	GOSFORTH NSW 2320		DRAWING NUMBER	REVISION
				COMMUNITIES	city council	CCALE 1 F 0 0 5 10 15 20 25 m	Level 1, 215 Pacific Hwy, Charlestown NSW 2290		ROAD LONGITUDINAL SECTIONS -	MP-C05.40	C
				DRAWING NOT TO BE USED FOR CONSTRUCTION	THE COPYRIGHT OF THIS DRAWING REMAINS WITH	SCALE 1:500@ A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au	MASTERPLANNING DA	SHEET 10	WII 303.40	
				UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED	NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:100 @ A1 0 1 2 3 4 5m	ABN 81 094 433 100			DRAWING SHEET SIZE = A1	1

LONGITUDINAL SECTION ALONG MC04 HORIZONTAL SCALE 1:500@A1 VERTICAL SCALE 1:100@A1

FUTURE STAGE



LONGITUDINAL SECTION ALONG MC04 HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1



NOT FOR CONSTRUCTION

REVISION	DESCRIPTION	ISSUED	VER'D	APP'D	DATE
Α	DRAFT ISSUE	JS		AK	09.08.24
В	DRAFT ISSUE	JS		AK	15.08.24
С	ISSUED FOR APPROVAL	JS	LM	AK	22.08.24

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UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED

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PROPOSED SUBDIVISION 559 ANAMBAH ROAD **GOSFORTH NSW 2320**

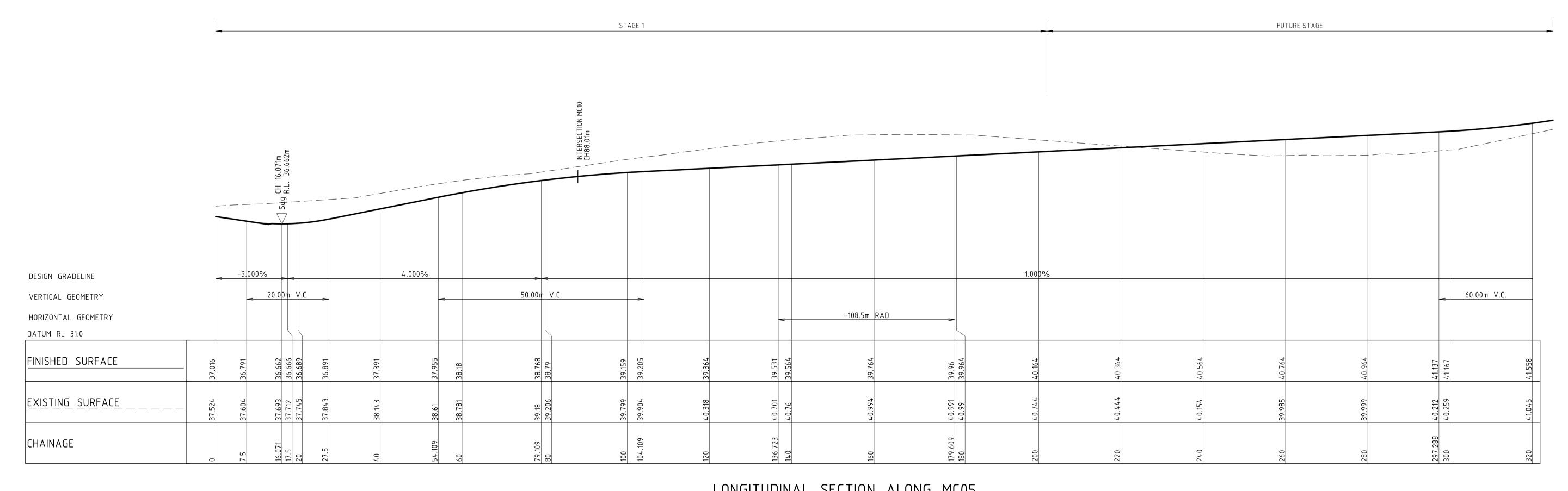
MASTERPLANNING DA

CIVIL ENGINEERING PACKAGE

SHEET 11

NL222055-01 DRAWING NUMBER **ROAD LONGITUDINAL SECTIONS -**

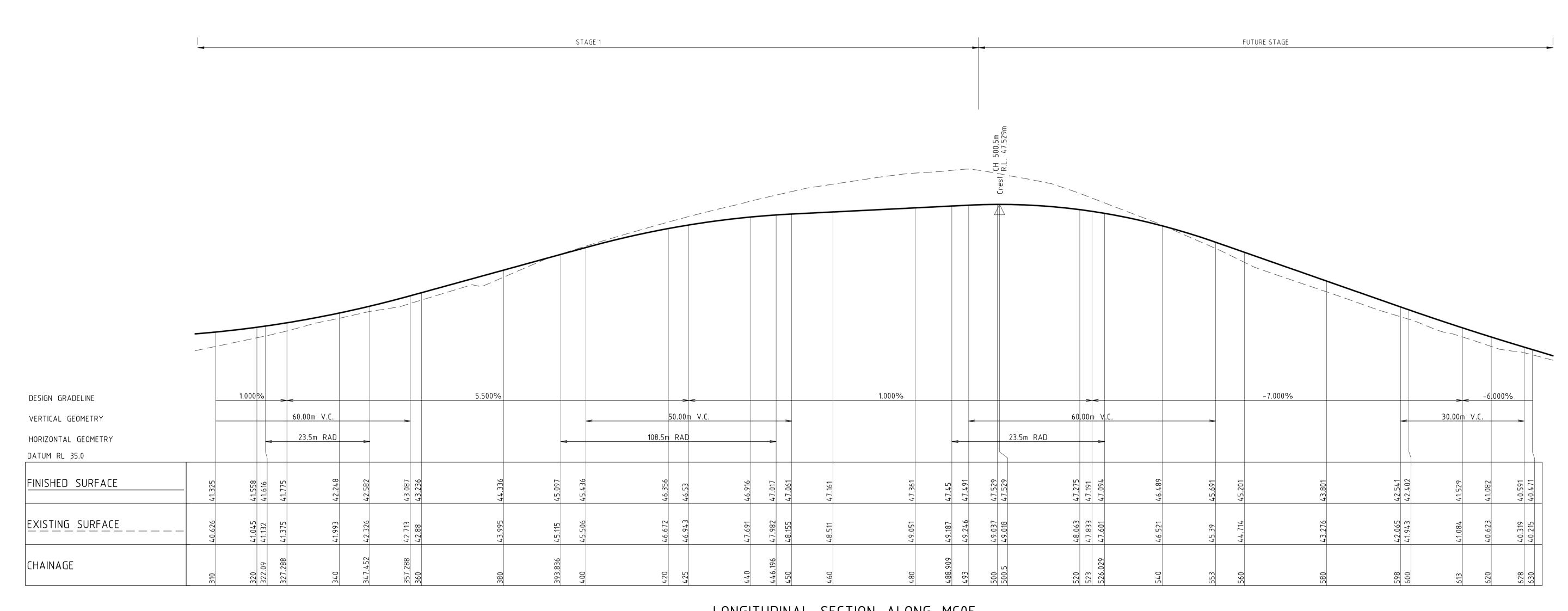
MP-C05.41 DRAWING SHEET SIZE = A1



LONGITUDINAL SECTION ALONG MC05 HORIZONTAL SCALE 1:500@A1 VERTICAL SCALE 1:100@A1



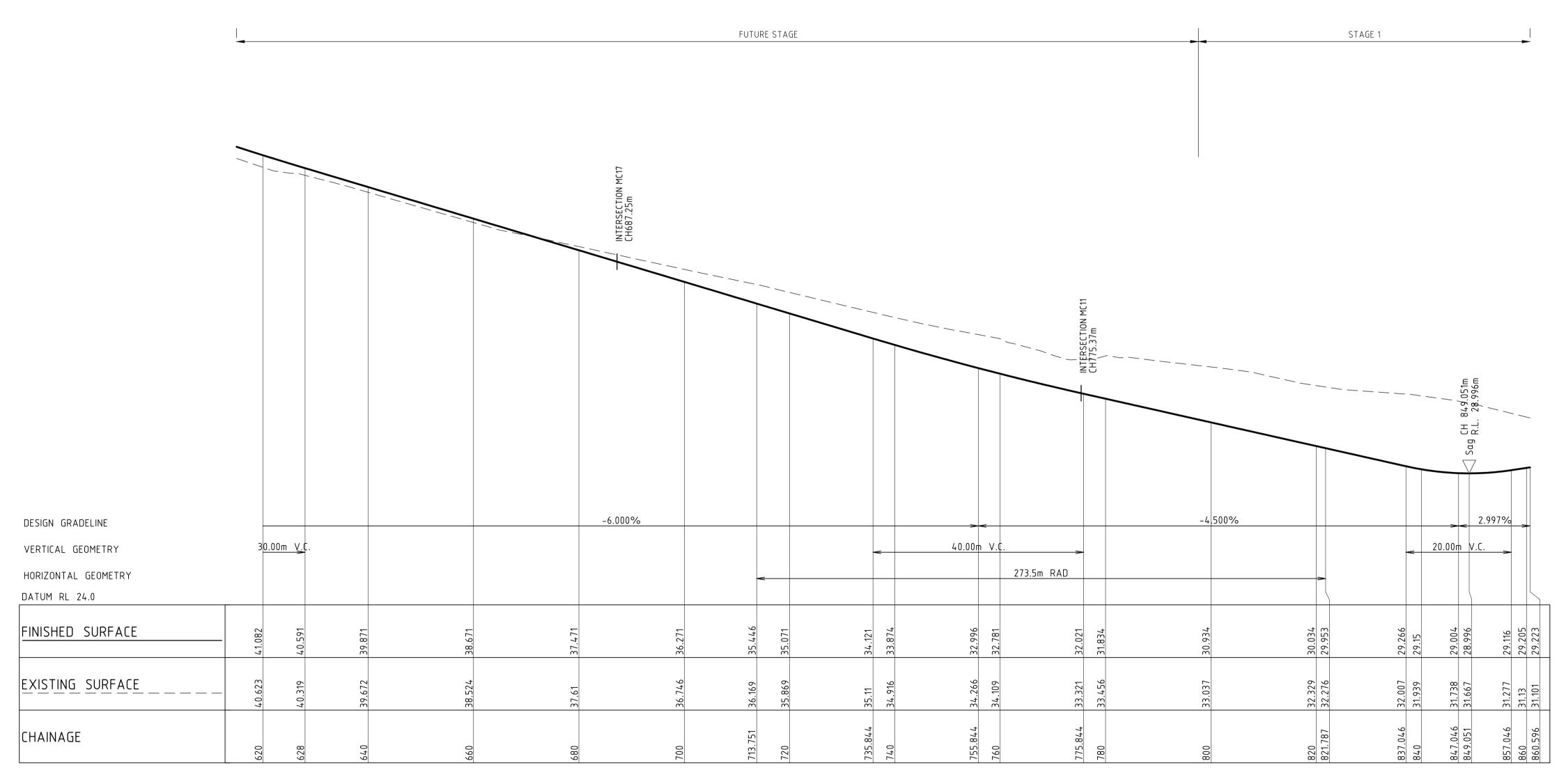
REVISI A	ON DESCRIPTION DRAFT ISSUE	ISSUED VER'D APP'D DATE JS AK 09.08.24	CLIENT	COUNCIL	ALL DIMENSIONS TO BE VERIFIED ON SITE BEFORE COMMENCING WORK. NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE USABILITY COMPLETENESS OF SCALE OF DRAWINGS.	NORTHROP	PROJECT PROPOSED SUBDIVISION	DRAWING TITLE CIVIL ENGINEERING PACKAGE	JOB NUMBER NL222055-0°	 1
С	DRAFT ISSUE ISSUED FOR APPROVAL	JS AK 15.08.24 JS LM AK 22.08.24	COMMUNITIES	maitland city council	TRANSFERRED ELECTRONICALLY. THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR, AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE. SCALE 1.500@ A1	Newcastle Level 1, 215 Pacific Hwy, Charlestown NSW 2290	559 ANAMBAH ROAD GOSFORTH NSW 2320	ROAD LONGITUDINAL SECTIONS -	DRAWING NUMBER MP-C05.42	REVISIO
D-t 22.00 f			DRAWING NOT TO BE USED FOR CONSTRUCTION UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED	THE COPYRIGHT OF THIS DRAWING REMAINS WITH NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:100 @ A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au ABN 81 094 433 100	MASTERPLANNING DA	SHEET 12	DRAWING SHEET SIZE = A1	.1



LONGITUDINAL SECTION ALONG MC05 HORIZONTAL SCALE 1:500@A1 VERTICAL SCALE 1:100@A1

YOU DIG www.byda.com.au

REVISION DESCRIPTION ISS	SUED VER'D APP'D DATE	CLIENT	COUNCIL	ALL DIMENSIONS TO BE VERIFIED ON SITE BEFORE COMMENCING WORK.		PROJECT	DRAWING TITLE	JOB NUMBER	,
A DRAFT ISSUE J	JS AK 09.08.24			NORTHROW ACCEPTS NO RESPONSIBILITY FOR THE		PROPOSED SUBDIVISION	CIVIL ENGINEERING PACKAGE	NL222055-01	
B DRAFT ISSUE J	JS AK 15.08.24] 'I H1ra 1		TRANSFERRED ELECTRONICALLY.	MONTHINOP	559 ANAMBAH ROAD			
C ISSUED FOR APPROVAL J	JS LM AK 22.08.24		maitland	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR, AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE.	Newcastle	GOSFORTH NSW 2320		DRAWING NUMBER RE	EVISION
		COMMUNITIES	city council	SCALE 1500@A1 0 5 10 15 20 25m	Level 1, 215 Pacific Hwy, Charlestown NSW 2290		ROAD LONGITUDINAL SECTIONS -	MP-C05.43	C
		DRAWING NOT TO BE USED FOR CONSTRUCTION	THE COPYRIGHT OF THIS DRAWING REMAINS WITH	SCALE 1:500@ A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au	MASTERPLANNING DA	SHEET 13	1111 000.40	
		UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED	NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:100 @ A1 0 1 2 3 4 5m	ABN 81 094 433 100			DRAWING SHEET SIZE = A1	



LONGITUDINAL SECTION ALONG MC05
HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1



DRAWING SHEET SIZE = A1

NOT FOR CONSTRUCTION

REVISION	DESCRIPTION	ISSUED	VER'D	APP'D	DATE	CLIEN
Α	DRAFT ISSUE	JS		AK	09.08.24	
В	DRAFT ISSUE	JS		AK	15.08.24	
С	ISSUED FOR APPROVAL	JS	LM	AK	22.08.24	
						[

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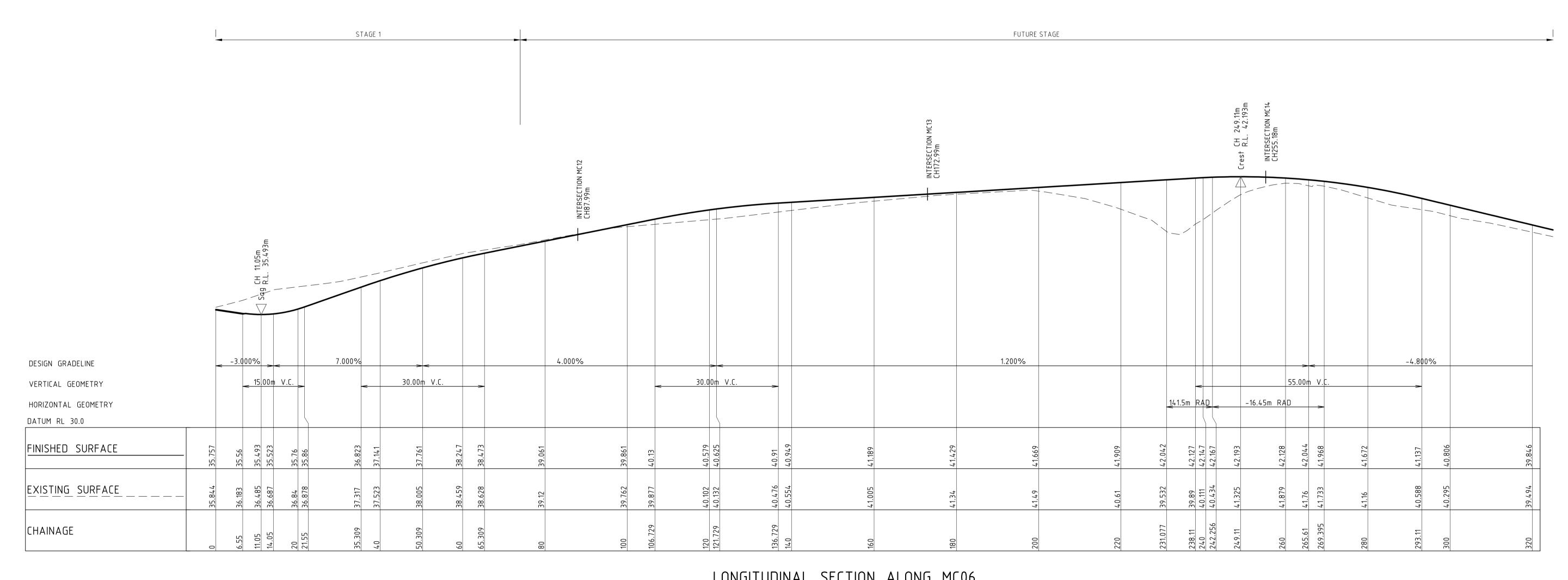
ABN 81 094 433 100

PROPOSED SUBDIVISION 559 ANAMBAH ROAD **GOSFORTH NSW 2320**

MASTERPLANNING DA

CIVIL ENGINEERING PACKAGE

NL222055-01 DRAWING NUMBER **ROAD LONGITUDINAL SECTIONS -**MP-C05.44 SHEET 14



LONGITUDINAL SECTION ALONG MC06 HORIZONTAL SCALE 1:500@A1 VERTICAL SCALE 1:100@A1



REVISI	ON DESCRIPTION	ISSUED VER'D APP'D DATE	CLIENT	COUNCIL	ALL DIMENSIONS TO BE VERIFIED ON SITE BEFORE		PROJECT	DRAWING TITLE	JOB NUMBER
А	DRAFT ISSUE	JS AK 09.08.24			COMMENCING WORK. NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE	NORTHROD	PROPOSED SUBDIVISION	CIVIL ENGINEERING PACKAGE	NL222055-01
В	DRAFT ISSUE	JS AK 15.08.24	i 'i mira i		TRANSFERRED ELECTRONICALLY.		559 ANAMBAH ROAD		
С	ISSUED FOR APPROVAL	JS LM AK 22.08.24		maitland	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR, AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE	Newcastle	GOSFORTH NSW 2320		DRAWING NUMBER REVISION
			COMMUNITIES	city council	0 5 10 15 20 25m	Level 1, 215 Pacific Hwy, Charlestown NSW 2290		ROAD LONGITUDINAL SECTIONS -	MP-C05.45 C
			DRAWING NOT TO BE USED FOR CONSTRUCTION	THE COPYRIGHT OF THIS DRAWING REMAINS WITH	SCALE 1:500@ A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au	MASTERPLANNING DA	SHEET 15	WII -003.43 0
			UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED	NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:100 @ A1 0 1 2 3 4 5m	ABN 81 094 433 100			DRAWING SHEET SIZE = A1
Date: 22.08.2	024 4:55 PM Plotted By: ANDREW KILLEN	Found: O:\5 Pre-July 24 Projects\Newcastle\YEAR 2022 Jobs\NL222055-01 - 559 Anambah Road, Gosforth\O - Drawings\CIVIL\03-CA	ADIMP-MASTERPLANINL222055-01-MP-C05.31-LONG SECTIONS.dwg						



ISSUED VER'D APP'D DATE CLIENT

castle /, Charlestown NSW 2290 newcastle@northrop.com.au 094 433 100

PROPOSED SUBDIVISION 559 ANAMBAH ROAD **GOSFORTH NSW 2320**

MASTERPLANNING DA

CIVIL ENGINEERING PACKAGE

ROAD LONGITUDINAL SECTIONS -SHEET 16

<i></i>		
	JOB NUMBER	
	NL222055-01	
	DRAWING NUMBER	F
-	MP-C05.46	

DRAWING SHEET SIZE = A1

			INTERSECTION MC CH332.19m								/ CH 437.443m pag R.L. 33.788m	INTERSECTION MC01 CH447.95m
DESIGN GRADELINE	_			-4.800%			><	-7.000%		>	1.957	1%
VERTICAL GEOMETRY HORIZONTAL GEOMETRY DATUM RL 29.0						<	30.00m V.C.	>		15.00m	V.C.	
FINISHED SURFACE	40.326	39.846	38.886	37.926	36.966	36.742	35.939	34.599	34.198	33.841	33.788	33.962
EXISTING SURFACE	39.927	39.494	38.581	37.828	36.963	36.762	36.24	35.502 35.275	35.066	34.791	34.548	
CHAINAGE	310	320	340	360	380	384.67	399.67	414.67	425.72	433.22	m	9

LONGITUDINAL SECTION ALONG MC06 HORIZONTAL SCALE 1:500@A1 VERTICAL SCALE 1:100@A1

FUTURE STAGE

REVISION DESCRIPTION	ISSUED VER'D	APP'D DATE	CLIENT	COUNCIL	ALL DIMENSIONS TO BE VERIFIED ON SITE BEFORE COMMENCING WORK.	
A DRAFT ISSUE	JS	AK 09.08.24			NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE USABILITY, COMPLETENESS OR SCALE OF DRAWINGS	NORT
B DRAFT ISSUE	JS	AK 15.08.24	'I HIMA I		TRANSFERRED ELECTRONICALLY.	NON!
C ISSUED FOR APPROVAL	JS LM	AK 22.08.24		maitland	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR, AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE.	Newcas
			COMMUNITIES	city council	SCALE 1:500@ A1	Level 1, 215 Pacific Hwy, Cł
			DRAWING NOT TO BE USED FOR CONSTRUCTION	THE COPYRIGHT OF THIS DRAWING REMAINS WITH		Ph (02) 4943 1777 Email nev
			UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED	NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:100 @ A1	ABN 81 094

REVISION DESCRIPTION ISSUED VER'D APP'D DATE A DRAFT ISSUE AK 09.08.24 AK 15.08.24 B DRAFT ISSUE JS JS LM AK 22.08.24 C ISSUED FOR APPROVAL DRAWING NOT TO BE USED FOR CONSTRUCTION maitland city council

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PROPOSED SUBDIVISION 559 ANAMBAH ROAD

GOSFORTH NSW 2320

MASTERPLANNING DA

CIVIL ENGINEERING PACKAGE

ROAD LONGITUDINAL SECTIONS -SHEET 17

	JOB NUMBER	
	NL222055-0 ²	1
	DRAWING NUMBER	F
-	MD COE 47	

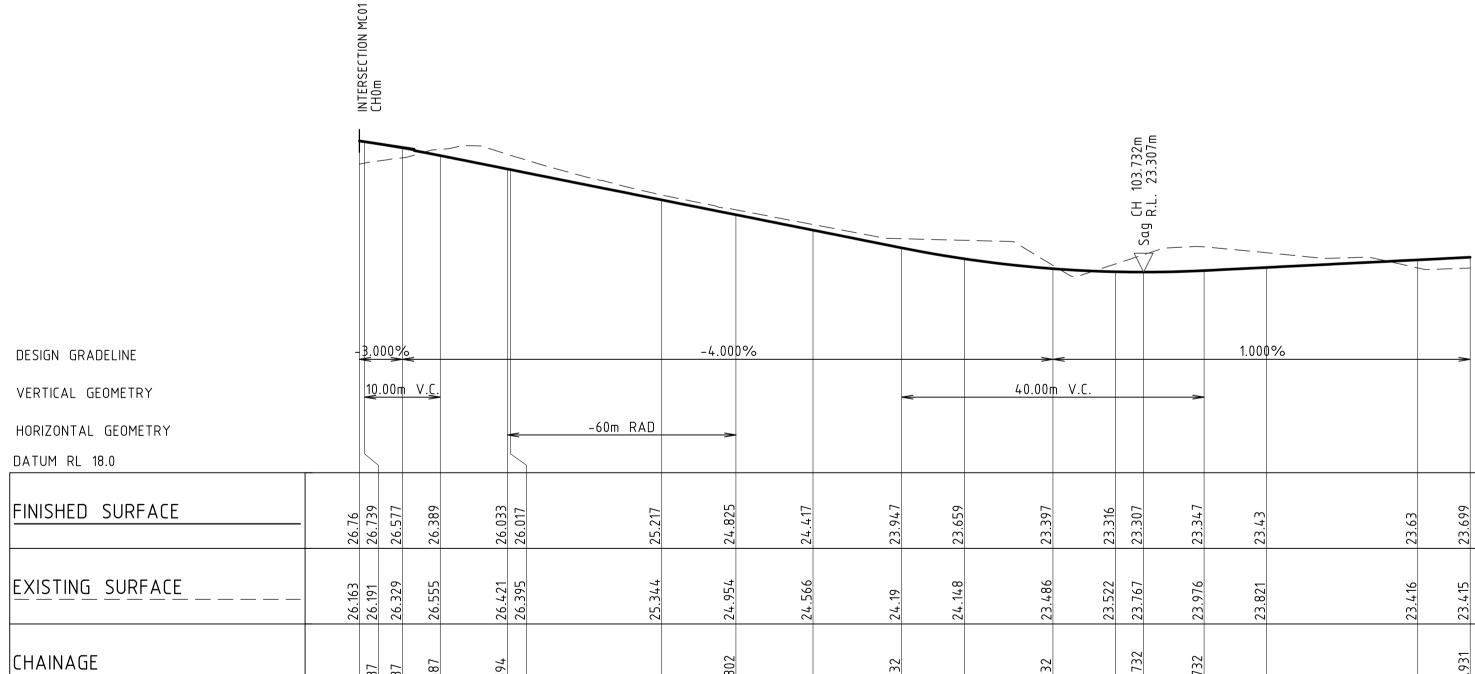
NOT FOR CONSTRUCTION

MP-C05.47

DRAWING SHEET SIZE = A1

YOU DIG

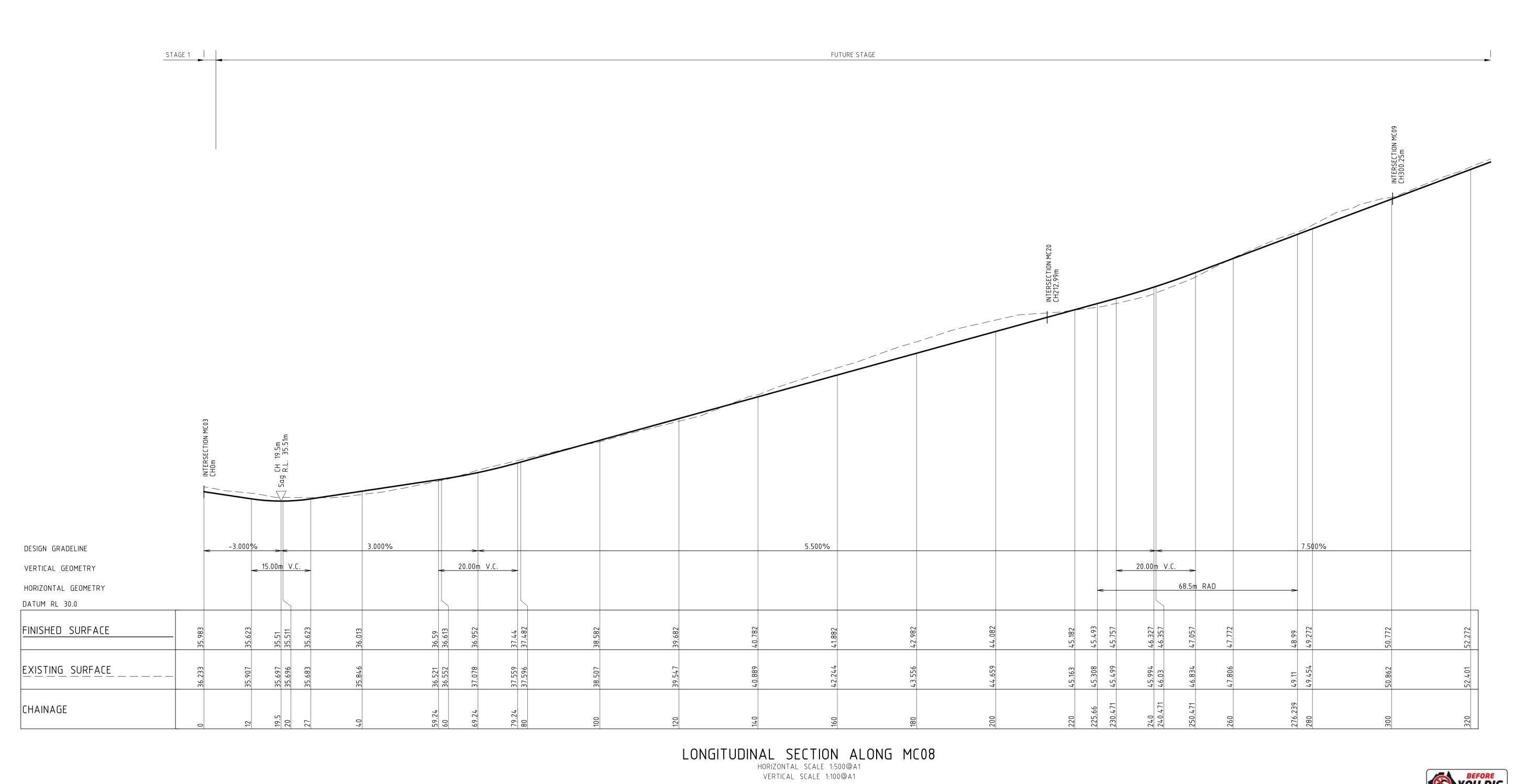
STAGE 1



UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED

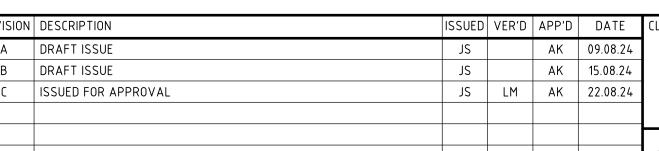
LONGITUDINAL SECTION ALONG MC07 HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1





REVISION DESCRIPTION A DRAFT ISSUE B DRAFT ISSUE	ISSUED VER'D APP'D DATE	CLIENT Thirdi	COUNCIL	ALL DIMENSIONS TO BE VERIFIED ON SITE BEFORE COMMENCING WORK. NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE USABILITY, COMPLETENESS OR SCALE OF DRAWINGS TRANSFERRED FLECTRONICALLY	NORTHROP	PROJECT PROPOSED SUBDIVISION 559 ANAMBAH ROAD	CIVIL ENGINEERING PACKAGE	JOB NUMBER NL222055-01	1
C ISSUED FOR APPROVAL	JS LM AK 22.08.24	COMMUNITIES	maitland city council	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR, AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE. O 5 10 15 20 25m	Newcastle Level 1, 215 Pacific Hwy, Charlestown NSW 2290	GOSFORTH NSW 2320	ROAD LONGITUDINAL SECTIONS -	MP-C05.48	REVISION
		DRAWING NOT TO BE USED FOR CONSTRUCTION UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED	THE COPYRIGHT OF THIS DRAWING REMAINS WITH NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:100 @ A1 0 1 2 3 4 5m	Ph (02) 4943 1777 Email newcastle@northrop.com.au ABN 81 094 433 100	MASTERPLANNING DA	SHEET 18	DRAWING SHEET SIZE = A1	1



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PROPOSED SUBDIVISION 559 ANAMBAH ROAD **GOSFORTH NSW 2320**

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CIVIL ENGINEERING PACKAGE

ROAD LONGITUDINAL SECTIONS -SHEET 19

NOT FOR CONSTRUCTION NL222055-01 DRAWING NUMBER MP-C05.49

DRAWING SHEET SIZE = A1

									INTERSECTION MC03 CH385.25m
DESIGN GRADELINE			7.500%			•	3.000%		
VERTICAL GEOMETRY				•	30.00n	n V.	C. >		
HORIZONTAL GEOMETRY									
DATUM RL 47.0									
FINISHED SURFACE	51.522	52.272		53.772	54.856	55.021	55.475	55.724	55.881
EXISTING SURFACE	51.649	52.401		53.895	55.077	55.381	56.083	56.294	56.3
CHAINAGE	310	320		340 341.7	356.7	360	371.7	380	385.25

LONGITUDINAL SECTION ALONG MC08 HORIZONTAL SCALE 1:500@A1 VERTICAL SCALE 1:100@A1

FUTURE STAGE

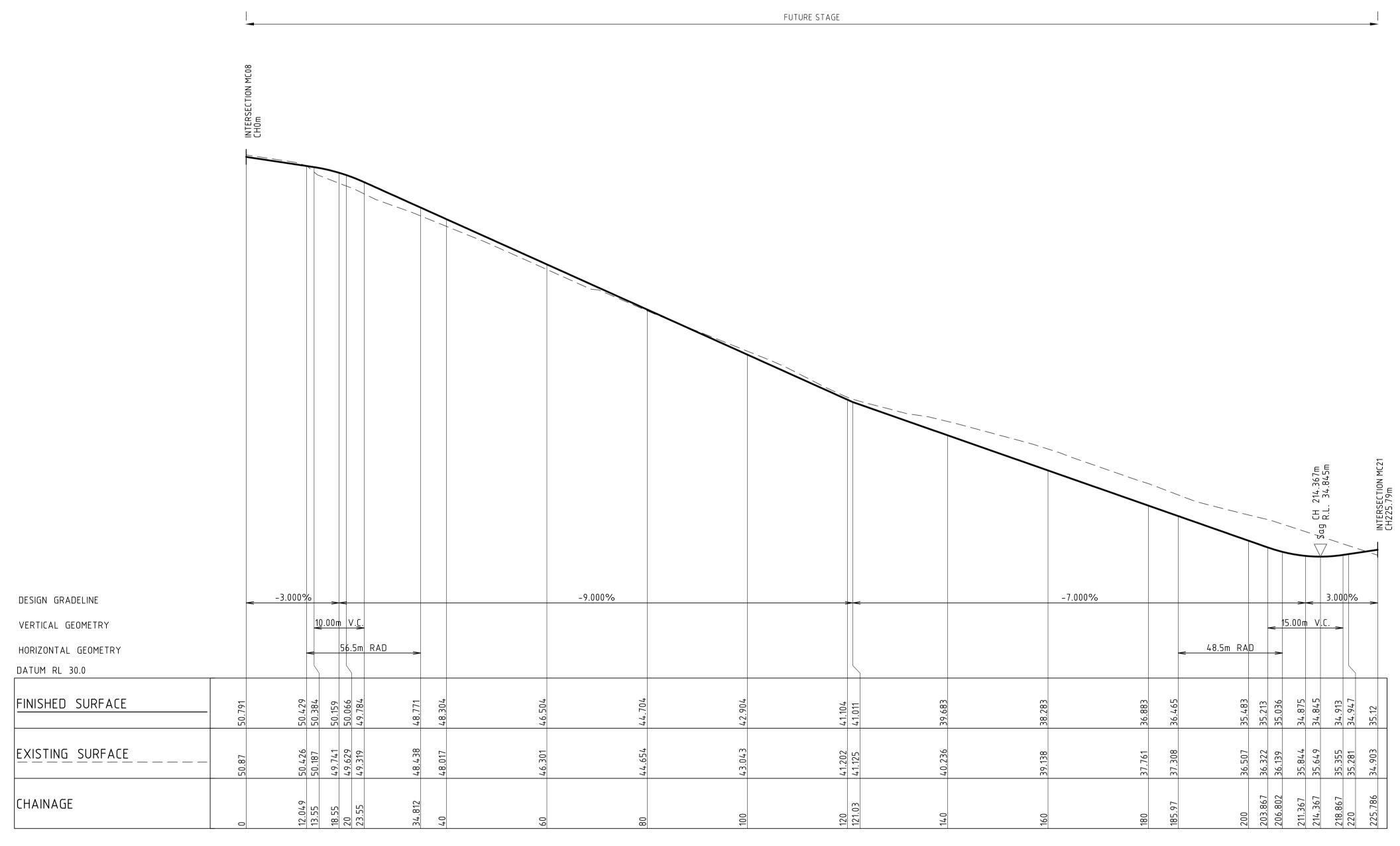
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REVISION	DESCRIPTION	ISSUED	VER'D	APP'D	DATE	CL
Α	DRAFT ISSUE	JS		AK	09.08.24	
В	DRAFT ISSUE	JS		AK	15.08.24	
С	ISSUED FOR APPROVAL	JS	LM	AK	22.08.24	

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AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE. SCALE 1:100 @ A1

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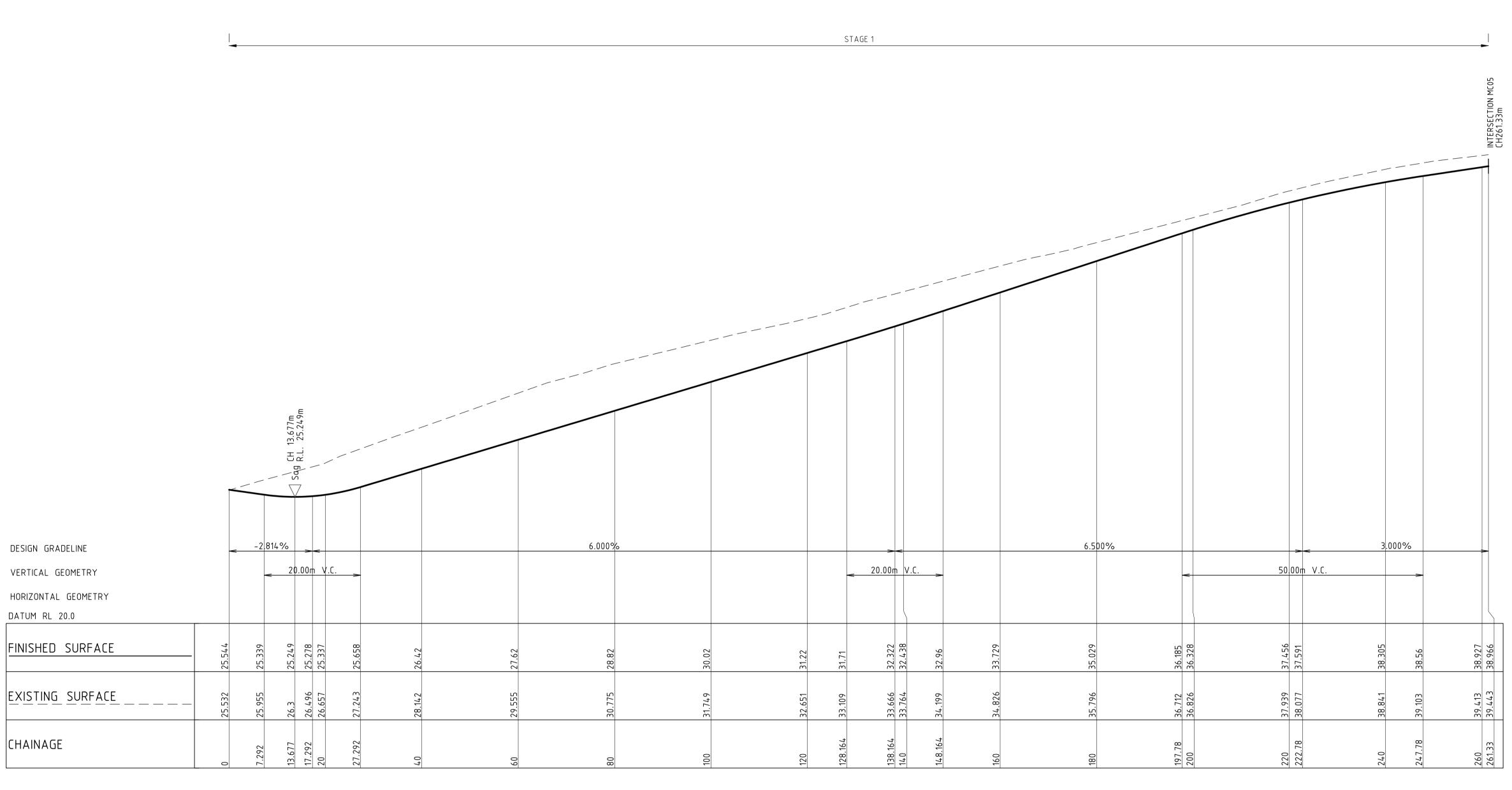
LONGITUDINAL SECTION ALONG MC09

HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1



REVISION DESCRIPTION	ISSUED VER'D APP'D DATE CLIENT	COUNCIL	ALL DIMENSIONS TO BE VERIFIED ON SITE BEFORE		PROJECT	DRAWING TITLE	JOB NUMBER	
A DRAFT ISSUE	JS AK 09.08.24		COMMENCING WORK. NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE	NODTHPOD	PROPOSED SUBDIVISION	CIVIL ENGINEERING PACKAGE	NL222055-01	l
B DRAFT ISSUE	JS AK 15.08.24		TRANSFERRED ELECTRONICALLY.	MONTHINOF	559 ANAMBAH ROAD			
C ISSUED FOR APPROVAL	JS LM AK 22.08.24	maitland	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR,	Newcastle	GOSFORTH NSW 2320		DRAWING NUMBER REV	EVISION
	COMMUNITIES	city council	0 5 10 15 20 25m	Level 1, 215 Pacific Hwy, Charlestown NSW 2290		ROAD LONGITUDINAL SECTIONS -	MP-C05.50 (C
	DRAWING NOT TO BE USED FOR CONSTRUCTION	THE CODYDIGHT OF THIS DDAWING DEMAINS WITH	SCALE 1:500@ A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au	MASTERPLANNING DA	SHEET 20	WIF-CUS.50 \	C
	UNLESS VERIFICATION SIGNATURE HAS BEEN ADD	ED NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:100 @ A1	ABN 81 094 433 100	MAGIERI EARINING DA		DRAWING SHEET SIZE = A1	
Date: 22.08.2024 4:55 PM Plotted By: ANDREW KILLEN Found: O	0:15 Pre-July 24 Projects\Newcastle\YEAR 2022 Jobs\NL222055-01 - 559 Anambah Road, Gosforth\O - Drawings\CIVIL\03-CAD\MP-MASTERPLAN\NL222055-01-MP-C05.31-LONG SECTIONS.dwg							



LONGITUDINAL SECTION ALONG MC10
HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1



NOT FOR CONSTRUCTION

REVISION	DESCRIPTION	ISSUED	VER'D	APP'D	DATE	CL
А	DRAFT ISSUE	JS		AK	09.08.24	
В	DRAFT ISSUE	JS		AK	15.08.24	
С	ISSUED FOR APPROVAL	JS	LM	AK	22.08.24	
						1
						1 1

ISSUED VER'D APP'D DATE CLIENT Third.i DRAWING NOT TO BE USED FOR CONSTRUCTION UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED THE COPYRIGHT OF THIS DRAWING REMAINS WITH

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ABN 81 094 433 100

MASTERPLANNING DA

PROPOSED SUBDIVISION 559 ANAMBAH ROAD **GOSFORTH NSW 2320**

ROAD LONGITUDINAL SECTIONS -SHEET 21

CIVIL ENGINEERING PACKAGE

NL222055-01 DRAWING NUMBER MP-C05.51



CHAINAGE

REVISION DESCRIPTION ISSUED VER'D APP'D DATE A DRAFT ISSUE AK 15.08.24 B DRAFT ISSUE JS C ISSUED FOR APPROVAL JS LM AK 22.08.24

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PROPOSED SUBDIVISION 559 ANAMBAH ROAD **GOSFORTH NSW 2320**

MASTERPLANNING DA

CIVIL ENGINEERING PACKAGE

ROAD LONGITUDINAL SECTIONS SHEET 22

NOT FOR CONSTRUCTION							
IGINEERING PACKAGE	JOB NUMBER NL222055-0 1	1					
NGITUDINAL SECTIONS - SHEET 22	MP-C05.52	RI					

YOU DIG

DRAWING SHEET SIZE = A1

LONGITUDINAL SECTION ALONG MC11

HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1

	INTERSECTION MC05 CH0m Sag CH 8.767m /				
DESIGN GRADELINE	-3.000%	8.500%		2.000%	3.000%
VERTICAL GEOMETRY HORIZONTAL GEOMETRY DATUM RL 27.0	20.00m V.C.		60.00m V.C.	>	
FINISHED SURFACE	32.042 31.935 31.857 31.923 32.22 32.485	33.884	37.014	38.536 38.583 38.983	39.225 39.29 39.398 39.45 39.725 39.725
EXISTING SURFACE	33.318 33.63 34.122 34.395 34.762 34.955	35.717	38.735	39.548	40.621 40.743 40.825 40.945 40.993 41.032 41.011

STAGE 1



CHAINAGE

REVISION DESCRIPTION ISSUED VER'D APP'D DATE A DRAFT ISSUE AK 09.08.24 JS AK 15.08.24 B DRAFT ISSUE JS LM AK 22.08.24 C ISSUED FOR APPROVAL DRAWING NOT TO BE USED FOR CONSTRUCTION UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED

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Newcastle Level 1, 215 Pacific Hwy, Charlestown NSW 2290

Ph (02) 4943 1777 Email newcastle@northrop.com.au ABN 81 094 433 100

PROPOSED SUBDIVISION 559 ANAMBAH ROAD **GOSFORTH NSW 2320**

MASTERPLANNING DA

CIVIL ENGINEERING PACKAGE

ROAD LONGITUDINAL SECTIONS SHEET 23

	JOB NUMBER	
	NL222055-0 ⁻	1
	DRAWING NUMBER	RE
-	MP-C05.53	

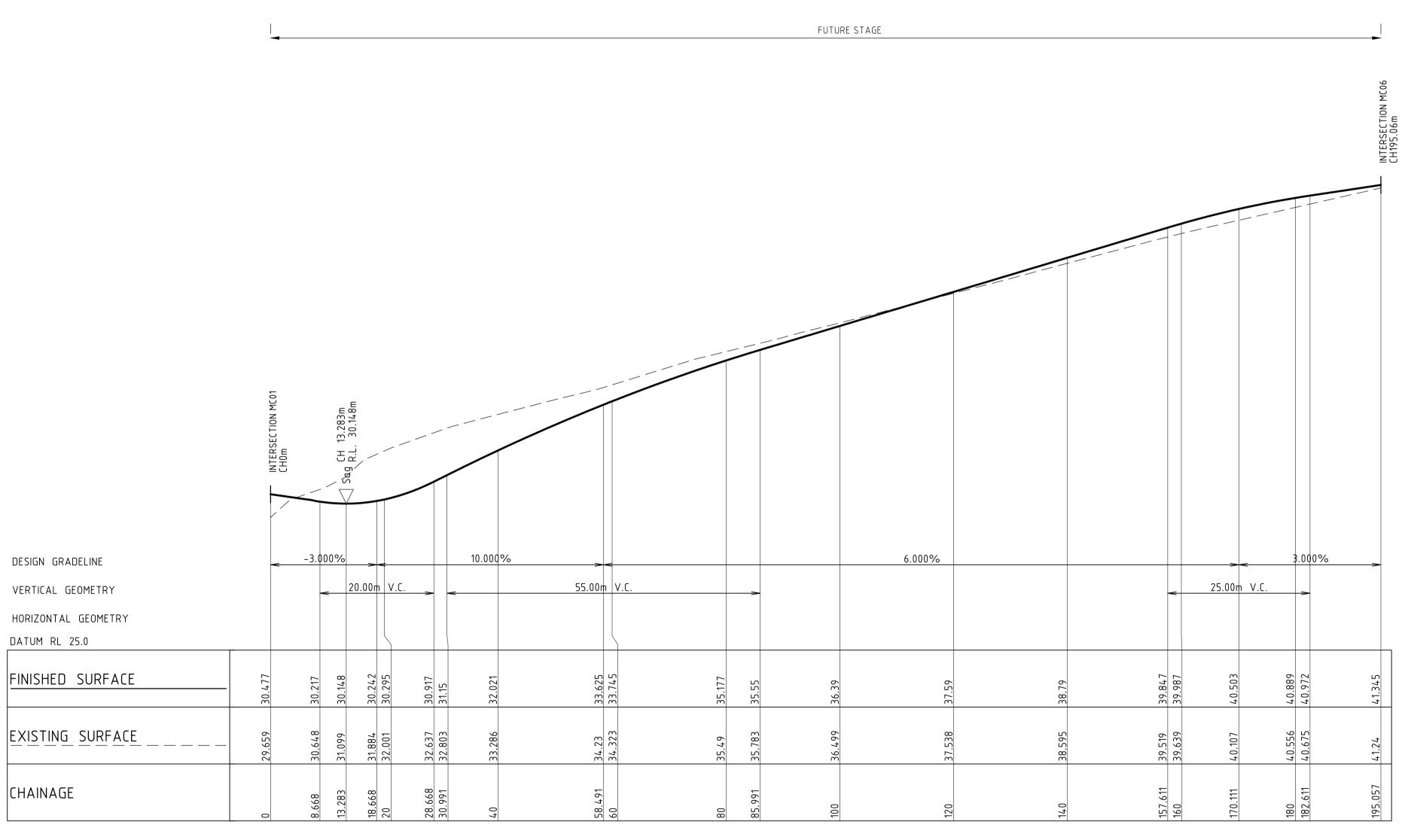
DRAWING SHEET SIZE = A1

3.000% DESIGN GRADELINE 60.00m V.C. 20.00m V.C. VERTICAL GEOMETRY HORIZONTAL GEOMETRY DATUM RL 24.0 FINISHED SURFACE EXISTING SURFACE

LONGITUDINAL SECTION ALONG MC12 HORIZONTAL SCALE 1:500@A1 VERTICAL SCALE 1:100@A1

FUTURE STAGE

YOU DIG NOT FOR CONSTRUCTION



LONGITUDINAL SECTION ALONG MC13
HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1



NOT FOR CONSTRUCTION

REVISION	DESCRIPTION	ISSUED	VER'D	APP'D	DATE	CL
Α	DRAFT ISSUE	JS		AK	09.08.24	
В	DRAFT ISSUE	JS		AK	15.08.24	
С	ISSUED FOR APPROVAL	JS	LM	AK	22.08.24	
					1	4

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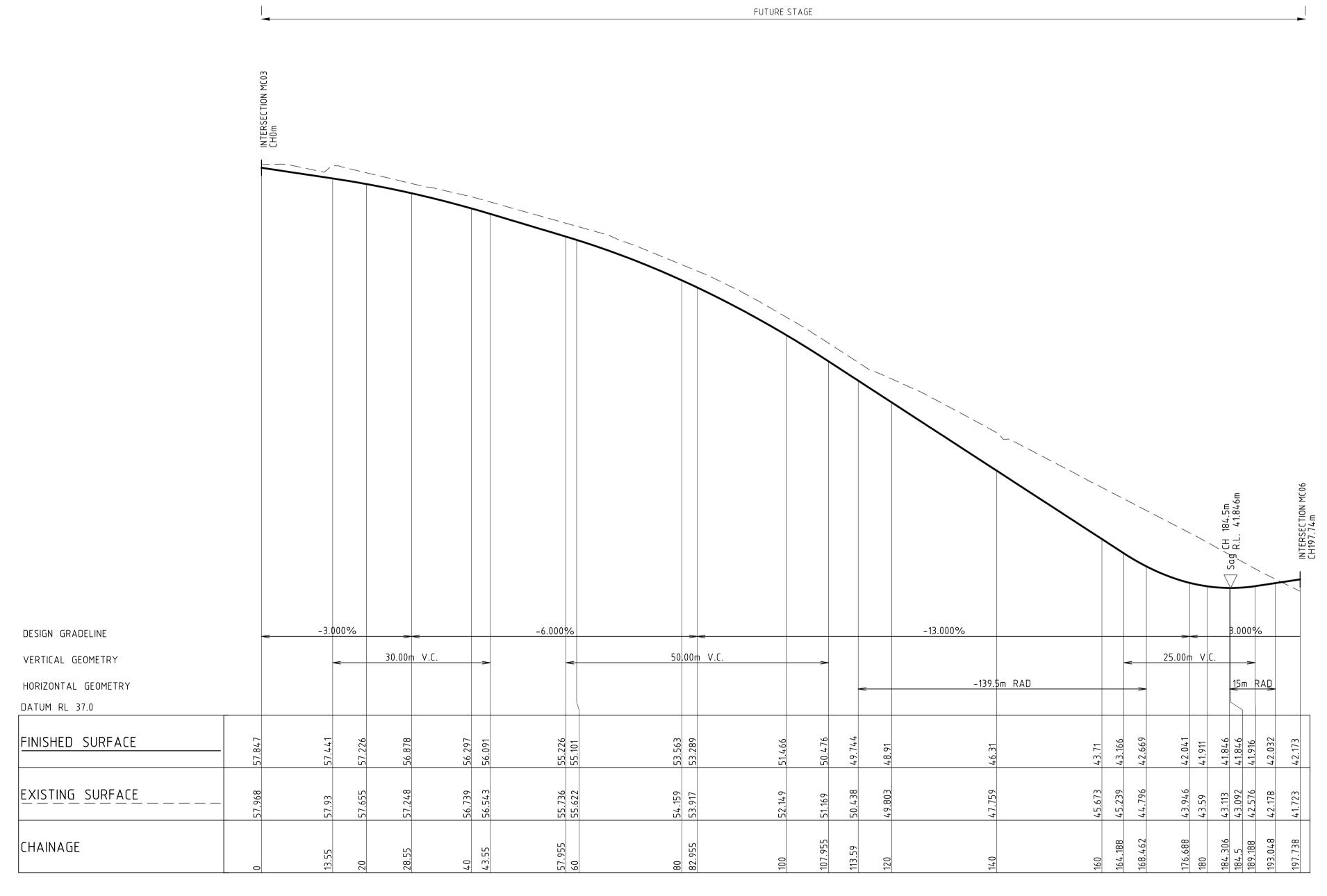
Newcastle Level 1, 215 Pacific Hwy, Charlestown NSW 2290 Ph (02) 4943 1777 Email newcastle@northrop.com.au ABN 81 094 433 100 PROPOSED SUBDIVISION 559 ANAMBAH ROAD **GOSFORTH NSW 2320**

MASTERPLANNING DA

CIVIL ENGINEERING PACKAGE

ROAD LONGITUDINAL SECTIONS -SHEET 24

JOB NUMBER	
NL222055-0 ⁻	1
DRAWING NUMBER	REV
MP-C05.54	(



LONGITUDINAL SECTION ALONG MC14
HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1



NOT FOR CONSTRUCTION

REVISION	DESCRIPTION	ISSUED	VER'D	APP'D	DATE	CL
Α	DRAFT ISSUE	JS		AK	09.08.24	
В	DRAFT ISSUE	JS		AK	15.08.24	
С	ISSUED FOR APPROVAL	JS	LM	AK	22.08.24	
						Г

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ABN 81 094 433 100

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PROPOSED SUBDIVISION 559 ANAMBAH ROAD **GOSFORTH NSW 2320**

CIVIL ENGINEERING PACKAGE

ROAD LONGITUDINAL SECTIONS -SHEET 25

JOB NUMBER	
NL222055-0 ⁻	1
DRAWING NUMBER	REVI
MP-C05.55	

FUTURE STAGE

					/
				`	
DESIGN GRADELINE			1.000%		>
VERTICAL GEOMETRY					
HORIZONTAL GEOMETRY					
DATUM RL 37.0					
FINISHED SURFACE	42.826	42.926		43.126	43.232
EXISTING SURFACE	43.213	43.068		42.602	43.719
CHAINAGE	310	320		340	350.506

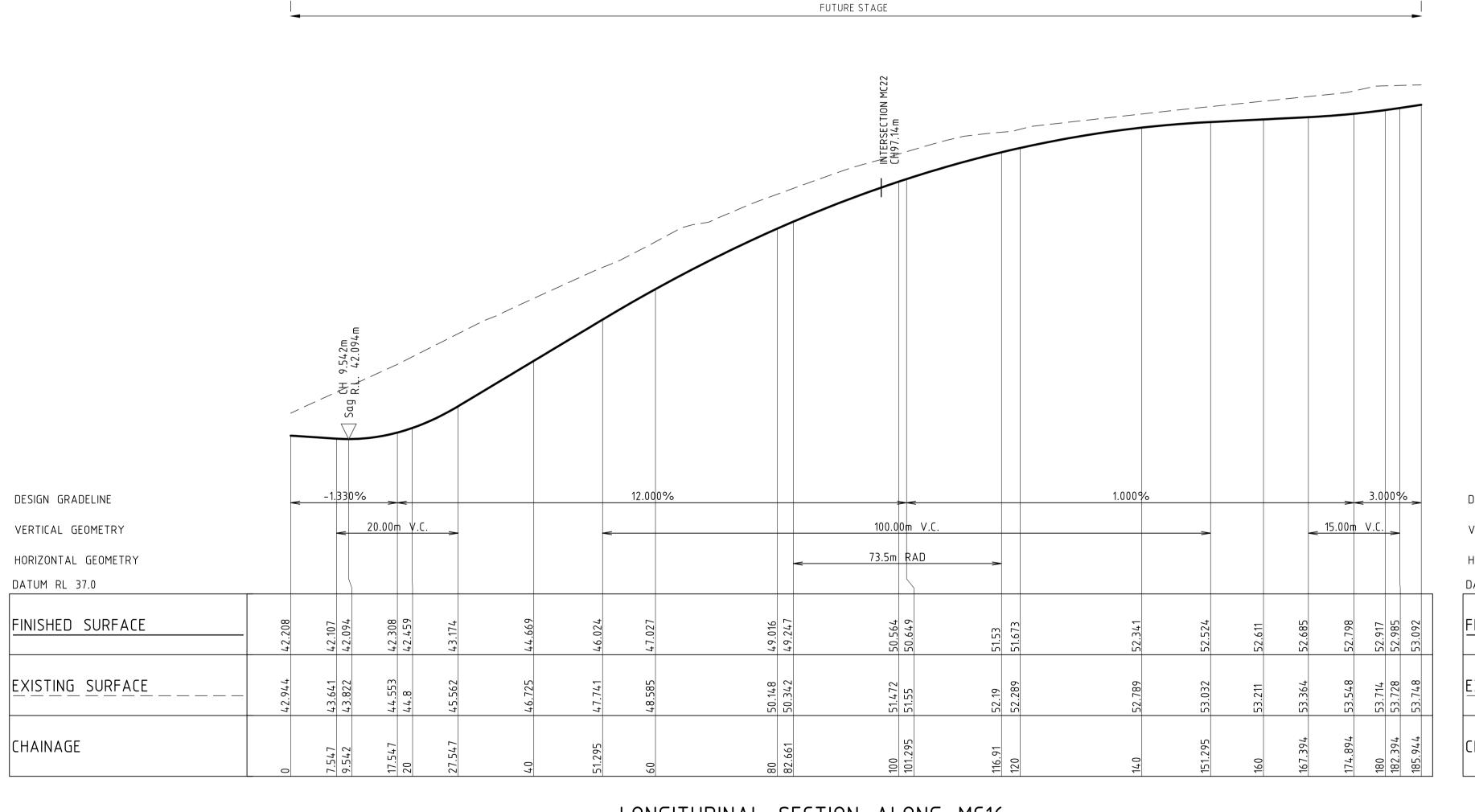
LONGITUDINAL SECTION ALONG MC15 HORIZONTAL SCALE 1:500@A1 VERTICAL SCALE 1:100@A1

FUTURE STAGE 1.000% -3.000% 10.000% DESIGN GRADELINE 60.00m V.C. 25.00m V.C. ____15.00m V.C. 80.00m V.C. VERTICAL GEOMETRY 23.5m RAD HORIZONTAL GEOMETRY DATUM RL 33.0 FINISHED SURFACE EXISTING SURFACE CHAINAGE

LONGITUDINAL SECTION ALONG MC15 HORIZONTAL SCALE 1:500@A1 VERTICAL SCALE 1:100@A1



REVISION DESCRIPTION A DRAFT ISSUE B DRAFT ISSUE	ISSUED VER'D APP'D DATE	CLIENT	COUNCIL	ALL DIMENSIONS TO BE VERIFIED ON SITE BEFORE COMMENCING WORK. NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE USABILITY, COMPLETENESS OR SCALE OF DRAWINGS	NORTHROP	PROJECT PROPOSED SUBDIVISION 559 ANAMBAH ROAD	DRAWING TITLE CIVIL ENGINEERING PACKAGE	JOB NUMBER NL222055-01	1
C ISSUED FOR APPROVAL	JS LM AK 22.08.24	COMMUNITIES	maitland city council	TRANSFERRED ELECTRONICALLY. THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR, AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE. SCALE 1.500@ A1 0 5 10 15 20 25m	Newcastle Level 1, 215 Pacific Hwy, Charlestown NSW 2290	GOSFORTH NSW 2320	ROAD LONGITUDINAL SECTIONS -	DRAWING NUMBER MP-C05.56	REVISION
		DRAWING NOT TO BE USED FOR CONSTRUCTION UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED	THE COPYRIGHT OF THIS DRAWING REMAINS WITH NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:100 @ A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au ABN 81 094 433 100	MASTERPLANNING DA	SHEET 26	DRAWING SHEET SIZE = A1	



DESIGN GRADELINE

-3,000%

5,000%

7,000%

3,000%

V.C.

20,00n V.C.

20,00n V.C.

40,000 V.C.

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40,000 V.C.

STAGE 1

LONGITUDINAL SECTION ALONG MC16

HORIZONTAL SCALE 1:500@A1

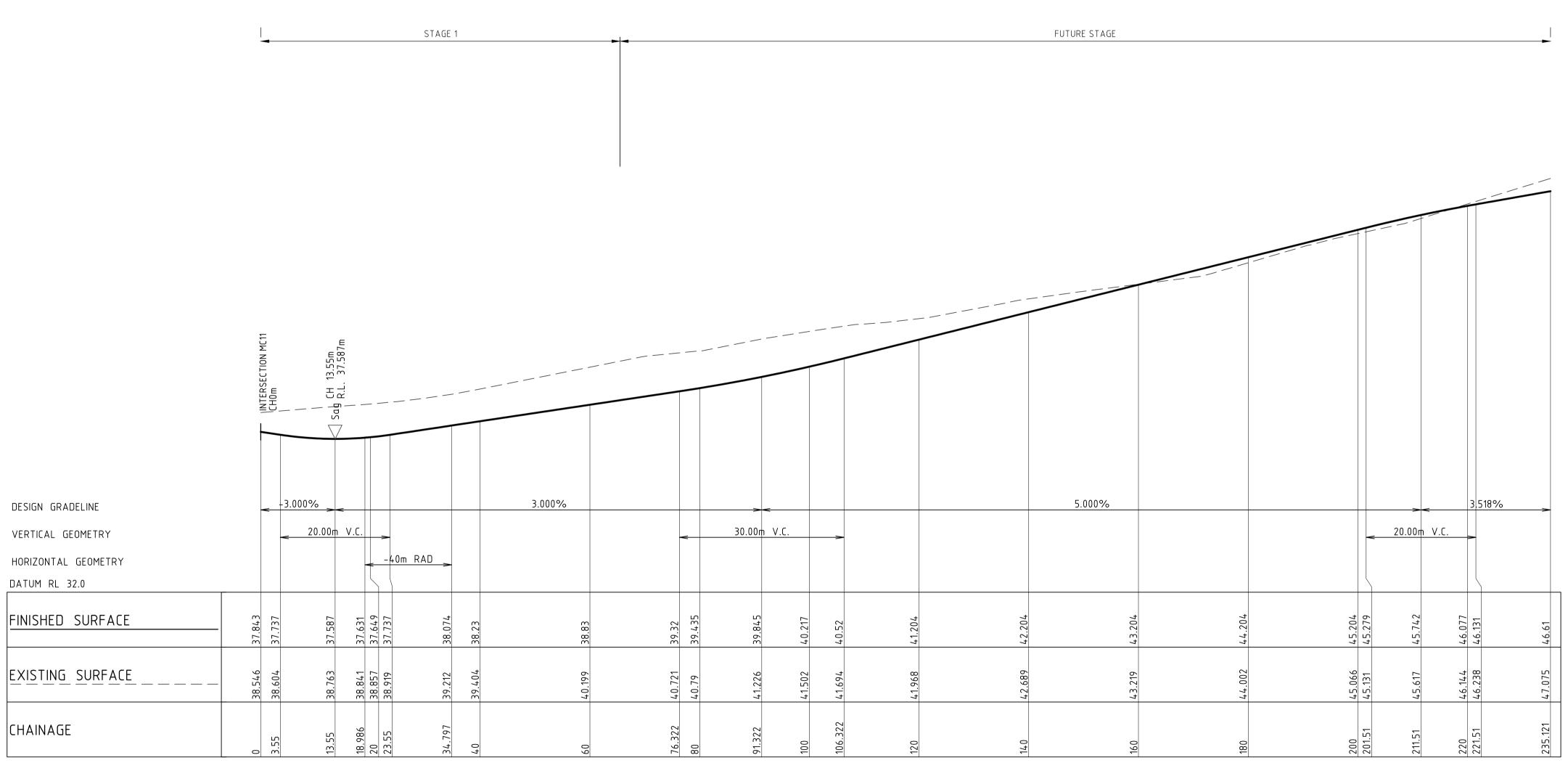
VERTICAL SCALE 1:100@A1

LONGITUDINAL SECTION ALONG MC17
HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:500@A1



REVISION DESCRIPTION	ISSUED VER'D APP'D D.	ATE CLIENT	COUNCIL	ALL DIMENSIONS TO BE VERIFIED ON SITE BEFORE		PROJECT	DRAWING TITLE	JOB NUMBER	•
A DRAFT ISSUE B DRAFT ISSUE	JS AK 09. JS AK 15.0	08.24		COMMENCING WORK. NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE USABILITY, COMPLETENESS OR SCALE OF DRAWINGS TRANSFERRED ELECTRONICALLY.	NORTHROP	PROPOSED SUBDIVISION 559 ANAMBAH ROAD	CIVIL ENGINEERING PACKAGE	NL222055-0	1
C ISSUED FOR APPROVAL	JS LM AK 22.	COMMUNITIES	maitland city council	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR, AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE. 0 5 10 15 20 25m	Newcastle Level 1, 215 Pacific Hwy, Charlestown NSW 2290	GOSFORTH NSW 2320	ROAD LONGITUDINAL SECTIONS -	MP-C05.57	REVISIO
		DRAWING NOT TO BE USED FOR CONSTRUCTION UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED	THE COPYRIGHT OF THIS DRAWING REMAINS WITH NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:100 @ A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au ABN 81 094 433 100	MASTERPLANNING DA	SHEET 27	DRAWING SHEET SIZE = 1	11



LONGITUDINAL SECTION ALONG MC18
HORIZONTAL SCALE 1:500@A1 VERTICAL SCALE 1:100@A1



NOT FOR CONSTRUCTION

REV	SION	DESCRIPTION	ISSUED	VER'D	APP'D	DATE	CLIE
<i></i>	7	DRAFT ISSUE	JS		AK	09.08.24	
E	3	DRAFT ISSUE	JS		AK	15.08.24	
(-	ISSUED FOR APPROVAL	JS	LM	AK	22.08.24	

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MASTERPLANNING DA

PROPOSED SUBDIVISION 559 ANAMBAH ROAD **GOSFORTH NSW 2320**

CIVIL ENGINEERING PACKAGE ROAD LONGITUDINAL SECTIONS -

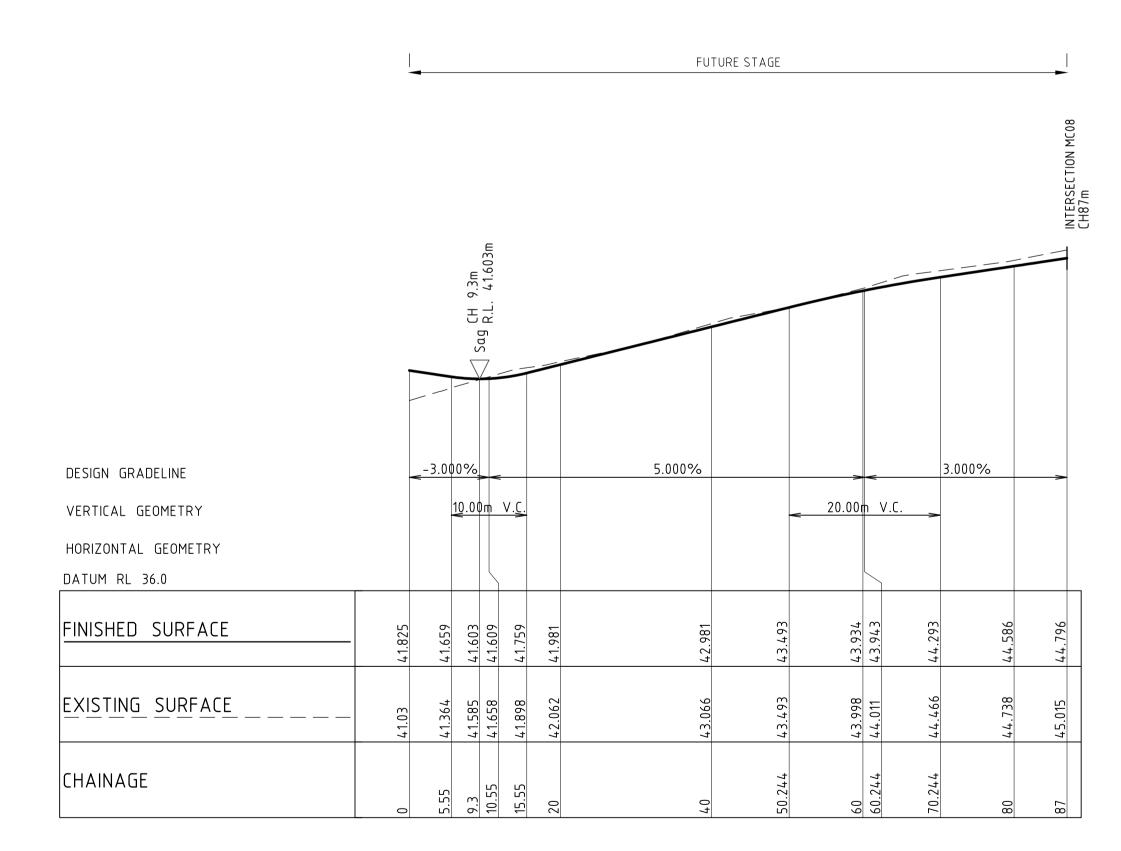
SHEET 28

JOB NUMBER	
NL222055-0 ⁻	1
DRAWING NUMBER	REV
MP-C05.58	(

DESIGN GRADELINE 10.00m V.C. 45.00m V.C. VERTICAL GEOMETRY HORIZONTAL GEOMETRY DATUM RL 35.0 FINISHED SURFACE EXISTING SURFACE 40.831 CHAINAGE

LONGITUDINAL SECTION ALONG MC19 HORIZONTAL SCALE 1:500@A1 VERTICAL SCALE 1:100@A1

FUTURE STAGE



LONGITUDINAL SECTION ALONG MC20 HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1



NOT FOR CONSTRUCTION

	JS			
A DRAFT ISSUE	,,		AK	09.08.24
B DRAFT ISSUE	JS		AK	15.08.24
C ISSUED FOR APPROVAL	JS	LM	AK	22.08.24

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10.00m V.C.

71.08 72.701 77.701 78.415 80 82.701 87

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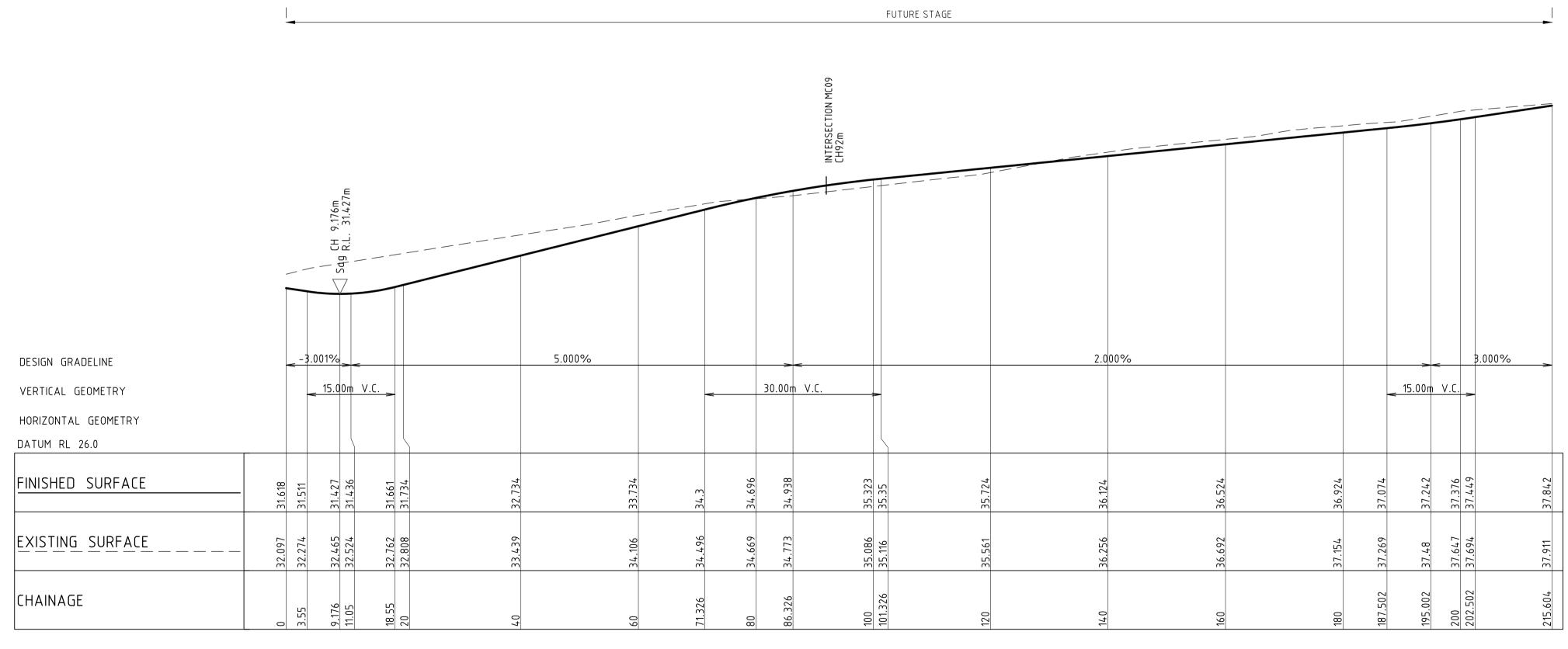
559 ANAMBAH ROAD **GOSFORTH NSW 2320**

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PROPOSED SUBDIVISION CIVIL ENGINEERING PACKAGE

ROAD LONGITUDINAL SECTIONS -SHEET 29

NL222055-01 DRAWING NUMBER MP-C05.59



LONGITUDINAL SECTION ALONG MC21
HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1



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REVISIO	N DESCRIPTION	ISSUED	VER'D	APP'D	DATE	CLI
Α	DRAFT ISSUE	JS		AK	09.08.24	
В	DRAFT ISSUE	JS		AK	15.08.24	
С	ISSUED FOR APPROVAL	JS	LM	AK	22.08.24	

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PROPOSED SUBDIVISION 559 ANAMBAH ROAD **GOSFORTH NSW 2320**

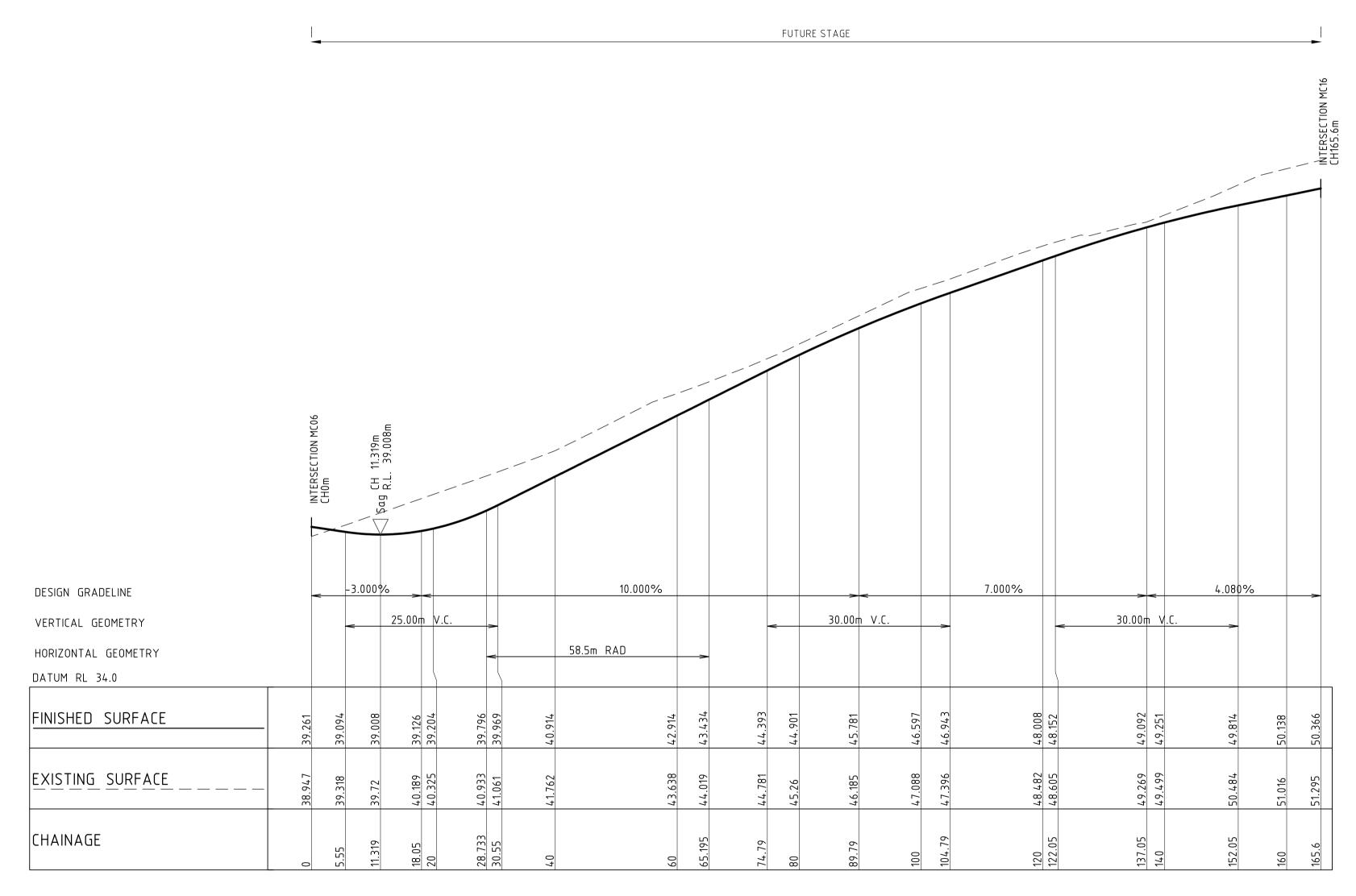
MASTERPLANNING DA

CIVIL ENGINEERING PACKAGE

ROAD LONGITUDINAL SECTIONS -SHEET 30

JOB NUMBER	
NL222055-0 ⁻	1
DRAWING NUMBER	RE'
MP-C05.60	(

DRAWING SHEET SIZE = A1



LONGITUDINAL SECTION ALONG MC22

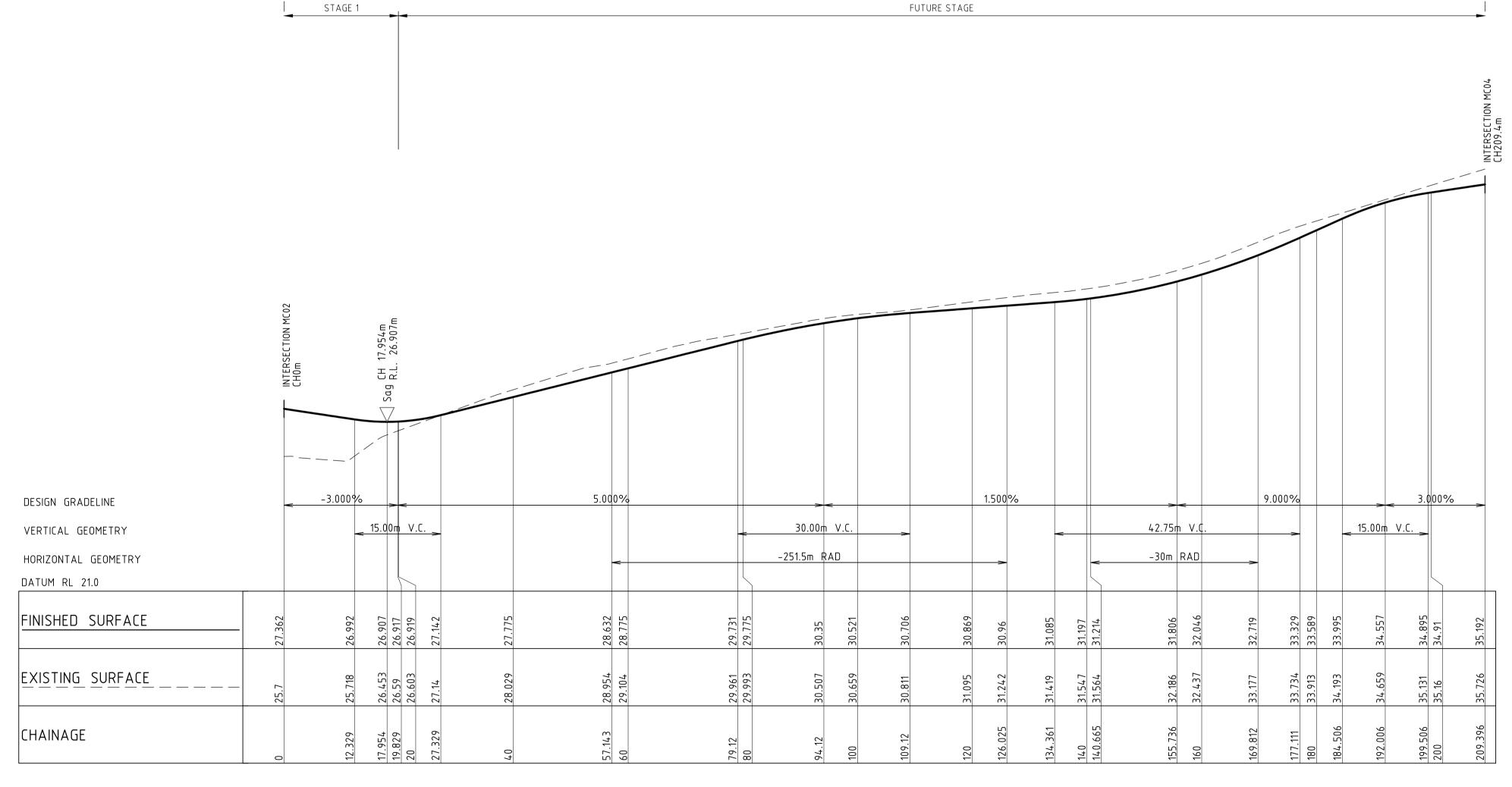
HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1



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REVISION DESCRIPTION	ISSUED VER	R'D APP'D DATE	CLIENT	COUNCIL	A	ALL DIMENSIONS TO BE VERIFIED ON SITE BEFORE		PROJECT	DRAWING TITLE	JOB NUMBER	
A DRAFT ISSUE	JS	AK 09.08.2	4		N	NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE		PROPOSED SUBDIVISION	CIVIL ENGINEERING PACKAGE	NL222055-	01
B DRAFT ISSUE	JS	AK 15.08.2			Ţ	USABILITY, CUMPLETENESS OR SCALE OF DRAWINGS TRANSFERRED ELECTRONICALLY.	MONTHING	559 ANAMBAH ROAD			
C ISSUED FOR APPROVAL	JS LM	1 AK 22.08.2		maitland	T A	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR, AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE.	Newcastle	GOSFORTH NSW 2320	DOAD LONGITUDINAL OFOTIONS	DRAWING NUMBER	l f
			COMMUNITIES	city council	SCALE 1.500@ A1	, 0 5 10 15 20 25m	Level 1, 215 Pacific Hwy, Charlestown NSW 2290		ROAD LONGITUDINAL SECTIONS -	MP-C05.61	
			DRAWING NOT TO BE USED FOR CONSTRUCTION	THE COPYRIGHT OF THIS DRAWING REMAINS WITH	SCALE 1:500@ A1	.	Ph (02) 4943 1777 Email newcastle@northrop.com.au	MASTERPLANNING DA	SHEET 31	WII 900:01	
			UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED	NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:100 @ A1	0 1 2 3 4 5m	ABN 81 094 433 100			DRAWING SHEET SIZE =	- A1
Date: 22.08.2024 4:55 PM Plotted By: ANDREW KILLEN Found: O:\5 Pre-July 24 Projects\Newcastle\YE	'EAR 2022 Jobs\NL222055-01 - 559 Anambah F	Road, Gosforth\O - Drawings\CIVIL\03-	CADIMP-MASTERPLANINL222055-01-MP-C05.31-LONG SECTIONS.dwg		·						



LONGITUDINAL SECTION ALONG MC23

HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1



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REVISION	DESCRIPTION	ISSUED	VER'D	APP'D	DATE	CLI
А	DRAFT ISSUE	JS		AK	09.08.24]
В	DRAFT ISSUE	JS		AK	15.08.24	
С	ISSUED FOR APPROVAL	JS	LM	AK	22.08.24	
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PROPOSED SUBDIVISION 559 ANAMBAH ROAD **GOSFORTH NSW 2320**

MASTERPLANNING DA

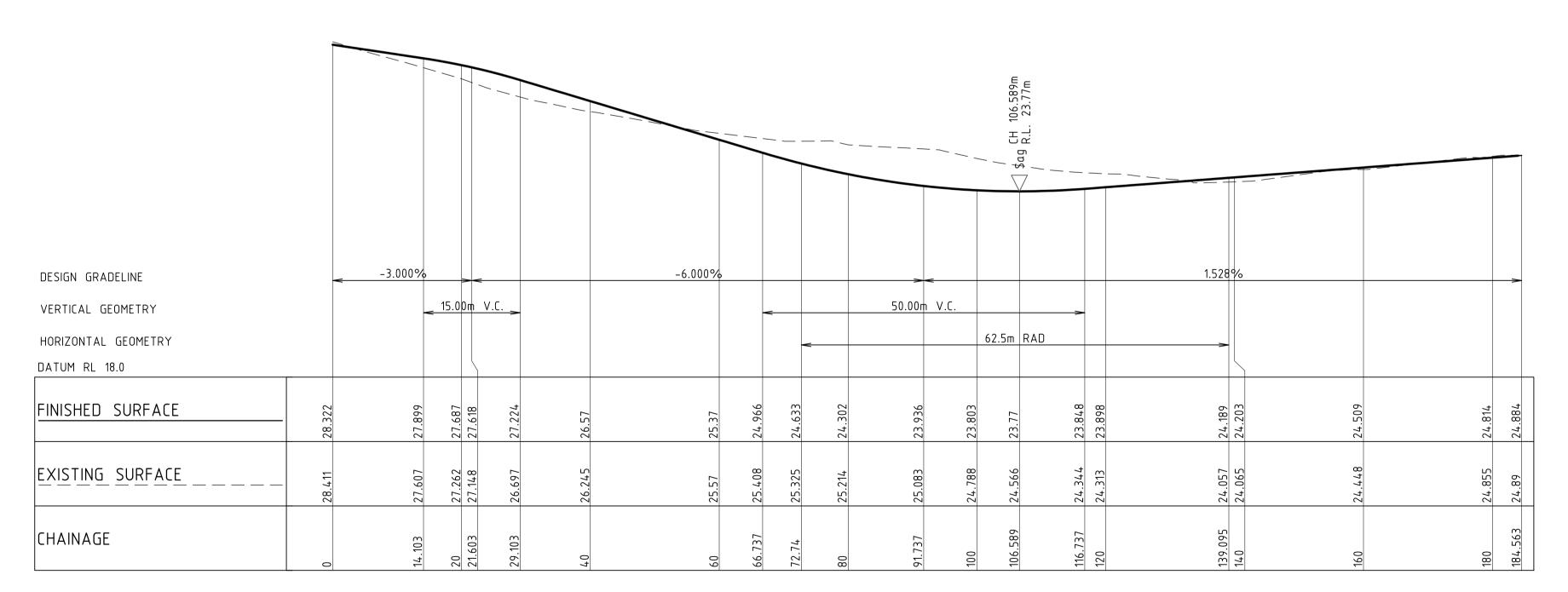
CIVIL ENGINEERING PACKAGE

ROAD LONGITUDINAL SECTIONS SHEET 32

	JOB NUMBER	
	NL222055-0 ⁻	1
	DRAWING NUMBER	R
-	MP-C05.62	

DRAWING SHEET SIZE = A1

STAGE 1



LONGITUDINAL SECTION ALONG MC24 HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1



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REVISION	DESCRIPTION	ISSUED	VER'D	APP'D	DATE	CL
Α	DRAFT ISSUE	JS		AK	09.08.24	
В	DRAFT ISSUE	JS		AK	15.08.24	
С	ISSUED FOR APPROVAL	JS	LM	AK	22.08.24	
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COMMUNITIES

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maitland
city council

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COMMENCING WORK.
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USABILITY, COMPLETENESS OR SCALE OF DRAWINGS
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SCALE 1:500@ A1

SCALE 1:100@ A1



ABN 81 094 433 100

PROPOSED SUBDIVISION 559 ANAMBAH ROAD GOSFORTH NSW 2320

MASTERPLANNING DA

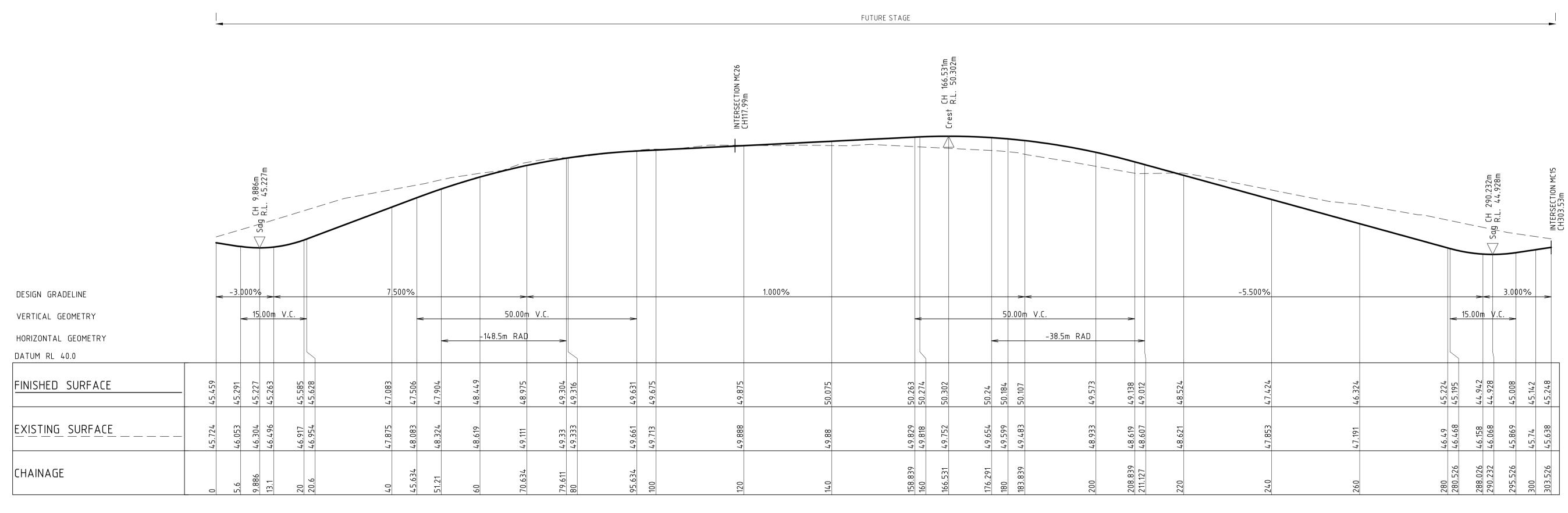
CIVIL ENGINEERING PACKAGE

ROAD LONGITUDINAL SECTIONS -SHEET 33

JOB NUMBER	
NL222055-0 ⁻	1
DRAWING NUMBER	R

MP-C05.63

DRAWING SHEET SIZE = A1

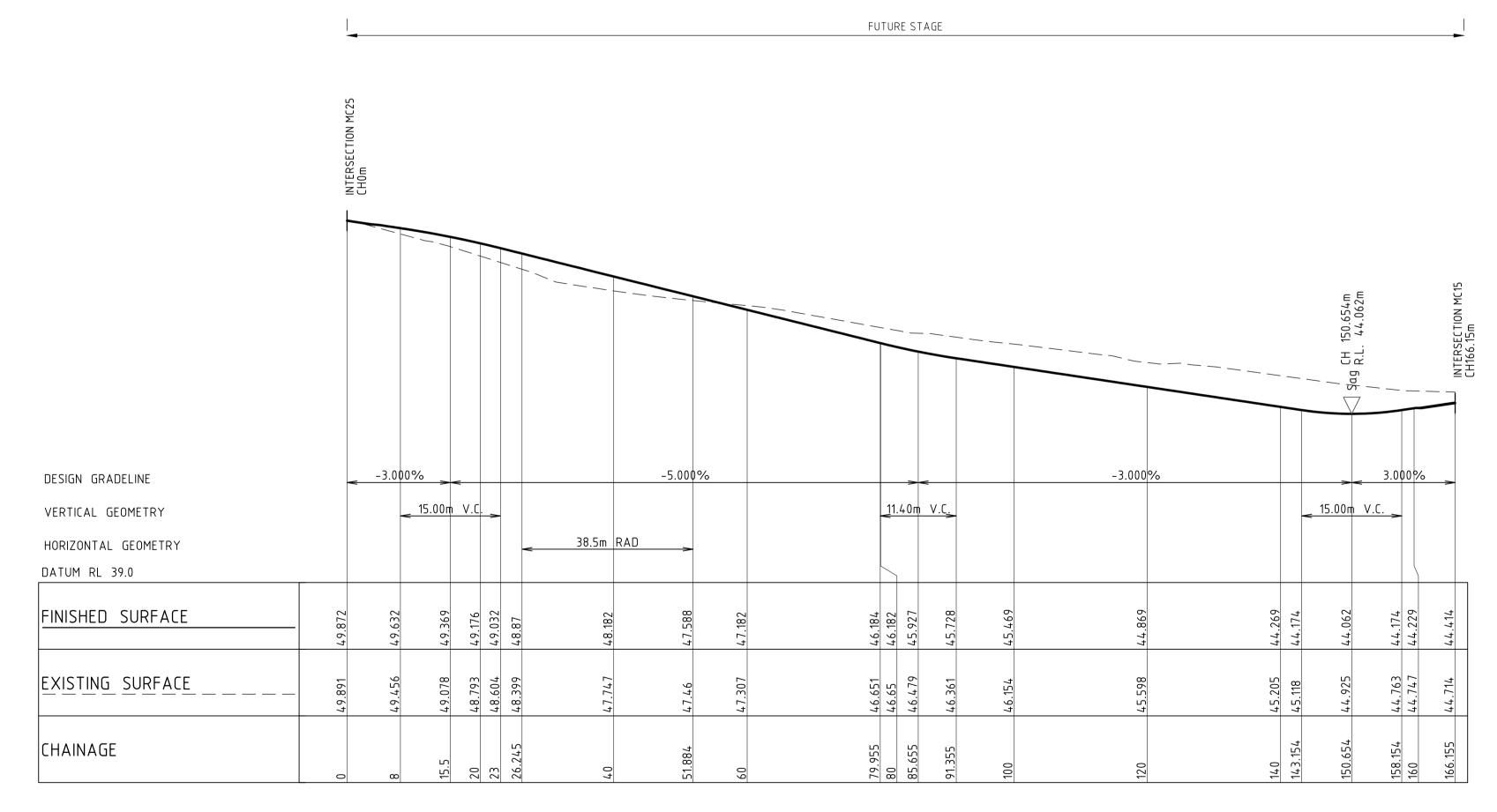


LONGITUDINAL SECTION ALONG MC25 HORIZONTAL SCALE 1:500@A1 VERTICAL SCALE 1:100@A1



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REVISIO	ON DESCRIPTION ISSUED VER'D APP'D DATE	CLIENT	COUNCIL	ALL DIMENSIONS TO BE VERIFIED ON SITE BEFORE		PROJECT	DRAWING TITLE	JOB NUMBER	
А	DRAFT ISSUE JS AK 09.08.24			COMMENCING WORK. NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE	NORTHROD	PROPOSED SUBDIVISION	CIVIL ENGINEERING PACKAGE	NL222055-01	
В	DRAFT ISSUE JS AK 15.08.24	' I M1ra 1		TRANSFERRED ELECTRONICALLY.		559 ANAMBAH ROAD			
С	ISSUED FOR APPROVAL JS LM AK 22.08.24		maitland	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR, AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE	Newcastle	GOSFORTH NSW 2320		DRAWING NUMBER REVI	√ISION
		COMMUNITIES	city council	0 5 10 15 20 25m	Level 1, 215 Pacific Hwy, Charlestown NSW 2290		ROAD LONGITUDINAL SECTIONS -	MP-C05.64 C	C
		DRAWING NOT TO BE USED FOR CONSTRUCTION	THE COPYRIGHT OF THIS DRAWING REMAINS WITH	SCALE 1:500@A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au	MASTERPLANNING DA	SHEET 34	1411 -005.04 (
		UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED	NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:100 @ A1 0 1 2 3 4 5m	ABN 81 094 433 100			DRAWING SHEET SIZE = A1	
Date: 22.08.20	024 4:55 PM Plotted By: ANDREW KILLEN Found: 0:15 Pre-July 24 Projects'Newcastle\YEAR 2022 Jobs\NL222055-01 - 559 Anambah Road, Gosforth\0 - Drawings\CIVIL\03-CAD\MP	P-MASTERPLANINL222055-01-MP-C05.31-LONG SECTIONS.dwg							



LONGITUDINAL SECTION ALONG MC26

HORIZONTAL SCALE 1:500@A1

VERTICAL SCALE 1:100@A1



NOT FOR CONSTRUCTION

REVISION	DESCRIPTION	ISSUED	VER'D	APP'D	DATE	CL
Α	DRAFT ISSUE	JS		AK	09.08.24	
В	DRAFT ISSUE	JS		AK	15.08.24	
С	ISSUED FOR APPROVAL	JS	LM	AK	22.08.24	
						Г

CLIENT

COMMUNITIES

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PROPOSED SUBDIVISION 559 ANAMBAH ROAD GOSFORTH NSW 2320

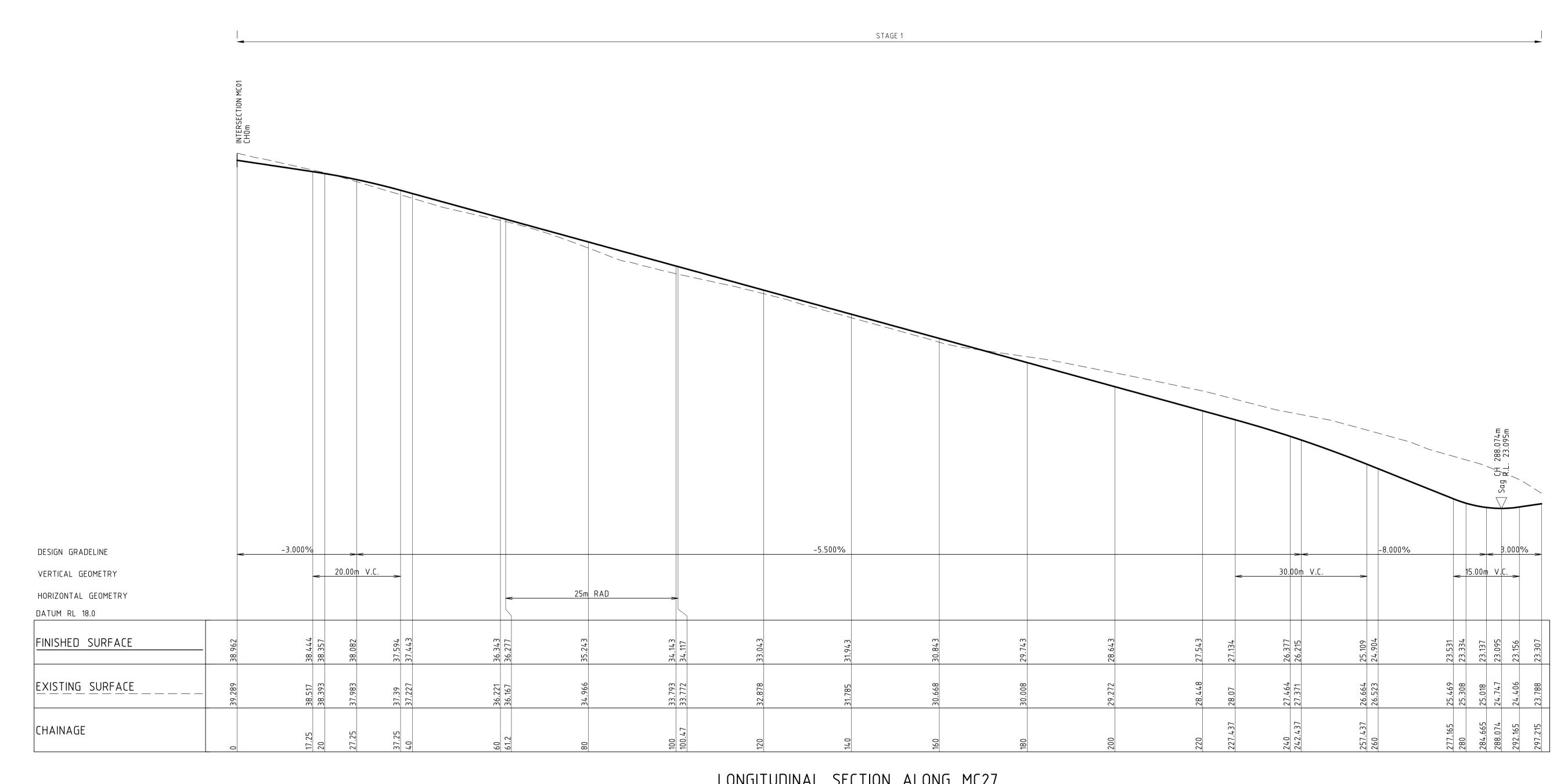
MASTERPLANNING DA

CIVIL ENGINEERING PACKAGE

ROAD LONGITUDINAL SECTIONS -SHEET 35

JOB NUMBER	
NL222055-0 ⁻	1
DRAWING NUMBER	REV
MP-C05.65	(

DRAWING SHEET SIZE = A1



LONGITUDINAL SECTION ALONG MC27

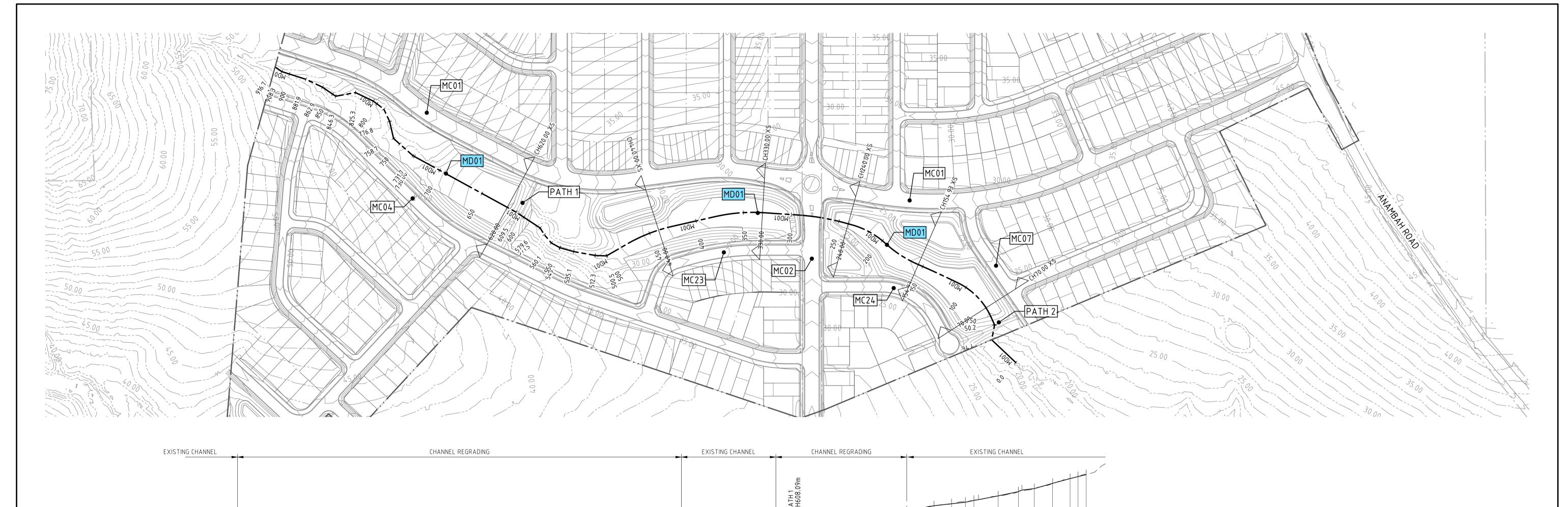
HORIZONTAL SCALE 1:500@A1

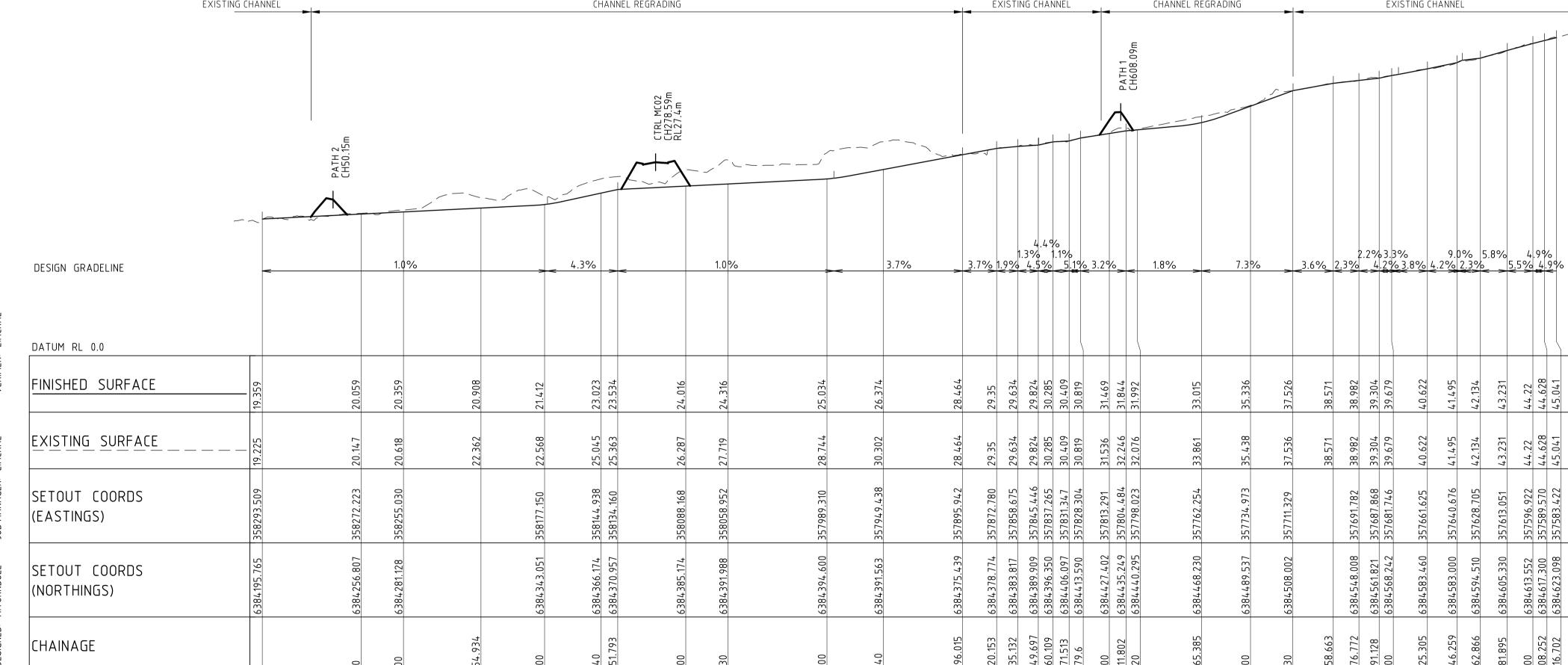
VERTICAL SCALE 1:100@A1



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A DRAFT ISSUE	JS AK 09.08.24	• •		COMMENCING WORK. NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE	NODTHOOD	PROPOSED SUBDIVISION	CIVIL ENGINEERING PACKAGE	NL222055-0 ²	1
B DRAFT ISSUE	JS AK 15.08.24	11111		USABILITY, COMPLETENESS OR SCALE OF DRAWINGS TRANSFERRED ELECTRONICALLY.	HUNITINUT	559 ANAMBAH ROAD			
C ISSUED FOR APPROVAL	JS LM AK 22.08.24	IIII U.I	maitland	THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR,	Newcastle	GOSFORTH NSW 2320		DRAWING NUMBER	REVISION
	СОМ	MUNITIES	city council	- 0 5 10 15 20 25m	Level 1, 215 Pacific Hwy, Charlestown NSW 2290		ROAD LONGITUDINAL SECTIONS -	MP-C05.66	
	DRAWING NOT	T TO BE USED FOR CONSTRUCTION	THE COPYRIGHT OF THIS DRAWING REMAINS WITH	SCALE 1:500@ A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au	MASTERPLANNING DA	SHEET 36	WIF-C03.00	
	UNLESS VERIFICA	ATION SIGNATURE HAS BEEN ADDED	NORTHROP CONSULTING ENGINEERS PTY LTD	SCALE 1:100 @ A1	ABN 81 094 433 100	MAGTERI EARRING DA		DRAWING SHEET SIZE = A1	<u>1</u>
Date: 22.08.2024 4:55 PM Plotted By: ANDREW KILLEN Found: O:\5 Pre-July 24 Projects\1	siNewcastleIYEAR 2022 JobsiNL222055-01 - 559 Anambah Road, GosforthIO - DrawingsiCIVILI03-CADIMP-MASTERPLANINL222055-01-MP-C	-C05.31-LONG SECTIONS.dwg						•	





LONGITUDINAL SECTION ALONG MD01

HORIZONTAL SCALE 1:2000@A1 VERTICAL SCALE 1:400@A1

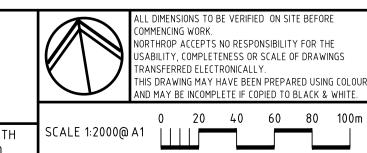


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В	DRAFT ISSUE	JS		AK	09.08.24		·	
С	DRAFT ISSUE	JS		AK	15.08.24			I
D	ISSUED FOR APPROVAL	JS	LM	AK	22.08.24		СО	М
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PROPOSED SUBDIVISION **559 ANAMBAH ROAD GOSFORTH NSW 2320**

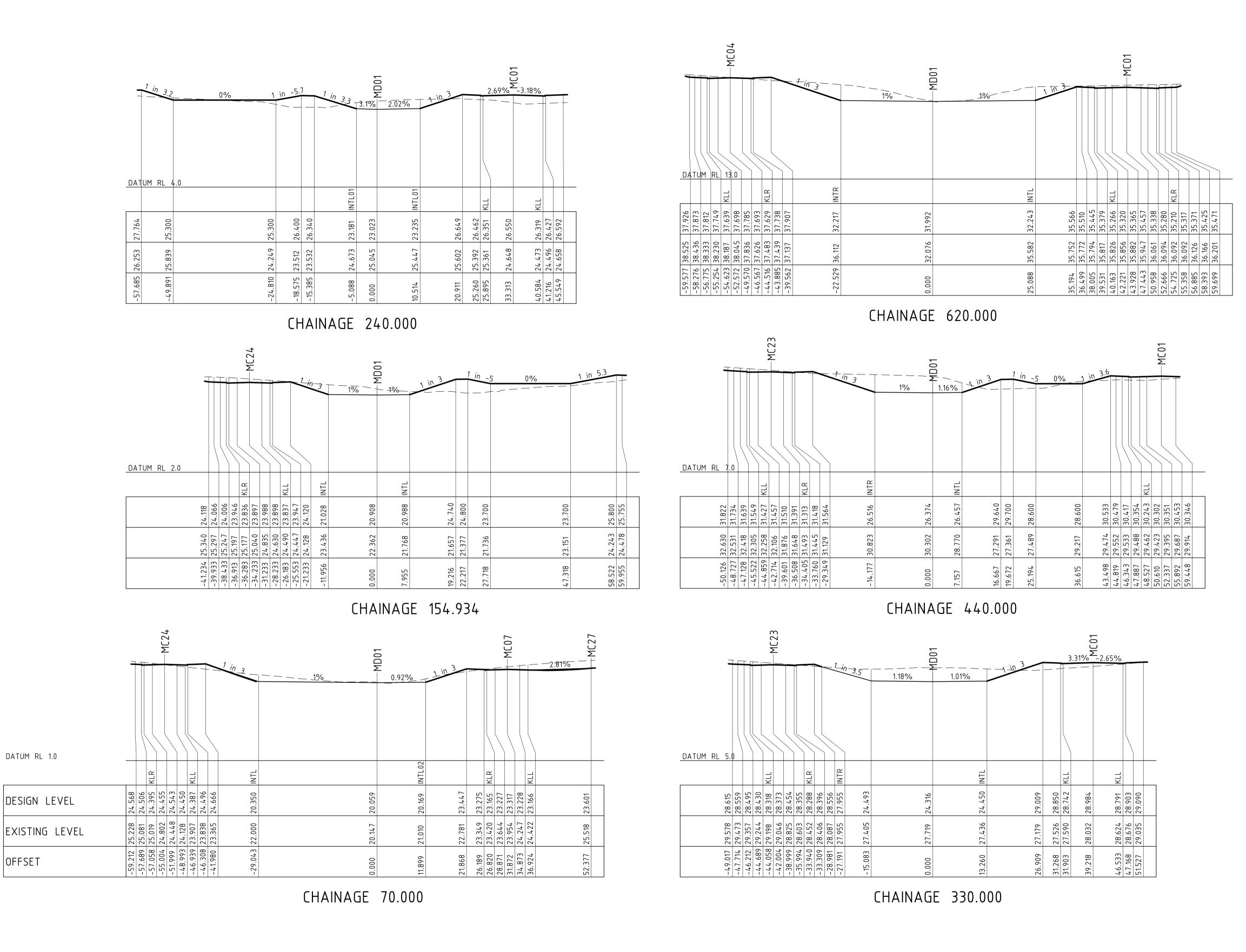
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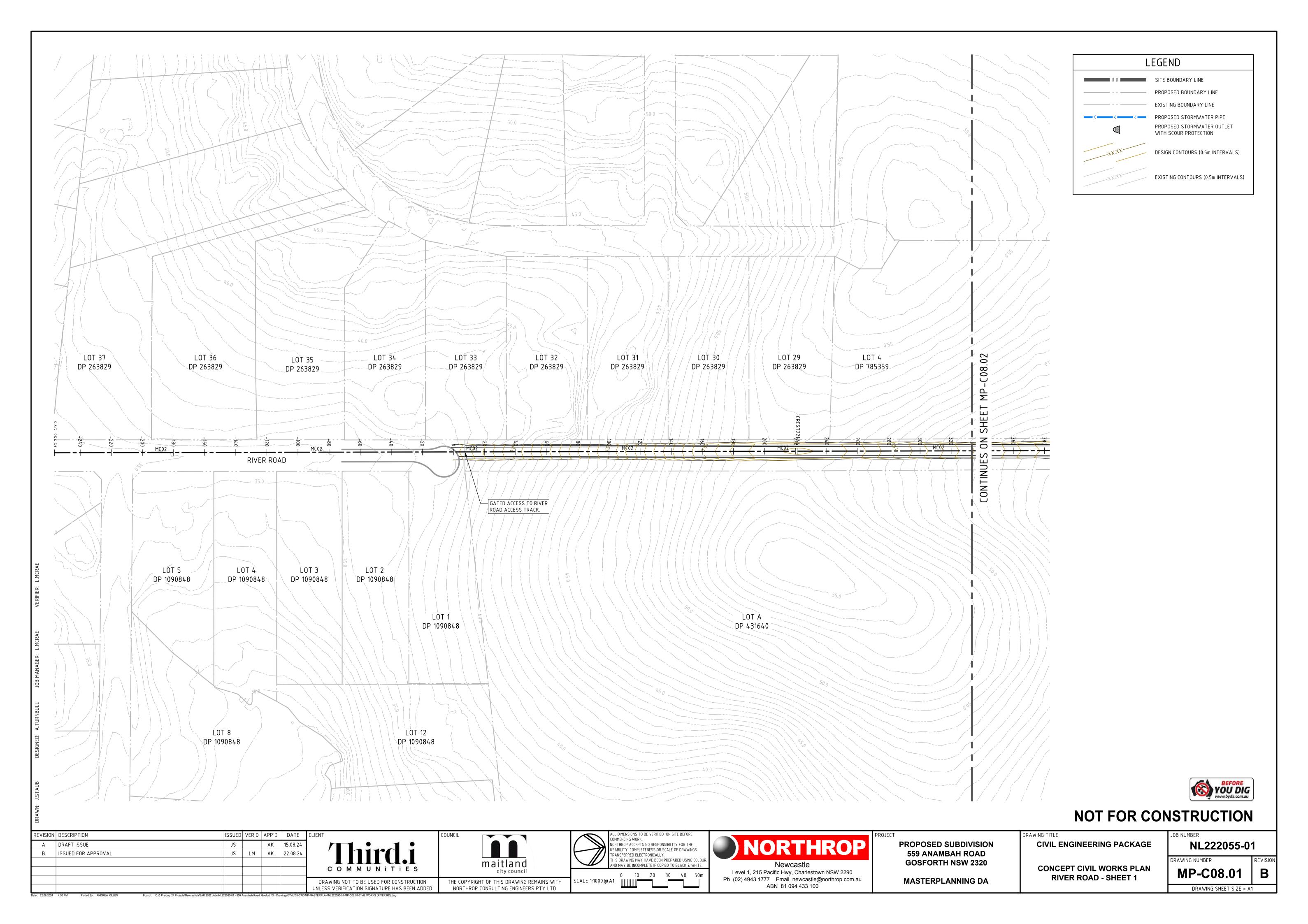


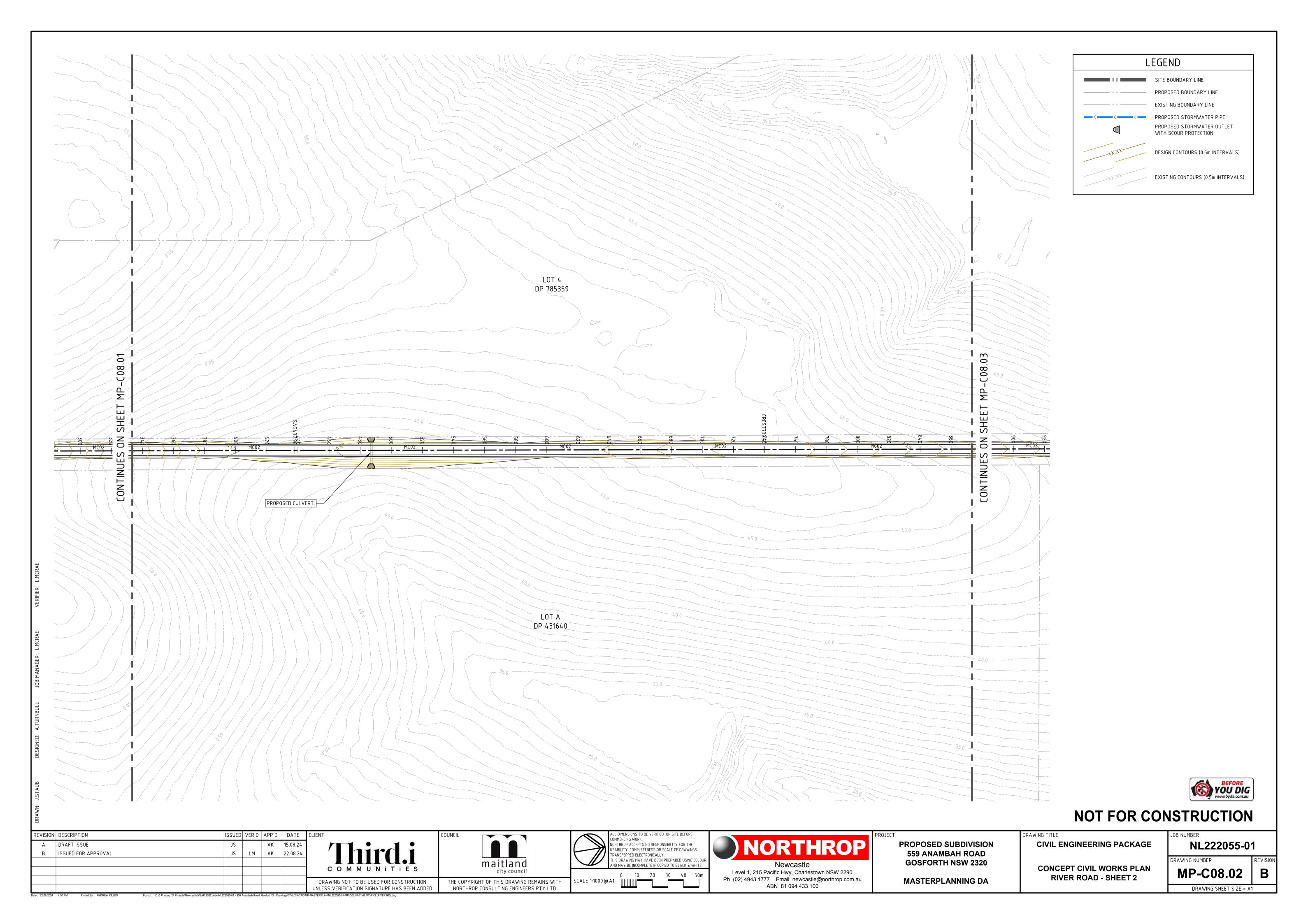
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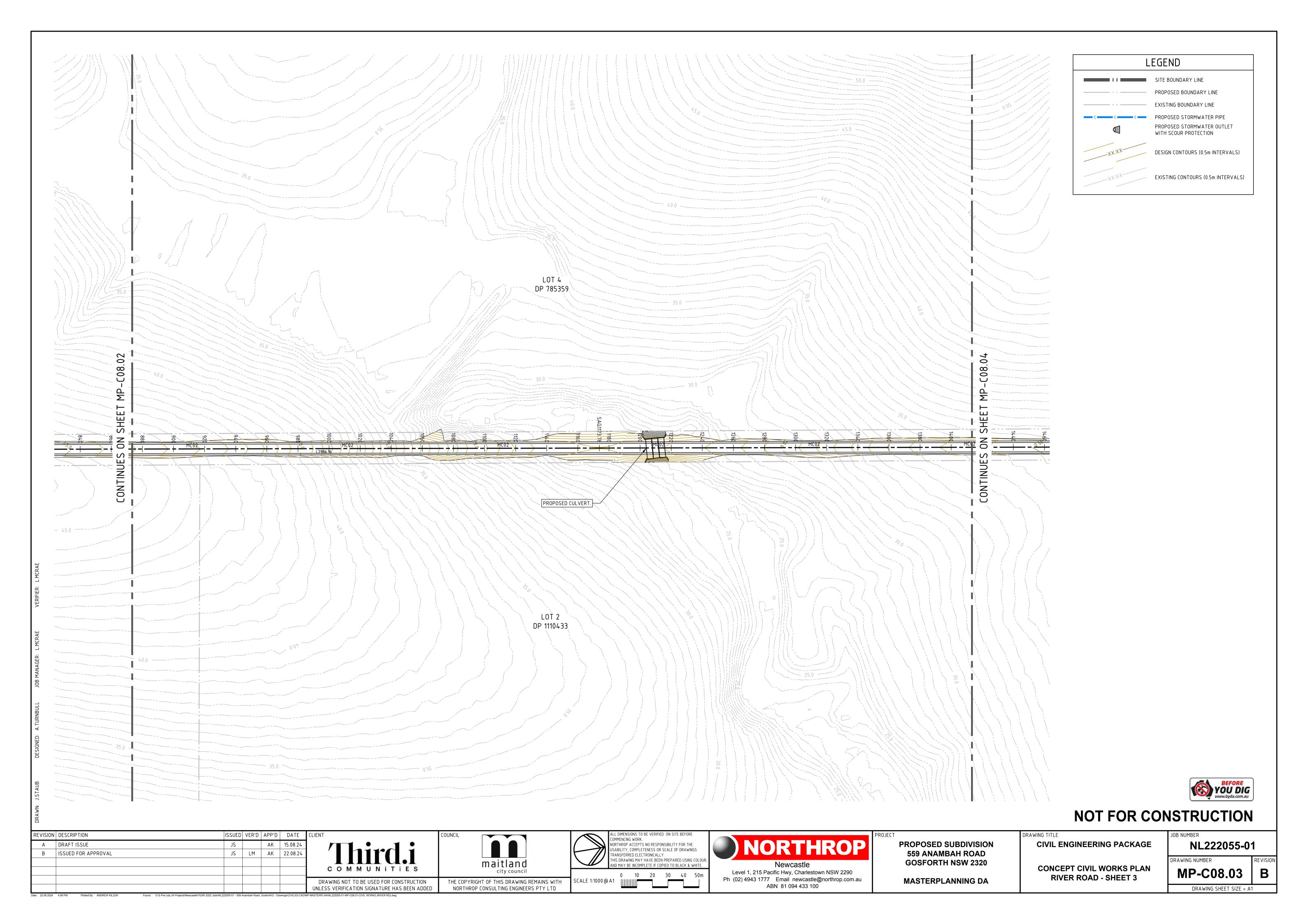
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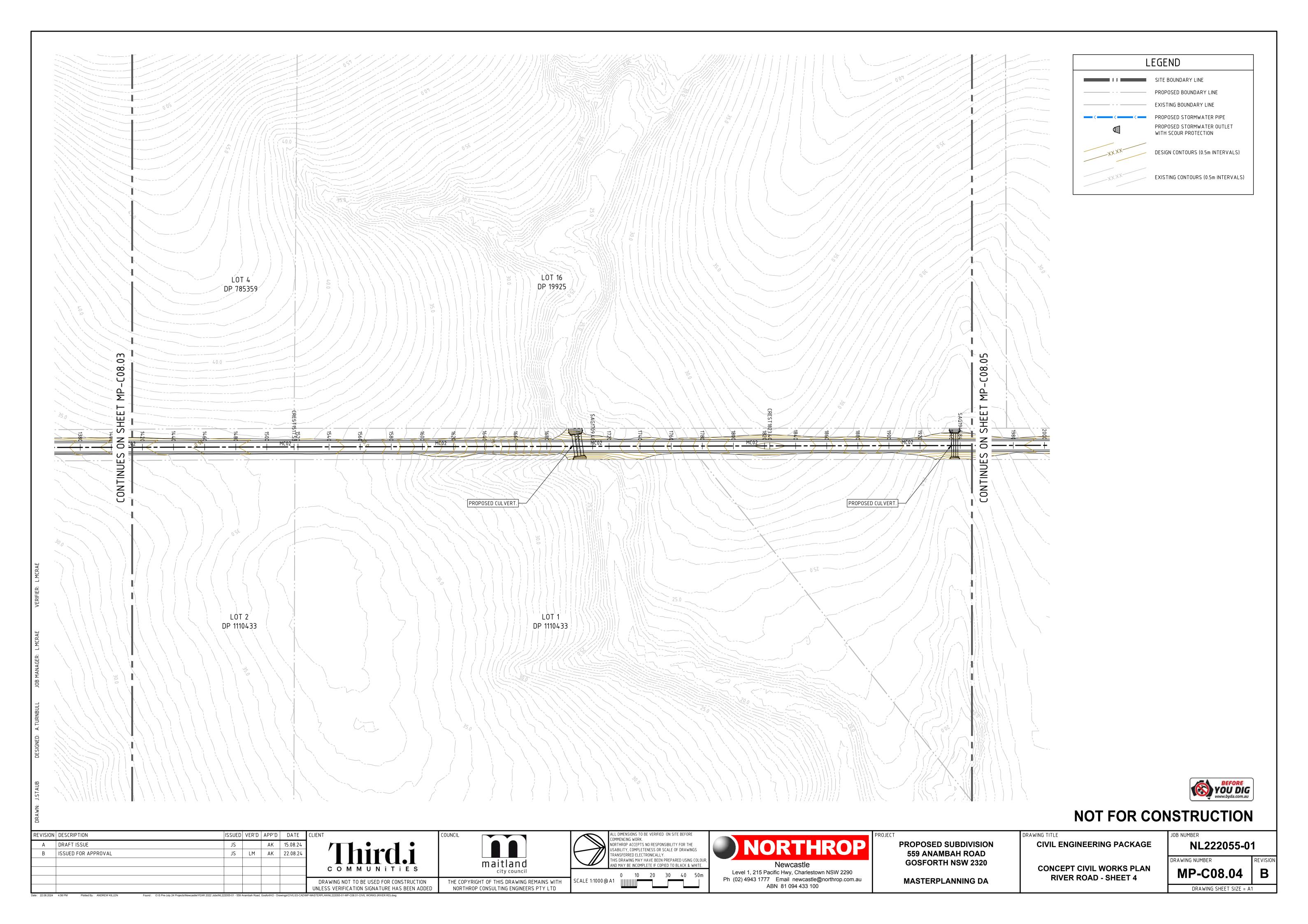
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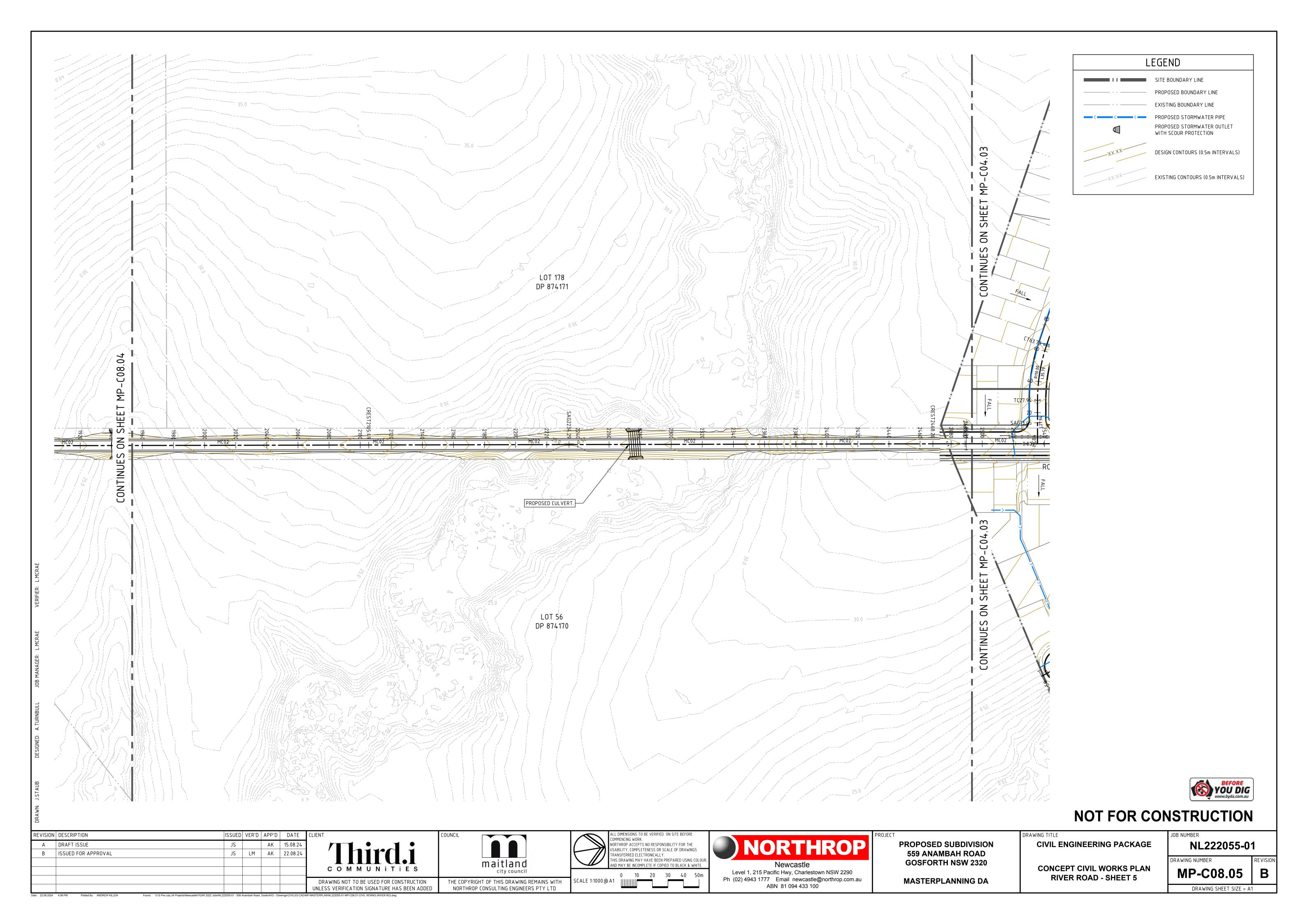
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LM AK 22.08.24	COMMUNITIES	city council	0 20 40 60 80 100m	Level 1, 215 Pacific Hwy, Charlestown NSW 2290		CREEK CROSS SECTIONS	MP-C06.11 D
	DRAWING NOT TO BE USED FOR CONSTRUCTION	THE COPYRIGHT OF THIS DRAWING REMAINS WITH	SCALE 1:2000@ A1	Ph (02) 4943 1777 Email newcastle@northrop.com.au	MASTERPLANNING DA		WII 300:11 B
	UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED	NORTHROP CONSULTING ENGINEERS PTY LTD		ABN 81 094 433 100			DRAWING SHEET SIZE = A1
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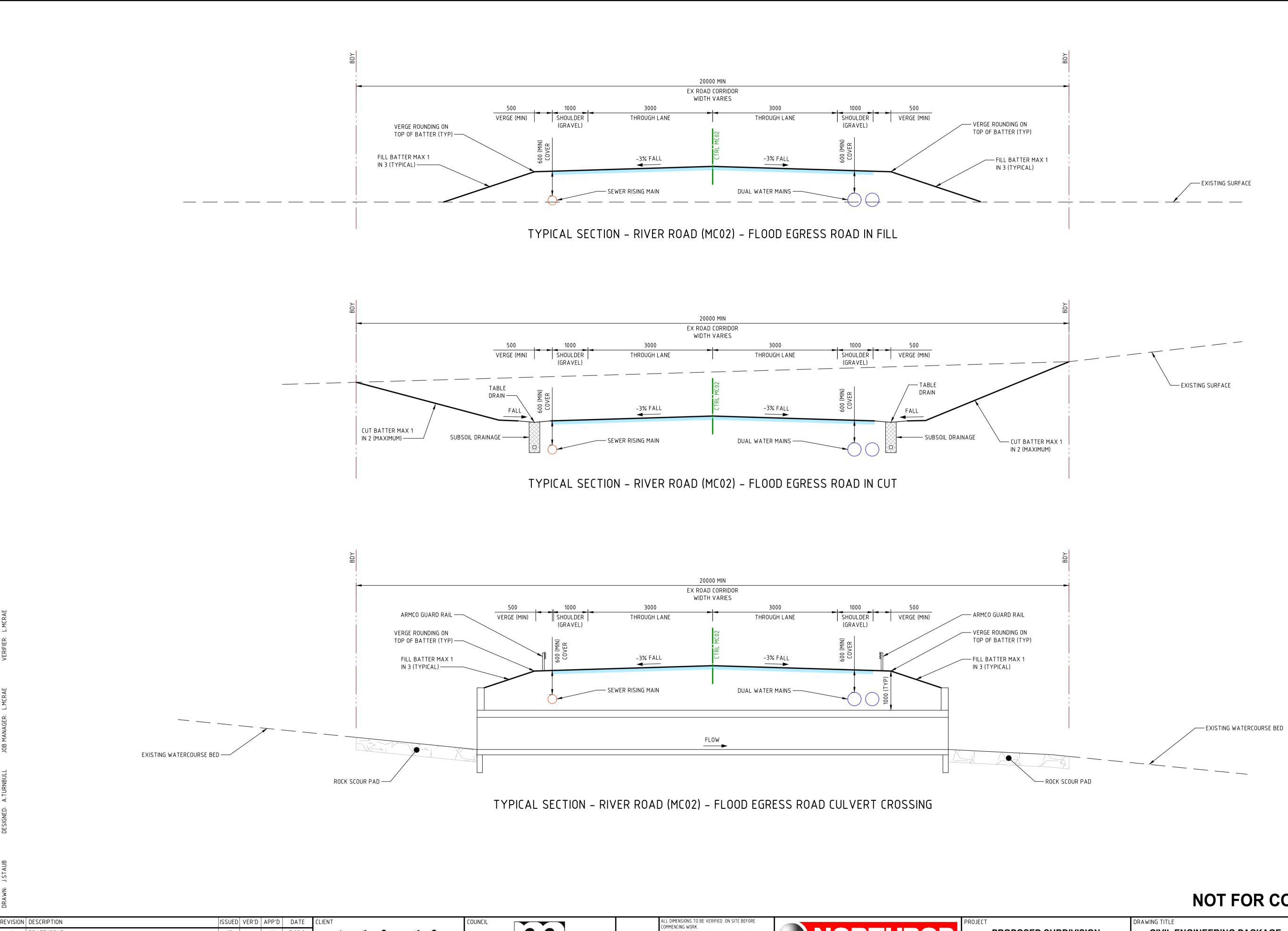








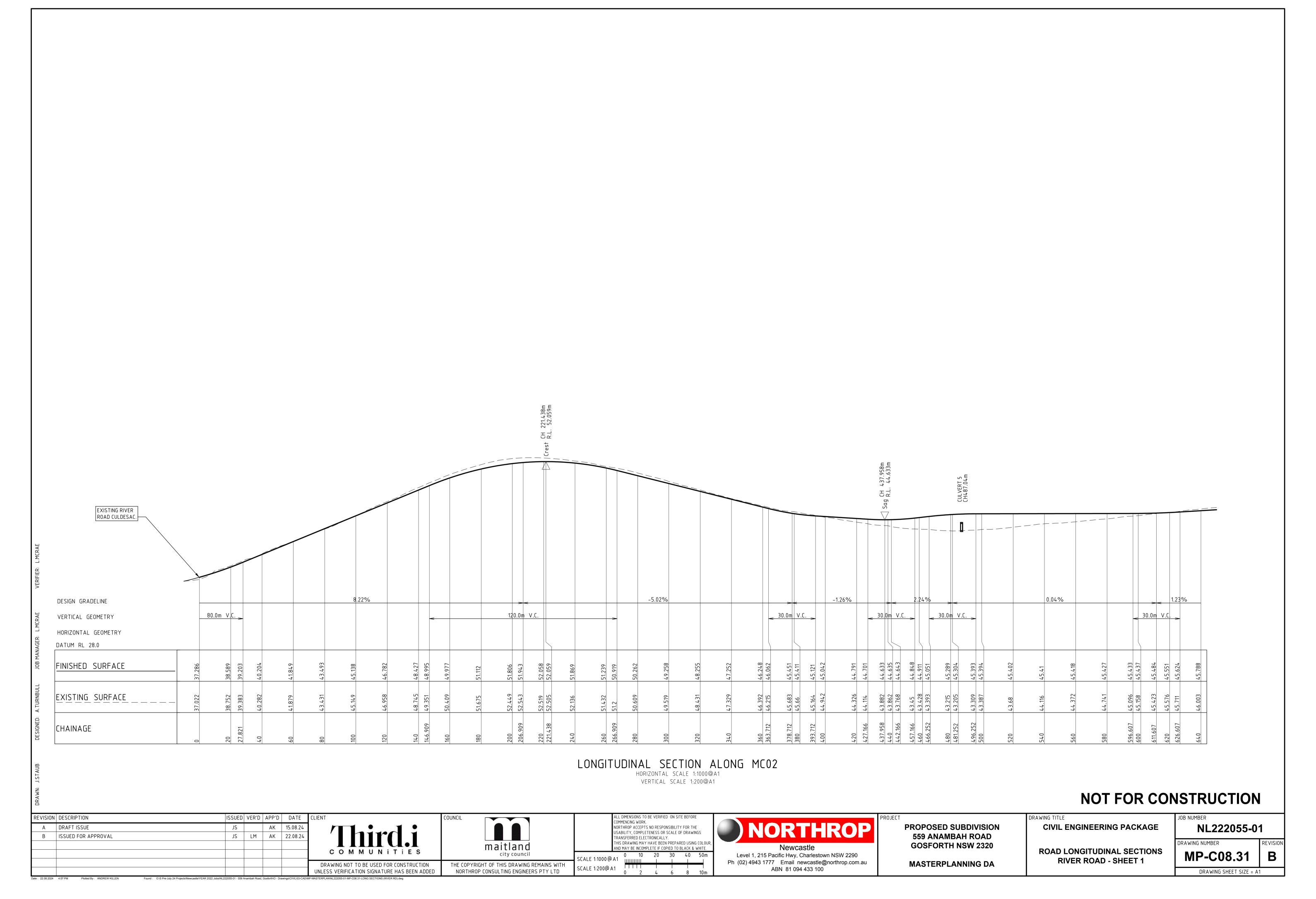


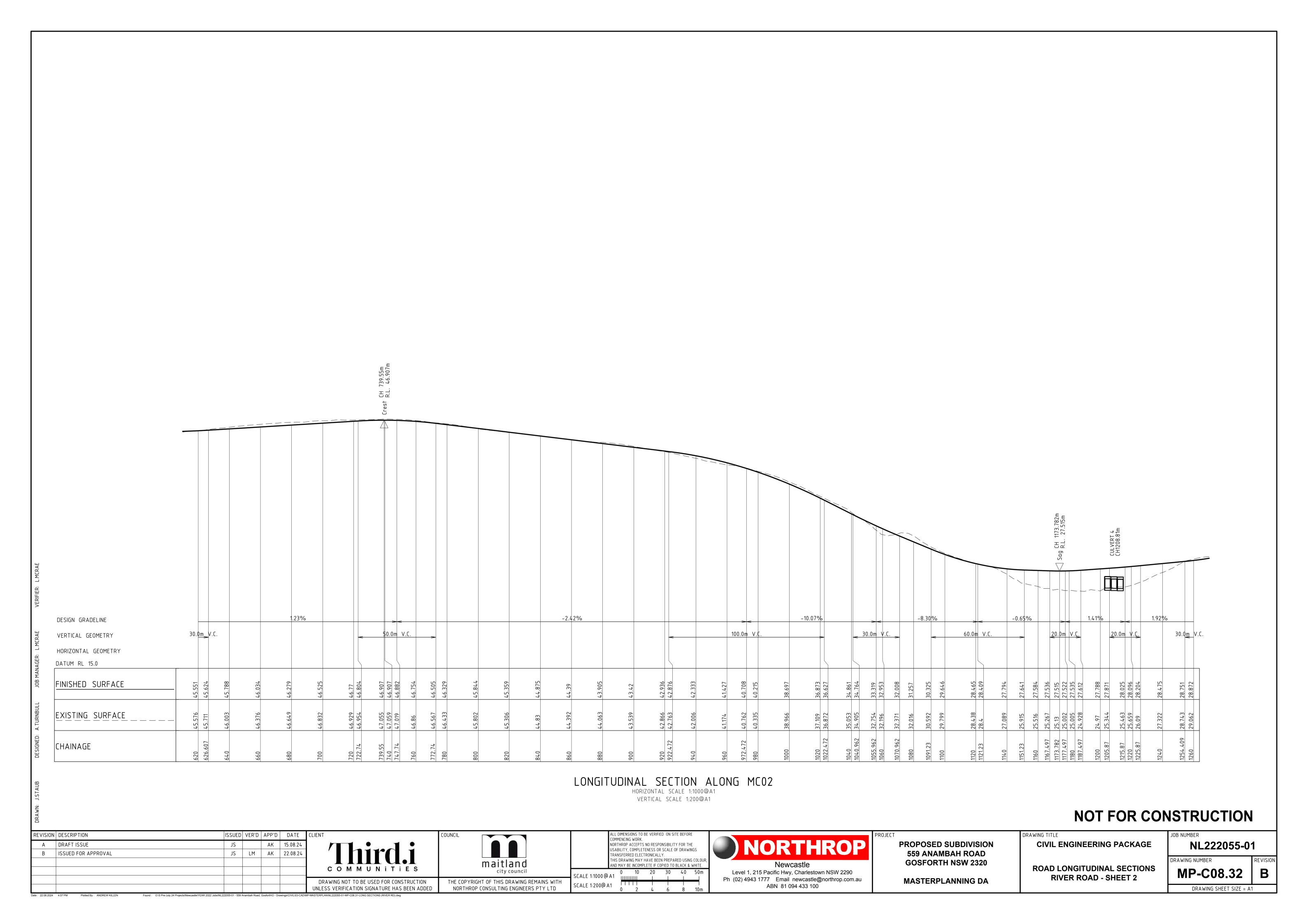


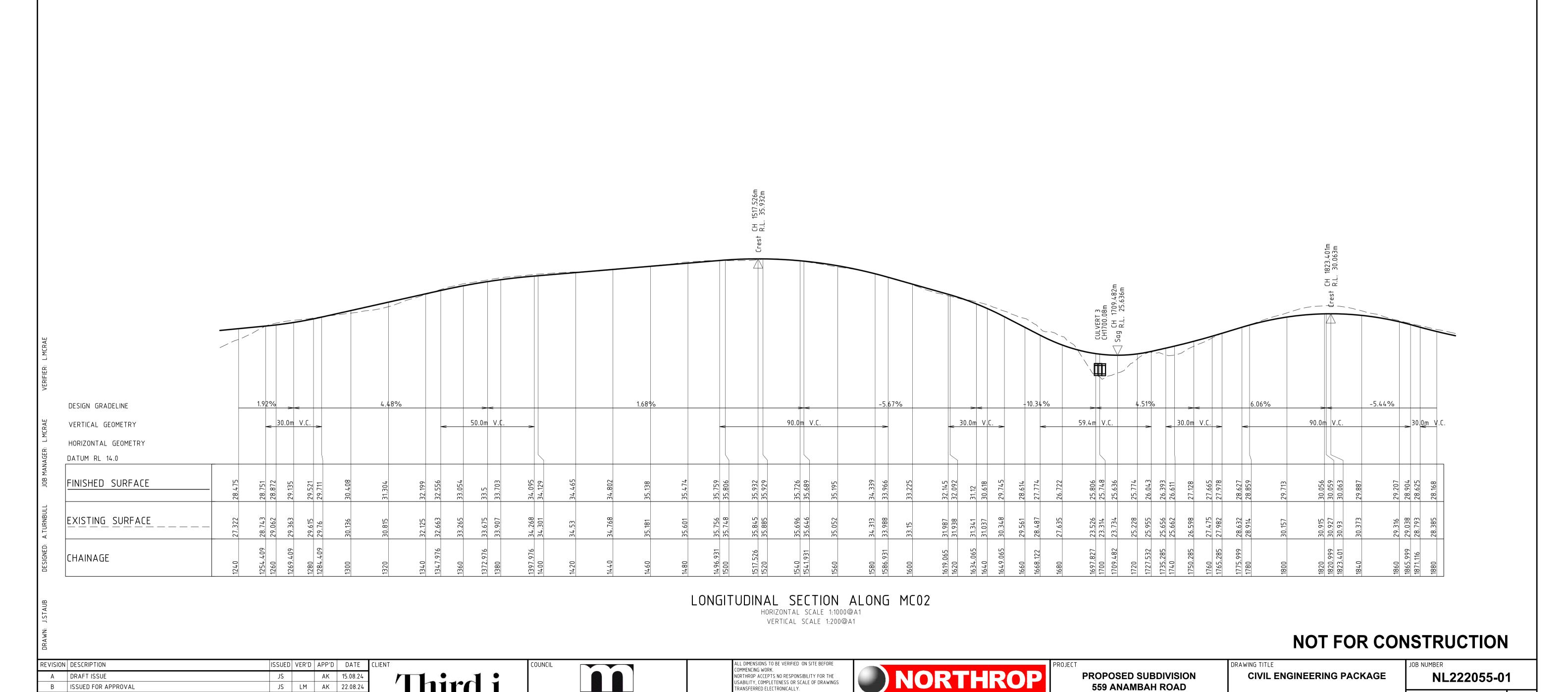
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PROPOSED SUBDIVISION **CIVIL ENGINEERING PACKAGE** NL222055-01 NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE AK 15.08.24 A DRAFT ISSUE SABILITY, COMPLETENESS OR SCALE OF DRAWINGS **559 ANAMBAH ROAD** JS LM AK 22.08.24 B ISSUED FOR APPROVAL TRANSFERRED ELECTRONICALLY. THIS DRAWING MAY HAVE BEEN PREPARED USING COLOUR AND MAY BE INCOMPLETE IF COPIED TO BLACK & WHITE. DRAWING NUMBER **GOSFORTH NSW 2320** maitland city council Newcastle **ROAD TYPICAL SECTIONS** MP-C08.21 В Level 1, 215 Pacific Hwy, Charlestown NSW 2290 **RIVER ROAD** Ph (02) 4943 1777 Email newcastle@northrop.com.au SCALE 1:50@ A1 MASTERPLANNING DA DRAWING NOT TO BE USED FOR CONSTRUCTION THE COPYRIGHT OF THIS DRAWING REMAINS WITH ABN 81 094 433 100 DRAWING SHEET SIZE = A1 UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED NORTHROP CONSULTING ENGINEERS PTY LTD







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SCALE 1:200@ A1

maitland city council

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ABN 81 094 433 100

DRAWING NUMBER

MP-C08.33

DRAWING SHEET SIZE = A1

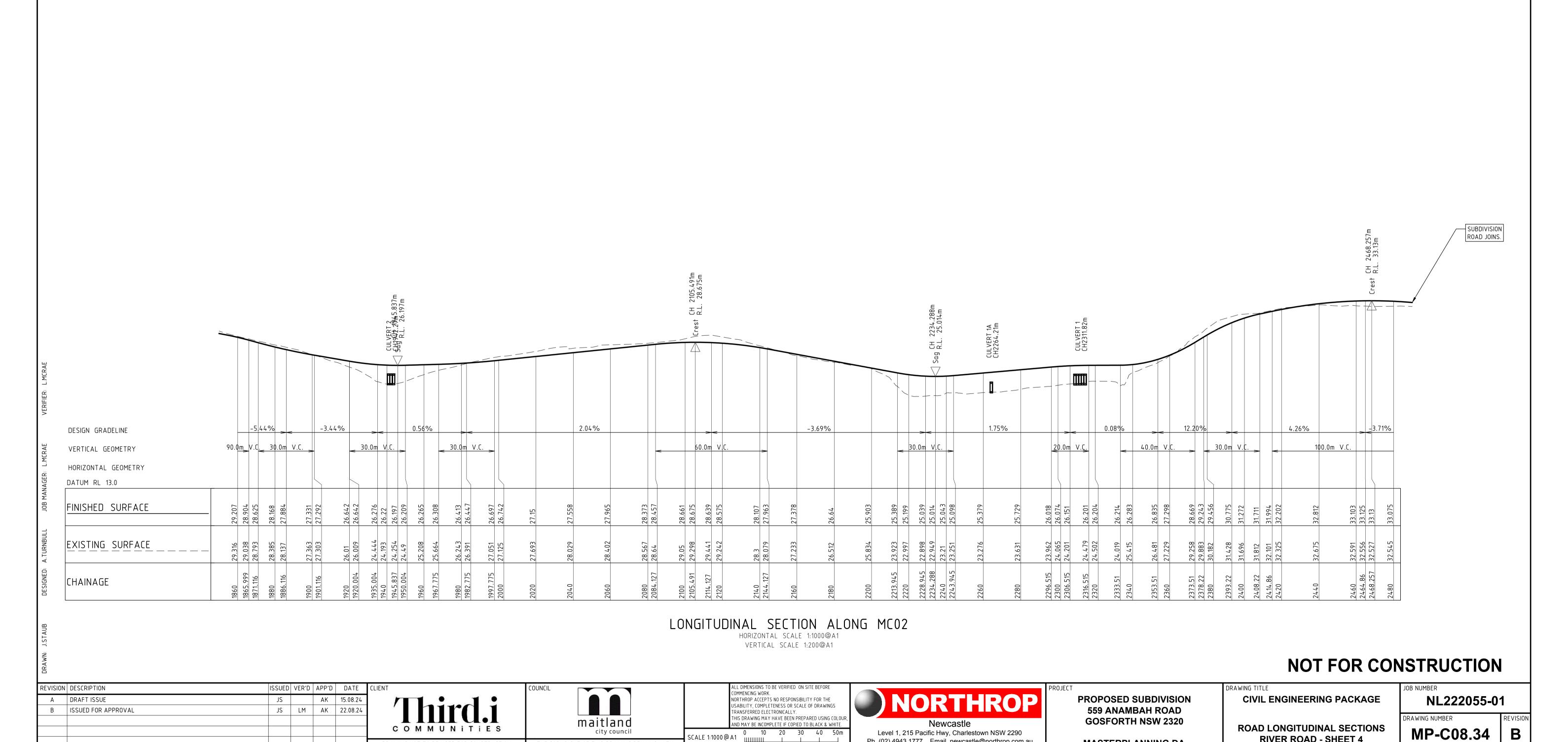
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ROAD LONGITUDINAL SECTIONS

RIVER ROAD - SHEET 3

GOSFORTH NSW 2320

MASTERPLANNING DA



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RIVER ROAD - SHEET 4

DRAWING SHEET SIZE = A1

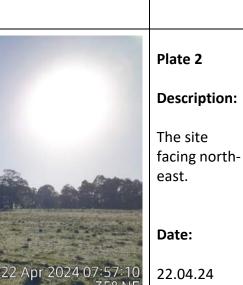
MASTERPLANNING DA



Appendix B







12 Benjamin Circle Rutherford

City of Maitland New South Wales EP3627 Plate 1

Date:

22.04.24

Description:

Looking west from the TP01-L location.





Description:

The site facing east.

Date:

22.04.24



Plate 4

Description:

The site facing south.

Date:





Description:

The site facing north.

Date:

22.04.24



Plate 6

Description:

Looking west from the TP12-P location.

Date:





Description:

The site facing south.

Date:

23.04.24

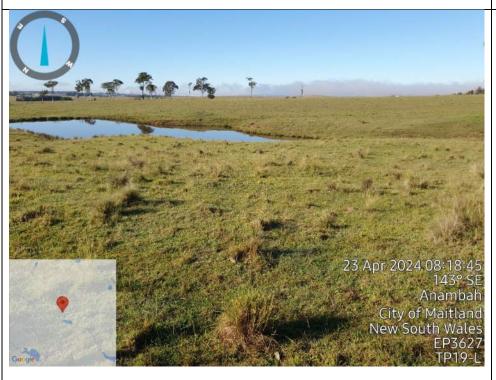


Plate 8

Description:

Water dam close to

TP19-L

Date:





Description:

The site facing east.

Date:

17.04.24



Plate 10

Description:

The site facing south.

Date:





Description:

Rock outcrops on top of the hill.

Date:

17.04.24



Plate 12

Description:

Erosion scarps on site.

Date:





Description:

The site facing northeast.

Date:

17.04.24



Plate 14

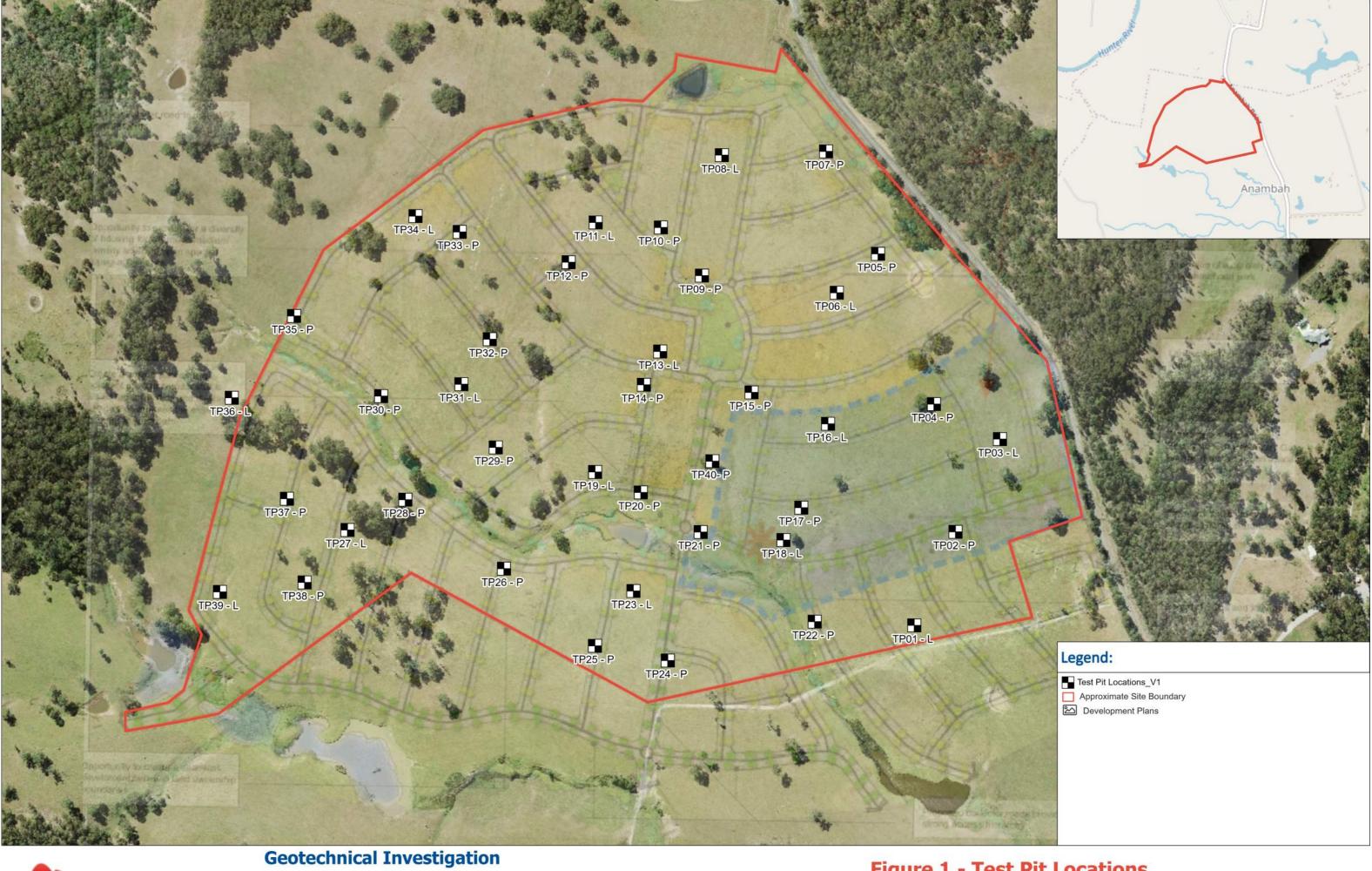
Description:

Water ponding on the surface.

Date:



Appendix C GEOTECHNICAL INVESTIGATION LOCATIONS





559 Anambah Road, Gosforth NSW, Australia

Job No: EP3627 Date: 14-05-2024 Version: draft



0 50 m 100 m Approximate Scale Only

Figure 1 - Test Pit Locations

Coordinate System: WGS 84 Drawn By: MC Checked By: OP Scale of regional map not shown
Source: © Department of Finance, Services & Innovation 2018





Appendix D



Soil Logging Symbols

CLAYS

CLAY



silty CLAY



sandy CLAY



gravelly CLAY

SILTS



SILT



clayey SILT



sandy SILT



gravelly SILT

SANDS



SAND



clayey SAND



silty SAND



gravelly SAND

GRAVELS



GRAVEL



clayey GRAVEL



silty GRAVEL



sandy GRAVEL

SEDIMENTARY ROCK



SANDSTONE



SILTSTONE



SHALE



CONGLOMERATE

FILL



FILL



CONCRETE



ASPHALT

GROUNDWATER WELL SYMBOLS



WELL SCREEN



CASING - filter pack



CASING – backfill



CASING – bentonite seal



CASING – grout seal



BACKFILL

OTHER



TOPSOIL - sandy SILT



TOPSOIL – highly organic

Rock Description Explanation Sheet (1 of 2)

Weathering Condition (Degree of Weathering):

The degree of weathering is a continuum from fresh rock to soil. Boundaries between weathering grades may be abrupt or gradational.

Rock Material Weathering Classification				
Weathering Grade	Symbol	Definition		
Residual Soil	RS	Soil-like material developed on extremely weathered rock; the mass structure and substance fabric are no longer evident; there is a large change in volume, but the material has not been significantly transported.		
Extremely Weathered Rock	XW	Rock is weathered to such an extent that it has 'soil' properties, i.e. it either disintegrates or can be remoulded in water, but substance fabric and rock structure still recognisable.		
Highly Weathered Rock	HW	Strong discolouration is evident throughout the rock mass, often with significant change in the constituent minerals. The intact rock strength is generally much weaker than that of the fresh rock.		
Moderately Weathered Rock	MW	Modest discolouration is evident throughout the rock fabric, often with some change in the constituent minerals. The intact rock strength is usually noticeably weaker than that of the fresh rock.		
Slightly Weathered Rock	SW	Rock is slightly discoloured but shows little or no change of strength from fresh rock.		
Fresh Rock	FR	Rock shows no sign of decomposition or staining.		

Notes:

- 1. Minor variations within broader weathering grade zones will be noted on the engineering borehole logs.
- 2. Extremely weathered rock is described in terms of soil engineering properties.
- 3. Weathering may be pervasive throughout the rock mass or may penetrate inwards from discontinuities to some extent.
- 4. The 'Distinctly Weathered (DW)' class as defined in AS1726-2017 is divided to incorporate HW and MW in the above table. The symbol DW should not be used.

Strength Condition (Intact Rock Strength):

Strength of Rock Material

(Based on Point Load Strength Index, corrected to 50mm diameter $-I_{s(50)}$. Field guide used if no tests available. Refer to AS 4133.4.1-2007.

Term	Symbol	Point Load Index (MPa)		Field Guide to Strength			
		I _{s(50)}		Material crumbles under firm blows with sharp end of pick; can be peeled with			
Very Low	VL	>0.03	≤0.1	knife; too hard to cut a triaxial sample by hand. Pieces up to 3cm thick can be broken by finger pressure.			
Low	L	>0.1	≤0.3	Easily scored with a knife; indentations 1mm to 3mm show in the specimen with firm blows of the pick point; has dull sound under hammer. A piece of core 150mm long by 50mm diameter may be broken by hand. Sharp edges of core may be friable and break during handling.			
Medium	М	>0.3	≤1.0	Readily scored with a knife; a piece of core 150mm long by 50mm diameter can be broken by hand with difficulty.			
High	н	>1	≤3	A piece of core 150mm long by 50mm diameter cannot be broken by hand but can be broken by a pick with a single firm blow; rock rings under hammer.			
Very High	VH	>3	≤10	Hand specimen breaks with pick after more than one blow; rock rings under hammer.			
Extremely High EH >10			Specimen requires many blows with geological pick to break through intact material; rock rings under hammer.				

Notes:

- 1. These terms refer to the strength of the rock material and not to the strength of the rock mass which may be considerably weaker due to the effect of rock defects.
- ${\bf 2.} \quad {\bf Anisotropy} \ {\bf of} \ {\bf rock} \ {\bf material} \ {\bf samples} \ {\bf may} \ {\bf affect} \ {\bf the} \ {\bf field} \ {\bf assessment} \ {\bf of} \quad {\bf strength}.$
- 3. Extremely Low Strength ('EL') is now not considered a description of rock strength in line with the updated AS1726-2017 as by definition EL rock should be described in terms of soil properties.

Rock Description Explanation Sheet (2 of 2)

Discontinuity Description: Refer to AS1726-2017, Table A10.

Discontinuity Description: Refer to								
Anisot	Anisotropic Fabric							
BED	Bedding							
FOL	Foliation							
LIN	Mineral lineation							
Defect	Туре							
LP	Lamination Parting							
Pt	Bedding Parting							
FP	Cleavage / Foliation Parting							
Jt	Joint							
SZ	Sheared Zone							
CZ	Crushed Zone							
BZ	Broken Zone							
HFZ	Highly Fractured Zone							
AZ	Alteration Zone							
VN	Vein							

Roughness (e.g. Planar, Smooth is abbreviated Pln / Sm) Class				
		Rough or irregular (R or	Irr)	I
Stepped (Stp)		Smooth (Sm)		П
		Slickensided (SI)		Ш
		Rough (R)		IV
Undulating (Ur	1)	Smooth (Sm)		٧
		Slickensided (SI)		VI
		Rough (R)		VII
Planar (Pln)		Smooth (Sm)		VIII
		Slickensided (SI)		IX
Aperture	Infilling			
Closed CD	No visible	No visible coating or infill Clean		
Open OP	Surfaces di	Surfaces discoloured by mineral/s Stain		
Filled FL	Visible mir	Visible mineral or soil infill <1mm		
Tight TI	t TI Visible mineral or soil infill >1mm Coating			Ct

Other			
Clay	Clay		
Fe	Iron		
Co	Coal		
Carb	Carbonaceous		
Sinf	Soil Infill Zone		
Qz	Quartz		
Ca	Calcite		
Chl	Chlorite		
Ру	Pyrite		
Int	Intersecting		
Inc	Incipient		
DI	Drilling Induced		
Н	Horizontal		
V	Vertical		

Note: Describe 'Zones' and 'Coatings' in terms of composition and thickness (mm).

Discontinuity Spacing: On the geotechnical borehole log, a graphical representation of defect spacing vs depth is shown. This representation takes into account all the natural rock defects occurring within a given depth interval, excluding breaks induced by the drilling / handling of core. Refer to AS1726-2017, BS5930-1999.

D	efect Spacing		Bedding Thickness (Sedimentary Rock Stratification)			
Spacing/Width (mm)	Descriptor	Symbol	Descriptor	Spacing/Width (mm)		
			Thinly Laminated	< 6		
<20	Extremely Close	EC	Thickly Laminated	6 – 20		
20 – 60	Very Close VC		Very Thinly Bedded	20 – 60		
60 – 200	Close	С	Thinly Bedded	60 – 200		
200 – 600	600 Medium M		Medium Bedded	200 – 600		
600 – 2000	600 – 2000 Wide W		Thickly Bedded	600 – 2000		
2000 – 6000	Very Wide	VW	Very Thickly Bedded	> 2000		
>6000	Extremely Wide	EW				

Defect Spacing in 3D				
Term	Description			
Blocky	Equidimensional			
Tabular	Thickness much less than length or width			
Columnar	Height much greater than cross section			

Defect Persistence					
(areal extent)					
Trace length of defect given in					
metres					

Symbols: The list below provides an explanation of terms and symbols used on the geotechnical borehole, test pit and penetrometer logs.

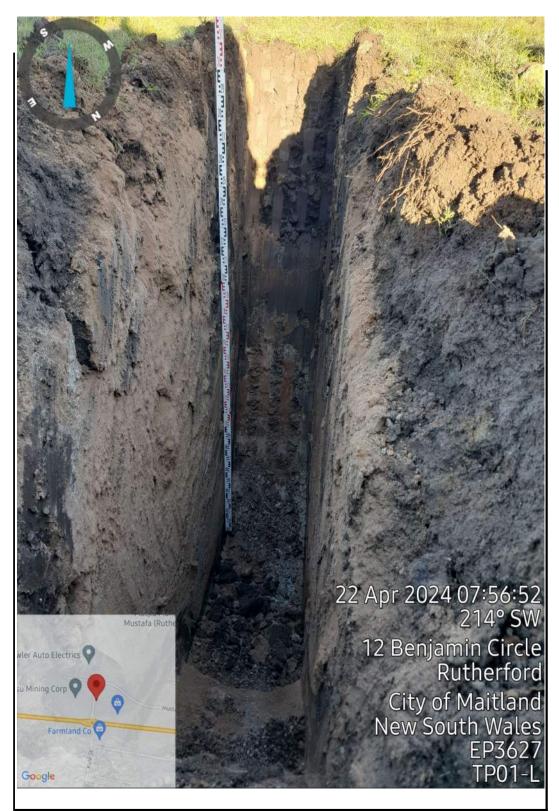
	Test Results					Test Symbols
PI	Plasticity Index	c′	Effective Cohesion		DCP	Dynamic Cone Penetrometer
LL	Liquid Limit	Cu	Undrained Cohesion		SPT	Standard Penetration Test
LI	Liquidity Index	C'R	Residual Cohesion		СРТи	Cone Penetrometer (Piezocone) Test
DD	Dry Density	φ′	Effective Angle of Internal Friction		PANDA	Variable Energy DCP
WD	Wet Density	фи	Undrained Angle of Internal Friction		PP	Pocket Penetrometer Test
LS	Linear Shrinkage	φ′ _R	Residual Angle of Internal Friction		U50	Undisturbed Sample 50 mm (nominal diameter)
МС	Moisture Content	Cv	Coefficient of Consolidation		U100	Undisturbed Sample 100mm (nominal diameter)
oc	Organic Content	m_{ν}	Coefficient of Volume Compressibility		UCS	Uniaxial Compressive Strength
WPI	Weighted Plasticity Index	Cαε	Coefficient of Secondary Compression		Pm	Pressuremeter
WLS	Weighted Linear Shrinkage	е	Voids Ratio		FSV	Field Shear Vane
DoS	Degree of Saturation	ϕ'_{cv}	Constant Volume Friction Angle		DST	Direct Shear Test
APD	Apparent Particle Density	q _t / q _c	Piezocone Tip Resistance (corrected / uncorrected)		PR	Penetration Rate
Su	Undrained Shear Strength	\mathbf{q}_{d}	PANDA Cone Resistance		PLI	Point Load Index Test (axial)
qu	Unconfined Compressive Strength	I _{s(50)}	I _{s(50)} Point Load Strength Index		D	Point Load Test (diametral)
TCR	Total Core Recovery	RQD	Rock Quality Designation		L	Point Load Test (irregular lump)

Groundwater level	- Water Inflow	Water Outflow
-------------------	----------------	---------------

Engineering Log - Test Pit

SHEET 1 OF 1

	Client Thirdi Group c/- Vara Consulting									Project No. EP3627						
Project Thirdi					irdi (Gosforth Anambah Rd					Logged By AN					
	Location 559 Anambah Rd, Gosforth NSW 2320										Checked By OP					
	Started Excavation 22.4.24 Northing 6384280.00 Slope Completed Excavation 22.4.24 Easting 358404.00 Bearing									90° Equipment 23T Excavator Ground Level 29 AHD						
EX	EXCAVATION MATERIAL DESCRIPTION										TESTING, SAMPLING & OTHER INFORMATION					
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		Descri (soil type: p colour and c		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Ε	Additional Comments (material origin, pocket penetrometer values, investigation observations)			
		-		W.W.	CL- CI	TOPSOIL: Silty	CLAY: low to med	lium plasticity, black, grey				0		TOPSOIL		
		-	- - -		CI- CH	Silty CLAY: med	dium to high plasti	city, grey		~PL	VS to F	1		SLOPE WASH		
d by Datgel		- - 28 -	1		CI- CH	Silty CLAY: med	y CLAY: medium to high plasticity, g	city, grey, brown, red				5 5 8 8	4 5 5 U50 8 8	RESIDUAL SOIL		
EP LIB US-GIEL LOG CW NON-CORED BOREHOLE LOG EP3827 I HIRDI GOSFOR IH ANAMBAH RU U.1 AN GPJ <-GJRWINGFII6>> ZZUSZUZ4 15.04 10.03.00.09 Developed by Jarge				CI	Extremely weathered Sandstone r plasticity, grey, brown and red, fine coarse grained, subangular gravel (50-100mm) Test Pit TP01-L Terminated at 3.0	e to coarse grained sand, with and ferruginous cementations	vith fine to	<pl< td=""><td>Н</td><td>15 17</td><td>В</td><td>EXTREMELY WEATHERED ROCK Target depth</td></pl<>	Н	15 17	В	EXTREMELY WEATHERED ROCK Target depth				
EP LIB 03.541B TOO OW NON-CORED BOREHOLE LOG	Rem	- - - - - 25														





EP3627 - Thirdi Anambah Geotechnical Investigation

TP01-L

Test Pit No: TP02-P

Engineering Log - Test Pit

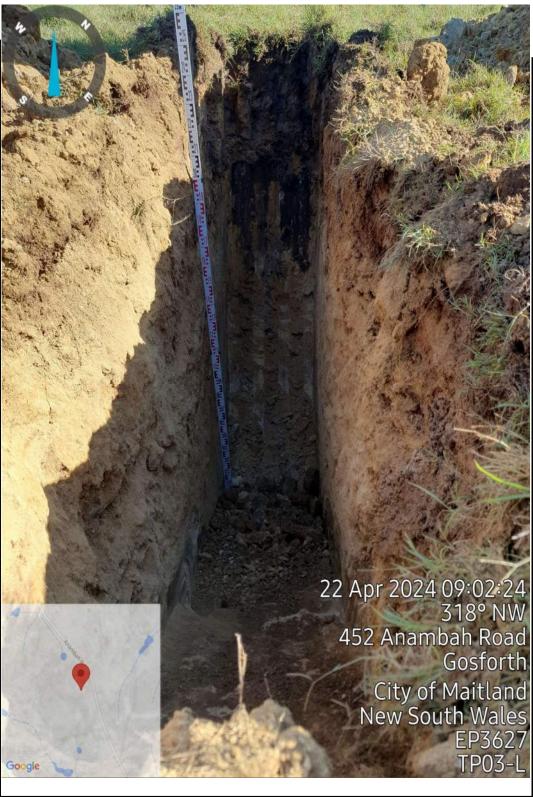
SHEET 1 OF 1

						rdi Group c/- Vara Consulting					Project No. EP3627					
	Proj Loc	ect ation				rdi Gosforth Anambah Rd) Anambah Rd, Gosforth NSW 2320					Logged By AN Checked By OP					
									Slope Bearing				quipment 23T Excavator sround Level 38 AHD			
E	EXCAVATION MATERIAL DESCRIPTION									TESTING, SAMPLING & OTHER INFORMATION						
Method	Water	RL (m)	Depth (m)		Classification		(soil type: pla	otion of Soil asticity/grainsize, her components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)		
		-	_		CL- CI	TOPSOIL: Sand medium grained		dium plasticity, dark grey, fin	e to		F	1 1		TOPSOIL		
		-	- - - - 1		CI- CH	Silty CLAY: med	Silty CLAY: medium to high plasticity, grey, brown				St to VSt	1 2		RESIDUAL SOIL		
		- 37										3 4 9 10				
EP LIB 05/G1B Log CW NON-CORED BOREHOLE LOG EP3827 THIRDI GOSFORTH ANAMBAH RD 0.1 ANI GPJ <-DrawingFile>> 22/05/2024 15/04 10/03:00:09 Developed by Daigel		-	-		CI- CH	high plasticity, gr	ered Sandstone re rey, brown and red entations (50-100r	ecovered as Sandy CLAY, m , fine to coarse grained sand nm)	edium to , with			16		EXTREMELY WEATHERED ROCK		
15:04 10:03:00:09 De		-	_							<pl< td=""><td>н</td><td></td><td></td><td></td></pl<>	н					
gFile>> 22/05/2024		36	2			Test Dit TD02 D	Terminated at 2.10) m					В	Target depth		
AN.GPJ < <drawn< td=""><td></td><td>-</td><td>_</td><td></td><td></td><td>163111111024</td><td>Terrimated at 2. Iv</td><td>, III</td><td></td><td></td><td></td><td></td><td></td><td>Target deptil</td></drawn<>		-	_			163111111024	Terrimated at 2. Iv	, III						Target deptil		
ANAMBAH KD 0.1		-	_													
HIKUI GOOFION		35	3													
LE LOG EP362/ 1		-	_													
N-COREU BOREILO		-	-													
LB LOG CW NO.	Ren	34 narks	4													
EP LIB 09.6																





Client Thirdi	Group c/- Vara Consulting		F	Project No) F	P3627
Project Thirdi	Gosforth Anambah Rd		L	ogged B	у А	.N
	nambah Rd, Gosforth NSW 2320			Checked I	-)P
Started Excavation Completed Excavation	22.4.24 Northing 6384547.00 Slope on 22.4.24 Easting 358531.00 Bearing		90°	•	uipment ound Lev	
EXCAVATION	MATERIAL DESCRIPTION	3		1		MPLING & OTHER INFORMATION
Method Water RL (m) Depth (m) Graphic Log Classification	Description of Soil (soil type: plasticity/grainsize, colour and other components)	Moisture	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
### CL-	TOPSOIL: Sandy CLAY: low to medium plasticity, grey, fine to medium grained sand	>PL		0		TOPSOIL
CI- CH	Sandy CLAY: medium to high plasticity, brown, yellow, fine to coarse grained sand	<pl< td=""><td>VS to</td><td>2 2 13 9</td><td></td><td>RESIDUAL SOIL</td></pl<>	VS to	2 2 13 9		RESIDUAL SOIL
CI-CH	Extremely weathered Sandstone recovered as Sandy CLAY, medium to high plasticity, yellow, brown, fine to coarse grained sand	<pl< td=""><td>VSt tr H</td><td>4</td><td></td><td>EXTREMELY WEATHERED ROCK DCP:-/5mm HB</td></pl<>	VSt tr H	4		EXTREMELY WEATHERED ROCK DCP:-/5mm HB
Billion Account to the process of th	Test Pit TP03-L Terminated at 2.50 m					Refusal





TP03-L

Test Pit No: TP04-P

Engineering Log - Test Pit

	Cli	ient	t		Th	irdi (Group c/- Vara	a Consulting				P	roject No	о. Е	P3627
		oje cat	ct tion				Gosforth Anar	mbah Rd losforth NSW	2320				ogged Bihecked		N OP
				Exc	avati		22.4.24	Northing	6384575.00	Slope	90			uipment	
							on 22.4.24	Easting	358435.00	Bearing		-		und Le	
E	XC	AV	ATI	ON				MATERIA	L DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	DO INCHION	Water	RL (m)	Depth (m)	1	Classification		(soil type: p colour and c	ption of Soil lasticity/grainsize, other components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
			-	_	W.W.	CL- CI	TOPSOIL: Sand medium grained	dy CLAY: low to m d sand	edium plasticity, dark grey, f	ine to	>PL		1		TOPSOIL
			_	-		CI- CH	Silty CLAY: med	dium to high plasti	city, grey, brown		~PL	F and St	2 2 3 2 5	В	RESIDUAL SOIL
			-	-		CL	Extremely west	hered Sandstone	recovered as Sandy CLAV	medium to		VSt	7 20		EXTREME! A MEVITHEDED BOOK
EP LB 05/GLB Log CW NON-CORED BOREHOLE LOG EP3627 THIRDI GOSFORTH ANAMBAH RD 0.1 AN.GPJ < <drawngfile>> 22/05/2024 15:04 10:03:00:09 Developed by Dargel</drawngfile>	1		-441 -	1		다.	high plasticity, ç	grey, brown and re	recovered as Sandy CLAY, i	medium to	<pl< td=""><td>н</td><td>20</td><td></td><td>EXTREMELY WEATHERED ROCK</td></pl<>	н	20		EXTREMELY WEATHERED ROCK
GLB LOG CW NON-CORED BOREHOLE LUG EF3627 IHIKUI GUSFURTIH ANA	Re	3	- - - - - - - - - - - - - - - - - - -	- - - - - - - - - ::			Test Pit TP04-F	PTerminated at 2.	70 m						Target depth
EP LIB 0															

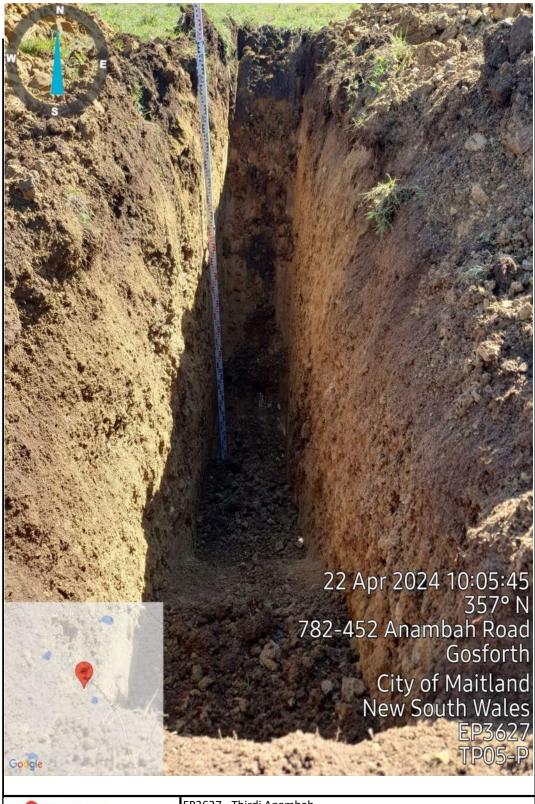




Test Pit No: TP05-P

Engineering Log - Test Pit

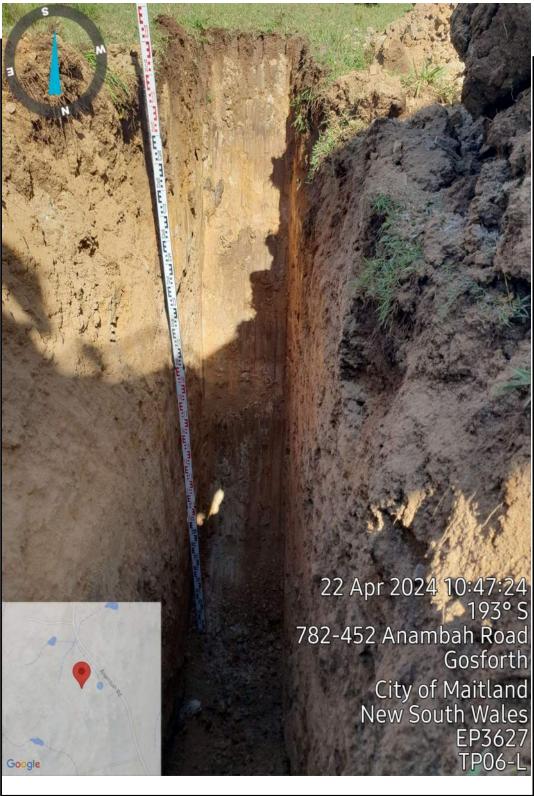
	С	lien	t		Thi	rdi C	Group c/- Vara	a Consulting				P	roject No	. Е	P3627
	Pı	oje	ct		Thi	rdi C	Sosforth Anan	nbah Rd	2220			L	ogged B	у А	N
-			tion					osforth NSW 2		01			hecked		P COT For work or
					avati Exca		22.4.24 on 22.4.24	Northing Easting	6384819.00 358352.00	Slope Bearing	90			uipment ound Lev	
E	XC	;AV	ATIO	NC				MATERIA	L DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
NA - 41	Netilod	Water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: pl	ption of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
				_	W.W.	CL- CI	TOPSOIL: Silty	CLAY: low to med	ium plasticity, dark grey				2		TOPSOIL
			-	- -		CI- CH	Silty CLAY: med	dium to high plastic	city, brown		~PL	F to St	1 2 4 10		RESIDUAL SOIL
y Dargel			34			CI- CH	Extremely weat to high plasticity	nered Mudstone re	ecovered as Silty CLAY (N n, with fine to coarse grain	Marl), medium ned sand			10		EXTREMELY WEATHERED ROCK DCP:-HB
FI E>> ZZ/US/ZUZ4 15:04 10:05:00:09 Devembed by	П		33	- - - - - - - 2							<pl< td=""><td>VSt to H</td><td></td><td>В</td><td></td></pl<>	VSt to H		В	
GOSFORTH ANAMBAH RD 0.1 AN.GPJ < <drawning< td=""><td></td><td></td><td>32</td><td>- - - - - - -</td><td></td><td></td><td>Test Pit TP05.P</td><td>Terminated at 3.0</td><td>0 m</td><td></td><td></td><td></td><td></td><td>В</td><td>Target depth</td></drawning<>			32	- - - - - - -			Test Pit TP05.P	Terminated at 3.0	0 m					В	Target depth
EP LIB USGLB LOG CW NON-CORED BOREHOLE LOG EF382/ I HIRDI GOSFOR IH ANAMBAH RD U.1 AN GFU <curwingfire>> ZZUSZUZ4 15:04 10.03:00.09 Developed by Datge</curwingfire>	R	ę,		- - - - - - - -			TOST IL IPUOP	, ominated at 3.0	~ ···						Talget dopar
EP LIB 05.GLB	K	cille	air NS	-											





TP05-P

	Clie					Group c/- Var	_					roject No		P3627
	Proj Loca	ect ation				Gosforth Anai nambah Rd, G	mbah Rd Sosforth NSW	2320				ogged B hecked		N P
	Star	ted	Exc	avat	ion	22.4.24	Northing	6384711.00	Slope	9	0°	Equ	uipment	23T Excavator
	Con	plet	ed	Exca	avati	on 22.4.24	Easting	358296.00	Bearing	-	-	Gro	ound Lev	vel 39 AHD
ΕX	(CA)	/AT	ION		_	I	MATERIA	L DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)		Classification		(soil type: p	ption of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
			-	W.W	CL- CI	TOPSOIL: Silty	CLAY: low to med	lium plasticity, dark brown				2		TOPSOIL
		-	- - - -		CI- CH	Silty CLAY: me	edium to high plasti	city, brown		~PL	F	2 2 2 2 2 2 2 4		RESIDUAL SOIL
eveloped by Datgel		38	- - 1 -			0.90m: become	es pale brown and	brown			St to VSt	6 6 5 6		
EP LIB 05/GLB Log CW NON-CORED BOREHOLE LOG EP3827 THIRDI GOSFORTH ANAMBAH RD 0.1 AN.GPJ <-Drawngrile>> 22/05/2024 15.04 10.03.00.09 Developed by Datgel		37	2		CI-CH	to high plasticit		ecovered as Silty CLAY (Marl) fine to coarse grained sand	, medium	<₽L	н	10 8 10 6 6		EXTREMELY WEATHERED ROCK DCP:-/5mm HB
IB 05.GLB Log CW NON-CORED BOREHOLE LUG EP:	Rem	- - - - - - 35	4			100011011001								





TP06-L

Test Pit No: TP07-P

Engineering Log - Test Pit

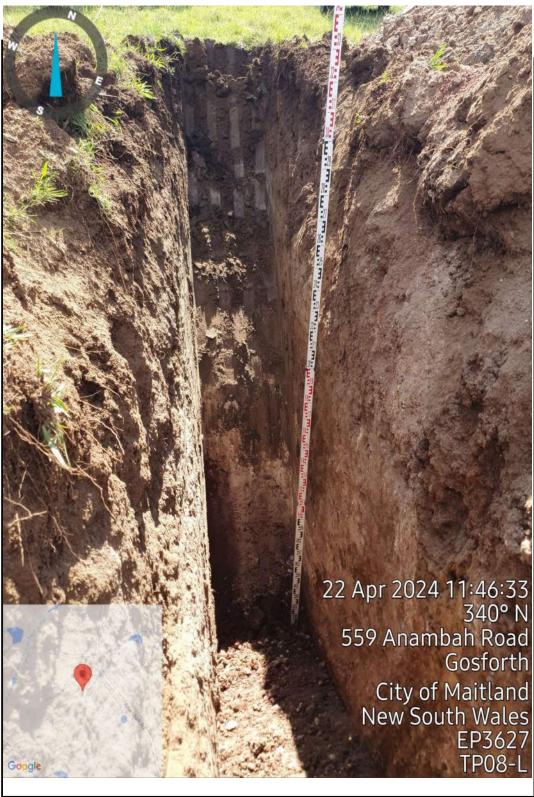
F	Clier Proje			Thi	rdi C	Group c/- Vara Gosforth Anan	_	2320			L	roject No ogged B	у А	P3627 N OP
5	Start	ed		avati	on	22.4.24 on 22.4.24	Northing Easting	6384917.00 358304.00	Slope Bearing		0°	Equ Gro	uipment ound Le	23T Excavator vel 29 AHD
EX	CAV	/ATI	ON				MATERIAL	DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: pla	otion of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
		_		₩W.	CL- CI	TOPSOIL: Silty	CLAY: low to medi	um plasticity, dark grey				2		TOPSOIL
		-	- - -		CI- CH	Silty CLAY: med	dium to high plastic	ity, brown		~PL	F to St	1 1 2 4		RESIDUAL SOIL
		- - - 28_	- - -		SC	fine to coarse gr	rained, brown, fine nterbedded with Mi	recovered as Clayey Grave to coarse grained, sub-ang udstone/MARL with ferrugir	ular to			9 15		EXTREMELY WEATHERED ROCK
F		- - -	-										В	
		- - - 27	2							M to D	D to VD			
		-	_											
		26	_3											
		-	- - - - - -			Test Pit TP07-P	Terminated at 3.0	0 m						Target depth
F	lRem	25 arks	<u>4</u> 5:											





TP07-P

F	Clier Proje			Thi	rdi C	Group c/- Vara	_	220			L	Project No logged B	у А	P3627 N OP
-	Start	ted		avati	on	22.4.24 on 22.4.24	Northing Easting	6384909.00 358149.00	Slope Bearing	90	0°	Equ	uipment ound Le	23T Excavator
EX	CA\	/ATI	ON				MATERIAL	DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: pla	otion of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
		-	_		CL- CI	TOPSOIL: Silty	CLAY: low to medi	um plasticity, dark brown		~PL		2 2 2		TOPSOIL
		-			CI- CH		lium to high plastic			~PL		5		RESIDUAL SOIL
F			1		SC	to coarse graine	d sand	ecovered as Clayey SAN		D		15 25		EXTREMELY WEATHERED ROCK
	-	28	2		CI-CH	recovered as Sa brown, with lime	andy CLAY, mediu	Sandstone and Mudstonen to high plasticity, dark I to coarse grained sand		<pl< td=""><td></td><td></td><td></td><td>Target depth</td></pl<>				Target depth
F	Rem	- - - - - - 26												





TP08-L

Test Pit No: TP09-P

Engineering Log - Test Pit

F	Clier Proje Loca			Th	irdi (Group c/- Vara Gosforth Anan ambah Rd, G	_	2320			L	roject No ogged B	у А	P3627 N DP
				avati Exca		22.4.24 on 22.4.24	Northing Easting	6384744.00 358131.00	Slope Bearing	90	0°	Equ	uipment	
EX	CA\	/ATI	ON				MATERIAL	DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	1	Classification		(soil type: pla	otion of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
		-	_	W.W.	CL- CI	TOPSOIL: Silty	CLAY: low to medi	um plasticity, dark brown		~PL		1		TOPSOIL
		- - - - - - 33	1		CL- CI	Silty CLAY: low	to medium plastici	ty, brown		~PL to <pl< td=""><td>F</td><td>1 1 1 1 2 1 2 2 2 2 2</td><td></td><td>SLOPE WASH</td></pl<>	F	1 1 1 1 2 1 2 2 2 2 2		SLOPE WASH
ш		- - - - - - 32			CI- CH	Silty CLAY: med	lium to high plastic	ity, brown, red		~PL		1 2 3 2 5 5 5 5 7	В	RESIDUAL SOIL
		-	_		CI- CH			MARL) recovered as Silty CL/ ine to coarse grained sand	AY, medium	<pl< td=""><td>VSt to H</td><td>7 9 9 8 8 10</td><td></td><td>EXTREMELY WEATHERED ROCK</td></pl<>	VSt to H	7 9 9 8 8 10		EXTREMELY WEATHERED ROCK
		- 31_	3							< <pl< td=""><td></td><td></td><td></td><td></td></pl<>				
		-	-			Test Pit TP09-P	Terminated at 3.0	0 m						Target depth
F	Rem	l30 narks	1 <u>4</u> 5:									<u> </u>		1





TP09-P

Test Pit No: TP10-P

Engineering Log - Test Pit

	Pr	ien oje cat			Thi	rdi C	Group c/- Vara Gosforth Anam ambah Rd, Go	-	320			L	roject No ogged By	у А	P3627 N OP
					avati Exca		22.4.24 on 22.4.24	Northing Easting	6384841.00 358029.00	Slope Bearing	90			uipment	
Е	XC.	AV.	ΆΤΙ	ON				MATERIAL	DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
10 ch ch	Medica	Water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: pla	otion of Soil asticity/grainsize, her components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
			_	_	WW)	CL- CI	TOPSOIL: Silty (CLAY: low to media	ım plasticity, dark grey				2		TOPSOIL
			-	- - -		CI- CH	Silty CLAY: med	ium to high plastici	ty, brown		~PL	F to St	2 3 2 4 5		RESIDUAL SOIL
loped by Datgel			- - 37 - -	- - 1 -		CI- CH	Extremely weath high plasticity, briggrained sand	ered Sandstone re own, interbedded	covered as Sandy CLAY, with Mudstone (MARL), fin	medium to e to coarse			12	В	EXTREMELY WEATHERED ROCK DCP:-/80mm HB
ngFile>> 22/05/2024 15:04 10.03.00.09 Deve	J	***	- - - 36	- - - - - 2							<pl< td=""><td>VSt to H</td><td></td><td></td><td></td></pl<>	VSt to H			
GOSFORTH ANAMEAN KD 0.1 AN.GP3 AADTAW			- - - - - 35	- - - - - - - -											
EP LIB USUSILIS CW NON-CURED BOREHOLE LUG EFSOZ/ I HIRDI GUSFUR IH ANAMBAH RU U.1 AN GFJ <-URAWIIGHIR>> ZZUSZUZ4 1534 4 10.03.00.09 DRVRKIDRG BY DRIGH			- - - - - - 34	4			Test Pit TP10-P	Terminated at 3.00) m						Target depth
EP LIB US.GLB LOG	Re	ema	arks	:		1									





F	Clier Proje Loca			Thi	rdi C	Group c/- Vara Gosforth Anam ambah Rd, Go	-	2320			L	roject No ogged B hecked I	у А	
				avati Exca		22.4.24 on 22.4.24	Northing Easting	6384806.00 357982.00	Slope Bearing	90			uipment ound Lev	
EX	CA\	/ATI	ON				MATERIAL	DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: pla	otion of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
				WW\ 	CL- CI	TOPSOIL: Silty	CLAY: low to medi	um plasticity, dark brown				2		TOPSOIL
		-	-		CI- CH	Silty CLAY: med	ium to high plastic	ity, brown		~PL	F to St	1 2 1 2 2 3		RESIDUAL SOIL
F			1		CI-CH	Extremely weath high plasticity, b	nered Sandstone rerown and dark gre	ecovered as Sandy CLAY, m	edium to	<pl< td=""><td>VSt to H</td><td>9 10 14 15</td><td></td><td>EXTREMELY WEATHERED ROCK</td></pl<>	VSt to H	9 10 14 15		EXTREMELY WEATHERED ROCK
		40				Test Pit TP11-L	Terminated at 3.00) m						Target depth
F	Rem	l39 narks	<u>1 4</u> 5:									<u> </u>		





TP11-L

Test Pit No: TP12-P

Engineering Log - Test Pit

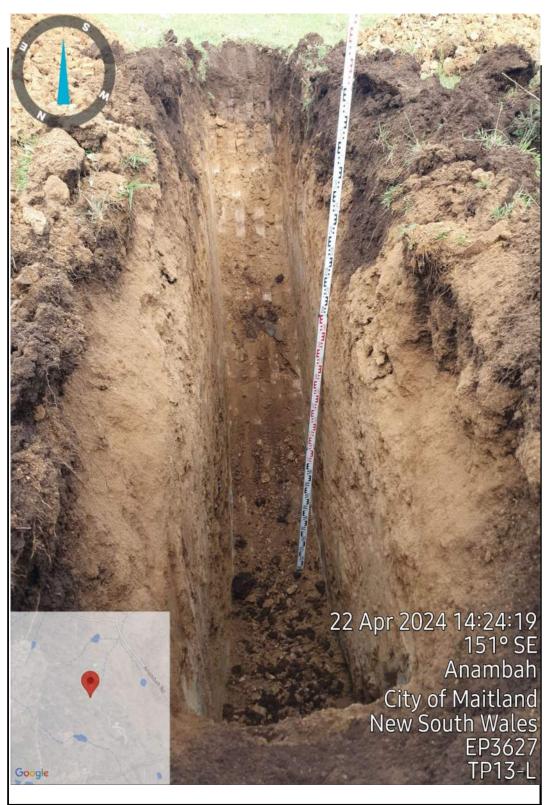
	Pro	ent ojed cati	ct		Thi	rdi C	Group c/- Vara Gosforth Anaml ambah Rd, Go	bah Rd	320			L	roject No ogged B	у А	P3627 N OP
					avati Exca		22.4.24 on 22.4.24	Northing Easting	6384748.00 357953.00	Slope Bearing	90			uipment	
E	XC/	4V/	ATIO	NC				MATERIAL	DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Motor	water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: pla	tion of Soil sticity/grainsize, ner components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
					W.W.	CL- CI	TOPSOIL: Silty C	CLAY: low to mediu	ım plasticity, dark grey				2		TOPSOIL
			-	- - -		CI- CH	Silty CLAY: mediu	um to high plastici	ly, grey, brown		~PL	F	2 2 2 2 8		RESIDUAL SOIL
EPLIB USUCIB LOG CW NON-CURED BOREHOLE LUG EPSEZ I HIRIZI GUSPURI II ANAMBAH KD U 1 AN.GPU KALTAWIGFIIR>> ZZUGZZUZ4 13:04 10.03:00.09 Developed by Datgel		4		- - - - - - - - - - - - - - - - - - -		CI-CH	Extremely weath high plasticity, greatly plasticity, greatly plasticity.	ey-yellow, fine to o	covered as Sandy CLAY, oarse grained sand	medium to	<pl< td=""><td>VSt tc H</td><td>23 21</td><td></td><td>EXTREMELY WEATHERED ROCK Target depth</td></pl<>	VSt tc H	23 21		EXTREMELY WEATHERED ROCK Target depth
LIB 05/GLB LOG CW NON-COKEU BOREHULE LUG EF302/ IIII	Re	4ema		- - - - - - - - - - - -											





TP12-P

	Cli	en	t		Th	irdi (Group c/- Vara	. Consulting				P	roject No	n F	P3627
	Pr				Th	irdi (Gosforth Anan	nbah Rd				L	ogged B	у А	.N
	Lo	cat	tion		55	9 An	ambah Rd, G	osforth NSW	2320			С	hecked	Ву С)P
					avati		22.4.24 on 22.4.24	Northing	6384644.00 358074.00	Slope		0°		uipment ound Le	
F		_		ON	EXCa	ivalio	DII 22.4.24	Easting	L DESCRIPTION	Bearing			1		MPLING & OTHER INFORMATION
-		\v.	A11					WATERIA	L DESCRIPTION				IESII	NG, SA	INFEING & OTTEN INFORMATION
704	DO INGELIOR	water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: p	ption of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Ē	Additional Comments (material origin, pocket penetrometer values, investigation observations)
			-	_	W.W.	CL- CI	TOPSOIL: Silty	CLAY: low to med	lium plasticity, dark grey				2		TOPSOIL
			-	- -		CI- CH	Silty CLAY: med	dium to high plasti	city, grey		~PL	F	2 2 1		SLOPE WASH
			-	-		CI- CH		dium to high plasti				S to VSt	3 9		RESIDUAL SOIL
			-	_		CI- CH	Extremely weath high plasticity, b	hered Sandstone i rown, fine to coars	recovered as Sandy CLA\ se grained Sand	/, medium to			18		EXTREMELY WEATHERED ROCK
03.00.09 Developed by Datgel	١.		38	1							<pl< td=""><td></td><td></td><td></td><td></td></pl<>				
< <drawingfile>> 22/05/2024 15:04 10.</drawingfile>			- - 37 - -	2		CI- CH	Extremely weat recovered as Sc coarse grained	andv CLAY, mediu	nterbedded with Mudston m to high plasticity, dark l	e (MARL), brown, fine to		н			
USFURTH ANAMBAH KD 0.1 AN GPJ			- - - - -								< <pl< td=""><td></td><td></td><td></td><td></td></pl<>				
EP LIB 05.GLB Log CW NON-CORED BOREHOLE LOG EP3827 THIRDI GOSFORTH ANAMBAH RD 0.1 ANI GPU < <drawngrile>> 22/05/2024 15:04 10.03:00.09 Developed by Dargel</drawngrile>			36				Test Pit TP13-L	Terminated at 3.0	0 m						Target depth
EP LIB 05.GLB LC	Re	ema	arks	S :											





Test Pit No: TP14-P

Engineering Log - Test Pit

	Clie	nt		Thi	irdi (Group c/- Vara	a Consulting				P	roject No	. Е	P3627
	Proj	ect		Thi	irdi (Gosforth Anan	nbah Rd	2220			L	ogged B	у А	N P
		ation					osforth NSW		Clana	0/		hecked		
				avati Exca		22.4.24 on 22.4.24	Northing Easting	6384591.00 358046.00	Slope Bearing	90			uipment ound Lev	
E	(CA	VAT	ON				MATERIA	L DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	1 1	Classification		(soil type: p	iption of Soil lasticity/grainsize, ither components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
			-	}};;;	CL- CI	TOPSOIL: Silty	CLAY: low to med	lium plasticity, dark grey				2		TOPSOIL
		-	_		CI- CH	Silty CLAY: med	dium to high plasti	city, grey		~PL	F to St	2 2 2 2 2		RESIDUAL SOIL
EP LIB 05/GLB Log CW NON-CORED BOREHOLE LOG EP3627 THIRDI GOSFORTH ANAMBAH RD 0.1 AN GPJ «ChrawingFile»> 22/05/2024 15:04 10:03:00.09 Developed by Datgel		38	1		Cl-CH	high plasticity, b	hered Sandstone prown, fine to coar		, medium to	<pl< td=""><td>VSt to</td><td>9 13 13 15</td><td></td><td>EXTREMELY WEATHERED ROCK Refusal</td></pl<>	VSt to	9 13 13 15		EXTREMELY WEATHERED ROCK Refusal
EP LIB 05.GLB Log CV	Ren	35 narks	<u> </u> 4 s:											





Test Pit No: TP15-P

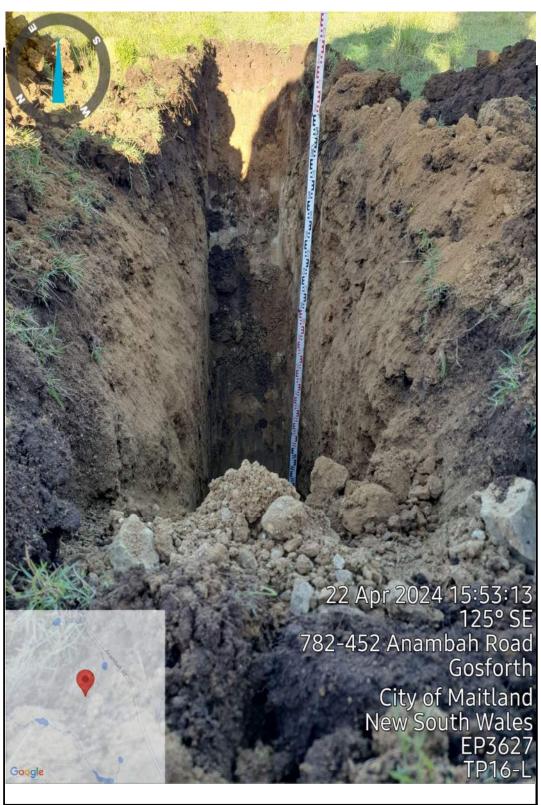
Engineering Log - Test Pit

F	Clier Proje Loca			Thi	rdi (Group c/- Vara Gosforth Anan ambah Rd, G	_	2320			L	roject No ogged B	у А	:P3627 N OP
				avati	on	22.4.24 on 22.4.24	Slope Bearing	90°		Equ	uipment ound Le			
EX	CAV	/ATI	ON				MATERIA	LDESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: pl	ption of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
		_		WW)	CL- CI	TOPSOIL: Silty	CLAY: low to med	ium plasticity, dark grey				2		TOPSOIL
		-	-		CI- CH	Silty CLAY: med	dium to high plastic	ity, brown		~PL	F and St	3 2		RESIDUAL SOIL
		-	_								Ö.	2 3	В	
		- - - 34	1		CI- CH	Extremely weat high plasticity, b	hered Sandstone r prown, fine to coars	ecovered as Sandy CLAY e grained sand	, medium to			12 10 15		EXTREMELY WEATHERED ROCK
ш					CI-CH		andy CLAY, mediu	nterbedded with Mudstone m to high plasticity, dark b		<pl< td=""><td>н</td><td></td><td></td><td></td></pl<>	н			
		32	3			Test Pit TP15-P	P Terminated at 3.0	0 m		< <pl< td=""><td></td><td></td><td></td><td>Target depth</td></pl<>				Target depth
F	Rem	31 narks	4											





F	Clier Proje Loca			Thi	rdi C	Group c/- Vara Gosforth Anan ambah Rd, G	_	2320			L	roject No ogged B	у А	P3627 N DP
				avati	on	22.4.24 on 22.4.24	Slope Bearing		0°	Equ	uipment ound Le			
EX	CAV	/ATI	ON				MATERIA	L DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: pl	ption of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
		-		WW)	CL- CI	TOPSOIL: Silty	CLAY: low to med	ium plasticity, dark grey				1		TOPSOIL
		- - -	- - -		CI- CH	Silty CLAY: med	dium to high plastio	city, grey		~PL	F	1 2 5		RESIDUAL SOIL
F		37	- - - 1 - - - - - - - - - - - - - - - -		Ci-CH	recovered as Sa coarse grained	andy CLAY, mediu	nterbedded with Mudstone m to high plasticity, dark bro	(MARL), own, fine to	₽ L	VSt to	11 15 15		EXTREMELY WEATHERED ROCK
F	Rem	- - - - - - - 34	- - - - - - - ::											Target depth





Test Pit No: TP17-P

Engineering Log - Test Pit

		`lien	nt		Thi	rdi G	Group c/- V	ara Consultino	1					roject No	, F	P3627			
	Client Thirdi Group c/- Vara Consulting Project Thirdi Gosforth Anambah Rd Location 559 Anambah Rd Gosforth NSW 2320												L	ogged B	у А	N			
L	Location 559 Anambah Rd, Gosforth NSW 2320												С	hecked	Ву О)P			
	Started Excavation 22.4.24 Northing 6384433.00 Slope Completed Excavation 22.4.24 Easting 358262.00 Bearing												90° Equipment 23T Excavator Ground Level 31 AHD						
ŀ	EXCAVATION MATERIAL DESCRIPTION												TESTING, SAMPLING & OTHER INFORMATION						
	Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		Des	cription of s plasticity/g d other com	Soil grainsize.		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)			
			_	_	₩ ₩ ₩ ₩ ₩	CL- CI	TOPSOIL: Si	ilty CLAY: low to m	nedium plastic	ity, dark grey				1		TOPSOIL			
			-	- -		CI- CH	Silty CLAY: r	nedium to high pla	asticity, grey			~PL	F	1 1		SLOPE WASH			
			-	_		CI- CH	Silty CLAY: r	nedium to high pla	sticity, brown			<pl< td=""><td></td><td>5 10</td><td></td><td>RESIDUAL SOIL</td></pl<>		5 10		RESIDUAL SOIL			
			-	_		CI- CH	Extremely we high plasticity	eathered Sandstor y, brown, fine to co	ne recovered a parse grained	as Sandy CLAY, me sand	edium to			13 14		EXTREMELY WEATHERED ROCK			
-			30	1															
oped by Datge			-	-											В				
00.09 Devek	ш		-	_															
< <drawingfile>> 22/05/2024 15:04 10.03.00.09 Developed by Datgel</drawingfile>			-	_									VSt to H						
22/05/2024			- 29	2								< <pl< td=""><td></td><td></td><td></td><td></td></pl<>							
rawingFile>>			-	_															
AN.GPJ < <d< td=""><td></td><td></td><td>-</td><td>_</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></d<>			-	_															
3AH RD 0.17			_	_															
EP LIB 05.GLB Log CW NON-CORED BOREHOLE LOG EP3627 THIRDI GOSFORTH ANAMBAH RD 0.1 AN.GPJ			-	- -															
IRDI GO	\dashv		28 <u> </u>	_3	1//		Test Pit TP1	7-P Terminated at	3.00 m							Target depth			
EP3627 TH			-																
HOLE LOG .			-	_															
RED BOREH			-	-															
OM NON-CO			-	- -															
5.GLB Log (R	Rem	27 arks	L 4 5:												<u>I</u>			
EP LIB 0																			





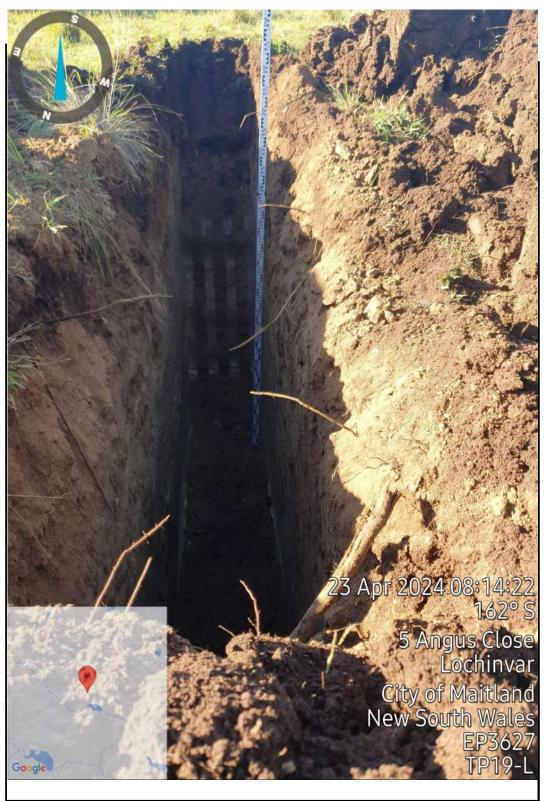
		ent					Group c/- Vara	_					roject No		P3627				
		oje cat	cı ion				Gosforth Anar ambah Rd, G	osforth NSW	2320				ogged B hecked		N P				
	Started Excavation 23.4.24 Northing 6384392.00 Slope													uipment					
	Completed Excavation 23.4.24 Easting 358227.00 Bearing												Ground Level 28 AHD						
E	EXCAVATION MATERIAL DESCRIPTION												TESTI	NG, SA	MPLING & OTHER INFORMATION				
N 4 - 41- 2-4	DOLLING	water	RL (m)	Depth (m)		Classification		(soil type: p	ption of Soil lasticity/grainsize, other components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)				
			-	_	X	CL- CI	TOPSOIL: Silty	CLAY: low to med	lium plasticity, dark grey				1		TOPSOIL				
			-	- -		CI- CH	Silty CLAY: med	dium to high plasti	city, dark brown		~PL	F to St	3 3	В	SLOPE WASH				
			-	-		CI- CH	Gravelly CLAY: angular to suba	medium to high p ngular gravel	lasticity, brown, fine to co	parse grained,			6 8		RESIDUAL SOIL				
EP LIB 05.GLB Log CW NON-CORED BOREHOLE LOG EF3627 THIRDI GOSFORTH ANAMBAH RD 0.1 AN.GPJ < <drawingfile>> 22/05/2024 15:04 10.03 00.09 Developed by Datgel</drawingfile>	J J	P A		1		CI-CH	CLAY, medium	to high plasticity, o	and Mudstone, recovered	d as Sandy e sand	<₽L	VSt tc	25		EXTREMELY WEATHERED ROCK				
Og CW NON-COKED BOREHOLE LOG ETO			- - - - -	- - - - - - - -			rest Mt. IP18-L	Terminated at 3.2	20 III						Target depth				
EP LIB 05.GLB	r\e	, i i l ĉ	arks	••															





TP18 - L

ı	Clier Proje	ect		Thi	irdi (Group c/- Vara	_	2220			L	Project No ogged B	у А	
-;	Start	ted	Exc	avati	on	23.4.24 on 23.4.24	Northing Easting	6384484.00 357971.00	Slope Bearing		0°	Equ	uipment ound Lev	23T Excavator
EX	EXCAVATION MATERIAL DESCRIPTION											TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: pl	ption of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
		_		}} } } } } } }	CL- CI	TOPSOIL: Silty	CLAY: low to med	ium plasticity, dark grey				2		TOPSOIL
		-	_		CI- CH	Silty CLAY: med	dium to high plastic	sity, brown		~PL	F to St	2 3 3 3 4	U500.29	SLOPE WASH
		- 31	† - - -		CI- CH	Sandy CLAY: m sand	edium to high plas	ticity, brown, fine to medi	um grained	-		5 5 7		RESIDUAL SOIL
E		30	2	CI- Extremely we CLAY, mediu	CLAY, medium	to high plasticity, d	and Mudstone, recovered lark brown, fine to coarse	as Sandy grained sand	<₽L	VSt to	9 7 9 10 9 13 16		EXTREMELY WEATHERED ROCK	
			3			Test Pit TP19-L	Terminated at 2.5	0 m						Target depth
	Rem	iai KS	·.											





TP19 - L

Test Pit No: TP20-P

Engineering Log - Test Pit

F	Clier Proje	ect		Thi	rdi C	Group c/- Vara	nbah Rd	2000			L	roject No	у А	EP3627 .N
5	Start			avati	on	23.4.24 on 23.4.24	Northing Easting	6384451.00 358060.00	Slope Bearing		0°		uipment	
EX	CCAVATION MATERIAL DESCRIPTION											TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: pla	otion of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
		-		W.W.	CL- CI	TOPSOIL: Silty	CLAY: low to medi	um plasticity, dark grey				2		TOPSOIL
		-	- - -		CI- CH	Silty CLAY: med	dium to high plastic	ity, dark brown		~PL	F and St	2 1 3 2 3	В	SLOPE WASH
		- - 29	1		CI- CH	Gravelly CLAY: angular to subar	medium to high pla ngular gravel	asticity, brown, fine to med	ium grained,			8 15 12		RESIDUAL SOIL
F					CI-CH	brown, fine to co	lered Santasone in	ecovered as Sandy CLAY,	grey and	<pl< td=""><td>VSt to</td><td>17</td><td></td><td>EXTREMELY WEATHERED ROCK</td></pl<>	VSt to	17		EXTREMELY WEATHERED ROCK
	- Pam	27	3			Test Pit TP20-P	Terminated at 2.4	0 m						Target depth
F	≺em	arks	5 :											





Geotechnical Investigation

Test Pit No: TP21-P

Engineering Log - Test Pit

ı	Clier Proje	ect		Thi	rdi C	Group c/- Vara Cor Gosforth Anambah ambah Rd, Gosfo	Rd	320			L	roject No ogged B	y A	
- ;	Star	ed		avati	on	23.4.24 N	lorthing asting	6384398.00 358132.00	Slope Bearing	90)°	Equ	ipment und Lev	23T Excavator
EX	CA\	/ATI	ON	<u> </u>		N	MATERIAL	DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification	(sc col	oil type: pla	tion of Soil sticity/grainsize, ner components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
				WW\ 	CL- CI	TOPSOIL: Silty CLAY	: low to mediu	m plasticity, dark grey				2		TOPSOIL
		-	- - -		CI- CH	Silty CLAY: medium to	o high plasticit	y, brown		~PL	F to St	2 2 3 3 3		SLOPE WASH
		-	_		CI- CH	Sandy CLAY: medium	n to high plasti	city, brown, fine to coarse	grained sand	<pl to ~PL</pl 		3 4		RESIDUAL SOIL
		- 26	1		SC	Extremely weathered coarse, brown	Sandstone re	covered as Clayey SAND,	fine to			10		EXTREMELY WEATHERED ROCK
ш		-	_									15		
		-	_										В	
ш		-	-											
		-	_											
		25 <u> </u>	2							D	VD			
		- -	_											
		-	-											
		24 <u> </u>	_3											
		-	- - -			Test Pit TP21-P Term	inated at 3.20	m						Target depth
		-	_ _ _											
I	L Rem	l23 Iarks	L_4_ 5:											<u> </u>

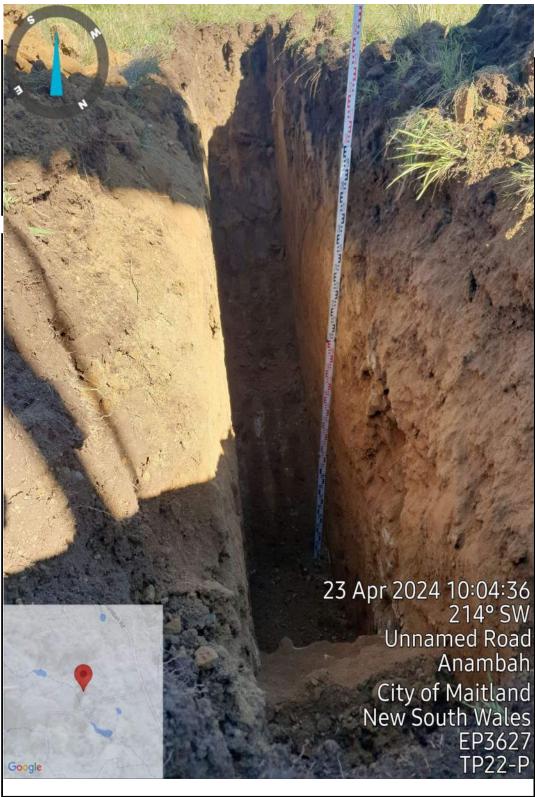




Test Pit No: TP22-P

Engineering Log - Test Pit

F	Clier			Thi	irdi (Group c/- Vara Gosforth Anam	_	2320			L	roject No ogged B	у А	:P3627 N OP
	Start	ted		avati	on	23.4.24 on 23.4.24	Northing Easting	6384289.00 358289.00	Slope Bearing		0°	Equ	uipment	23T Excavator
EX	CA\	/ATI	ON				MATERIAL	DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: pla	otion of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
				₩ } } }	CL- CI	TOPSOIL: Silty	CLAY: low to medi	um plasticity, dark grey				1		TOPSOIL
		-	_		CI- CH	Silty CLAY: med	lium to high plastic	ity, brown			F to St	1 1 2		SLOPE WASH
		- 	_		CI- CH	Silty CLAY: med	lium to high plastic	ity, yellow, brown		~PL		3 5 8		RESIDUAL SOIL
F		22	1		CH	high plasticity, p		ecovered as Sandy CLAY	r, medium to	<pl< td=""><td>VSt tc</td><td>12 12</td><td></td><td>EXTREMELY WEATHERED ROCK Target depth</td></pl<>	VSt tc	12 12		EXTREMELY WEATHERED ROCK Target depth
		-												
F	Rem	arks	s: 											





Engineering Log - Test Pit

	CI	ien	t		Th	irdi (Group c/- Vara	a Consulting					roject No		P3627
		oje cat	ct tion				Gosforth Anar Iambah Rd, G	mbah Rd Josforth NSW 2	2320				ogged B hecked		N OP
	St	arte	ed	Exc	avati		23.4.24	Northing	6384325.00	Slope	90	0°		uipment	23T Excavator
	Co	omp	plet	ed	Exca	vati	on 23.4.24	Easting	358042.00	Bearing		-	Gro	ound Le	vel 30 AHD
E	XC	AV	ΆΤΙ	ON				MATERIA	L DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
-	Method	Water	RL (m)	Depth (m)		Classification		(soil type: pl	ption of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
			-	-	W.W.	CL- Cl	TOPSOIL: Silty	CLAY: low to med	ium plasticity, dark grey				1		TOPSOIL
			-	-	W	CI- CH	Silty CLAY: me	dium to high plastic	city, brown				2		SLOPE WASH
			-	_							~PL	F	2 2 2 1	U50	
			-	<u> </u>		CI- CH	Gravelly CLAY: angular gravel	medium to high pl	asticity, brown, fine to med	ium grained,			4 5		RESIDUAL SOIL
_			29 <u> </u>	_1									6		
oy Datge			-								<pl< td=""><td>VSt</td><td>7</td><td></td><td></td></pl<>	VSt	7		
eloped			-	+									8		
.09 Dev													7		
0.03.00	ш		-	-		CI-	Extremely weat	hered Sandstone i	nterbedded with Mudstone	(MARL)			8		EXTREMELY WEATHERED ROCK
15:04 1			-	ł		CH	recovered as S coarse grained	andy CLAY, mediu	m to high plasticity, brown,	fine to			7		
)5/2024			-										9		
>> 22/(1	28	_2									17		
wingFile			-	t									15		
< <drain< td=""><td></td><td></td><td>-</td><td>Į.</td><td></td><td></td><td></td><td></td><td></td><td></td><td><<pl< td=""><td></td><td></td><td></td><td></td></pl<></td></drain<>			-	Į.							< <pl< td=""><td></td><td></td><td></td><td></td></pl<>				
AN.GPJ			-	-								Н			
KD 0.1,			_	H											
MBAH			-	Į.											
TH AN			-	-											
OSFOR			- 27	3											
HRDI G															
3627 TI	\dashv		-	+			Test Pit TP23-L	. Terminated at 3.2	0 m						Target depth
90 EP			-	İ											
HOLE			_	_											
D BOR			-	+											
-core			-	<u> </u>											
EP LIB 05.GLB Log CW NON-CORED BOREHOLE LOG EP3627 THIRDI GOSFORTH ANAMBAH RD 0.1 ANIGPJ < <drawngfile>> 22/05/2024 15.04 10.03.00.09 Developed by Dagel</drawngfile>			-	-											
Fog	Re	ema	₂₆ arks	<u> </u>											
3 05.GLE															
T															





Test Pit No: TP24-P

Engineering Log - Test Pit

1	Clier Proje					Group c/- Vara Gosforth Anam	_				L	roject No	у А	:P3627 .N
	Loca						osforth NSW 2					hecked)P
				avati Exca		23.4.24 on 23.4.24	Northing Easting	6384221.00 358092.00	Slope Bearing		0° 		uipment ound Le	
EX	CA\	/ATI	ON				MATERIAL	LDESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: pl	ption of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
		_			CL- CI	TOPSOIL: Silty	CLAY: low to medi	ium plasticity, dark grey				1 2		TOPSOIL
		- - -	- - - -		CI- CH	Silty CLAY: med	ium to high plastic	ity, brown, red		~PL	F to St	1 2 2 3 3 3		SLOPE WASH
		-										5	В	
		30	_1		CI- CH	Silty CLAY: med	lium to high plastic	ity, brown, grey				7		RESIDUAL SOIL
ET ELE OUTGO DE STATEMENT DE LE LOC ET TOTAL THE MANAGEMENT DE L'ANGELE L'OUTGE TOTAL TOTA			2		CI-CH	recovered as Sa coarse grained s	indy CLAY, mediu	nterbedded with Mudstone m to high plasticity, brown	e (MARL), ,, fine to	< <pl< td=""><td>VSt tc</td><td>10</td><td></td><td>EXTREMELY WEATHERED ROCK Target depth</td></pl<>	VSt tc	10		EXTREMELY WEATHERED ROCK Target depth
F	Rem	- - - - - - 27												





Test Pit No: TP25-P

Engineering Log - Test Pit

		lien					Group c/- Vara	-					roject No		P3627
		roje oca	ct tion				Gosforth Anar ambah Rd, G	nbah Rd osforth NSW 2	2320				ogged B		N P
F	S	tarte	ed	Exca	avati	on	23.4.24	Northing	6384248.00	Slope	90	0°	Equ	uipment	23T Excavator
		_			Exca	vatio	on 23.4.24	Easting	358009.00	Bearing		-		ound Lev	
E	XC	VAC	ΆΤΙ	ON				MATERIA	L DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
	Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		Descri (soil type: pl colour and o	ption of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
			_	_	W.W.	CL- CI	TOPSOIL: Silty	CLAY: low to med	ium plasticity, dark grey				2		TOPSOIL
			-	- - -		CI- CH	Silty CLAY: med	dium to high plastic	pity, brown		~PL	F to St	3 3 3		SLOPE WASH
			- - - 33	- - - 1		CI- CH	Gravelly CLAY: angular to suba		asticity, brown, fien to coa	rse grained,		VSt to	10		RESIDUAL SOIL
EP LIB 05.G1B Log CW NON-CORED BOREHOLE LOG EP3627 THIRDI GOSFORTH ANAMBAH RD 0.1 AN.GPJ < <drawingfile>> 22/05/2024 15:04 10.03.00.09 Developed by Datgel</drawingfile>	п	÷	33	1		GP	fine to coarse g coarse grained	rained, sub-angula	ecovered as Clayey Sandr to angular, brown to darlous cementations (50-70r	brown, fine to	M to D	VD	14 12 11 15	В	EXTREMELY WEATHERED ROCK Target depth
EP LIB US.GLB LOG CW NOR	R	ema	- 30 arks	4											

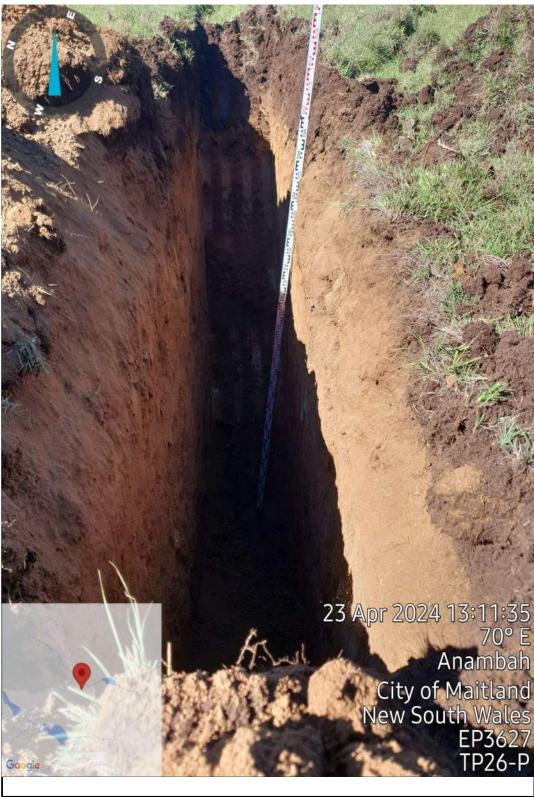




Test Pit No: TP26-P

Engineering Log - Test Pit

	Clie	ent		Т	hire	di G	Group c/- Vara	a Consulting				Р	roject No	р. Е	P3627
		ject atio	า				Sosforth Anan ambah Rd, G		2320				ogged B hecked		N P
				cava			23.4.24	Northing	6384349.00	Slope	90			uipment	23T Excavator
				_	av	atio	on 23.4.24	Easting	357850.00	Bearing		-	Gro	ound Lev	vel 33 AHD
E	XCA	TAV	101	1	_			MATERIA	AL DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Denth (m)		_	Classification		(soil type: p	iption of Soil lasticity/grainsize, other components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
			ļ	W.V.		CL- CI	TOPSOIL: Silty	CLAY: low to me	dium plasticity, dark grey			F	2		TOPSOIL
	CI-CH Silty CLAY: medium to high plasticity, brown												3 3 3 3 5		RESIDUAL SOIL
EP LIB 05/G1B Log CW NON-CORED BOREHOLE LOG EP3627 THIRDI GOSFORTH ANAMBAH RD 0.1 AN.GPJ < <drawingfile>> 22/05/2024 15:04 10.03:00:09 Developed by Datgel</drawingfile>		31				SC	to dark brown, fi	nered Sandstone ine to coarse graine to	ned sand	D, dark brown	M to D	VD	12 10 9 9 17		EXTREMELY WEATHERED ROCK Target depth
PLIB 05.GLB Log CW	Rei	₂₉ mark	is:	1											





TP26 - P

Engineering Log - Test Pit

	Clier Proje					Group c/- Vara	-						roject No		P3627 N
	_oca						osforth NSW	2320					hecked I)P
				avati Exca		23.4.24 on 23.4.24	Northing Easting	6384402.00 357675.00		pe aring	90			uipment	
EX	CAV	/ATI	ON				MATERIA	L DESCRIPTION					TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)		Classification		(soil type: pl	ption of Soil asticity/grainsize, ther components))		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
		_		₩ <u>₩</u>	CL- CI	TOPSOIL: Silty boulders	CLAY: low to med	lium plasticity, dark gre	y, with 300mr	n			2		TOPSOIL
		-			CI- CH		edium to high plas	sticity, brown, fine to co	arse grained	sand	~PL	F St	1 2 2 2 2 3 4		RESIDUAL SOIL
ш		- - 45	1		SC	Extremely weat coarse grained,	hered Sandstone i brown	recovered as Clayey SA	AND, fine to		D	VD	7		EXTREMELY WEATHERED ROCK DCP:-/80mm HB
F		-	_			Test Pit TP27-L	Terminated at 1.6	i0 m							Refusal
		- - 44 - -	2												
		-	_												
			-												
F	Remarks:														



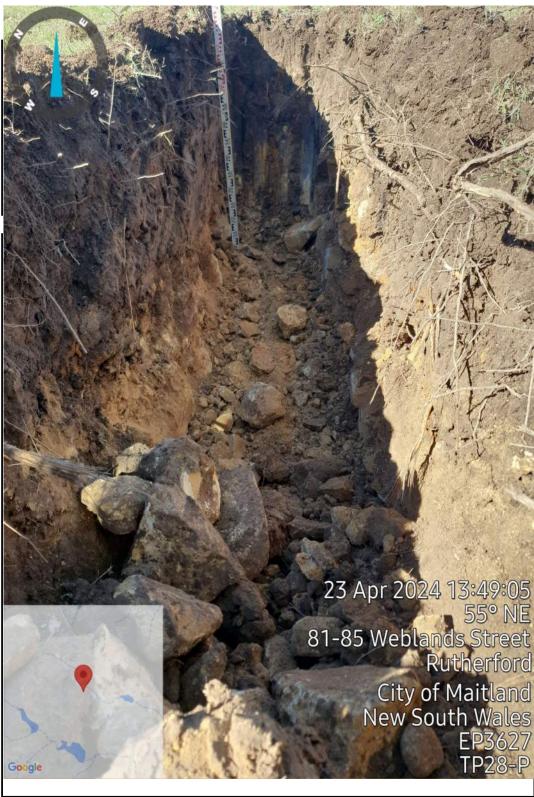


TP27 - L

Test Pit No: TP28-P

Engineering Log - Test Pit

	Clier	nt		Thi	rdi C	Group c/- Vara	Consulting				—— Р	roject No	о. Е	P3627
F	⊃roj∈	ect		Thi	rdi C	Gosforth Anan	nbah Rd	0000			L	ogged B	у А	N
	_oca					ambah Rd, G			01			hecked		P COT For work or
				avati Exca		23.4.24 on 23.4.24	Northing Easting	6384445.00 357731.00	Slope Bearing	90			uipment ound Lev	
		/ATI					MATERIA	L DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: p	iption of Soil lasticity/grainsize, tther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
		-		W.W.	CL- CI	TOPSOIL: Silty	CLAY: low to med	dium plasticity, dark grey				1		TOPSOIL
		-			CI- CH	Silty CLAY: med	lium to high plasti	city, grey		~PL	F	1		RESIDUAL SOIL
ш		 - -	- -		SC	Extremely weath coarse grained,	nered Sandstone pale brown	recovered as Clayey SANI	D, fine to			5		EXTREMELY WEATHERED ROCK DCP:-/50mm HB
<u> </u>	_	37 <u> </u>	_1							D	VD			
Dy Datg		-	_										В	
EF LE USSUEL LOG CW NOW-CURED BONEHOLE LUG EFSOZ/ I HIROLI GOSFOR IH ANAMBAH RU U.1 AN UFJ. <-CURAMIGNIES> ZZUSZUZA 1534 10J33,00J8 Developed by Jagge		36				Test Pit TP28-P	Terminated at 1.3	30 m						Refusal
LIB VO:GED EVA														
i L														



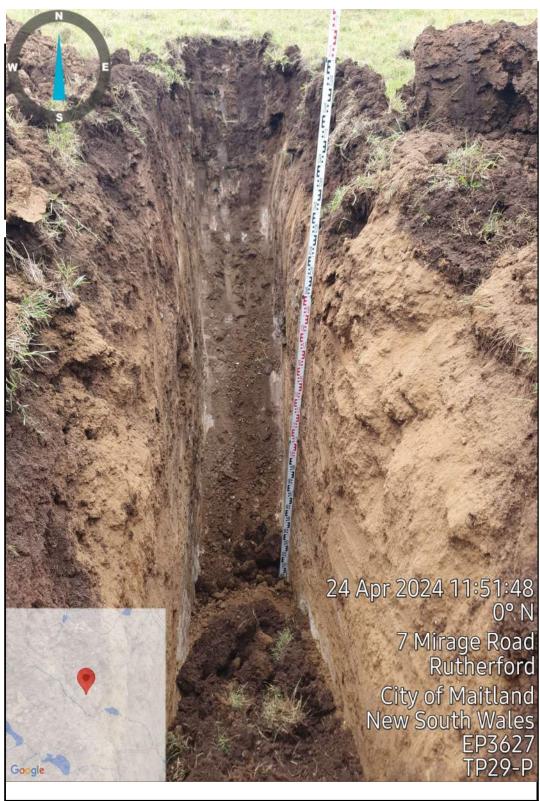


TP28 - P

Test Pit No: TP29-P

Engineering Log - Test Pit

	Cli	Client Thirdi Group c/- Vara Consulting Project No. EP3627 Project Thirdi Gosforth Anambah Rd Logged By AN Location 559 Anambah Rd, Gosforth NSW 2320 Checked By OP													
									2320						
				Evo	avati		24.4.24	Northing	6384503.00	Slope	90			uipment	
							24.4.24 on 24.4.24	Easting	357850.00	Bearing				und Lev	
Е	XCA	٩V٨	ATI	ON				MATERIAL	DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Wetnod	water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: pla	otion of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
					W.W.	CL- CI	TOPSOIL: Silty	CLAY: low to medi	um plasticity, dark grey				1		TOPSOIL
				-		CI- CH	Silty CLAY: med	dium to high plastic	ity, brown, grey		~PL	F to St	2 2 2 4		RESIDUAL SOIL
EXTREMELY WEATHERED ROCK DCP:-/20mm HB															
ZGIMAN .			=	_	2/2		Test Pit TP29-P	Terminated at 2.7	0 m						Refusal
Test Pit TP29-P Terminated at 2.70 m Refusal Remarks:															
בא רום ממיפרני נ	Кe	ma	arks												





Test Pit No: TP30-P

Engineering Log - Test Pit

- 1	Clie Proj					Group c/- Vara Gosforth Anan	_				L	roject No	у А	P3627 N
	Loca	ation		55	9 An	ambah Rd, G	osforth NSW	2320			С	hecked	Ву С	P
				avat Exca		24.4.24 on 24.4.24	Northing Easting	6384571.00 357708.00	Slope Bearing	90			uipment ound Lev	
E	(CA)	VATI	ON				MATERIA	L DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: p	ption of Soil lasticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
				W.W.	CL- CI	TOPSOIL: Silty	CLAY: low to med	lium plasticity, grey		>PL to		0		TOPSOIL
		-	_		CI- CH	Silty Gravelly Cl grained, angular	_AY: medium to hi to subangular gra	igh plasticity, grey, brown, i avel	fine to coarse	~PL/ ~PL to <pl< td=""><td>VS to St</td><td>2 3</td><td></td><td>RESIDUAL SOIL</td></pl<>	VS to St	2 3		RESIDUAL SOIL
ET LIB OSCILLE LOG CW NOW-CURED BOREHOLE LOG EFOOZ I TRIKUI GOSTOR IT ANAMBATI RU U. IAN GFU «Kulawingfille» / ZZUGZZZZZ 1834 1834 1834 1834 1835 Dangel		42	1		다	plasticity, brown		ecovered as Silty CLAY, m	edium to high	< <pl< td=""><td>St to VSt VSt and H</td><td>9 8 10 6 9 14 20</td><td></td><td>Target depth</td></pl<>	St to VSt VSt and H	9 8 10 6 9 14 20		Target depth
		-	- - -											
8	Ren	l39 narks	<u> 4</u> S:											





Engineering Log - Test Pit

	Clie					Group c/- Vara	_					roject No		P3627
	Proj Loc	ect atior	1			Gosforth Anar ambah Rd, G	nbah Rd osforth NSW	2320				ogged B hecked		N P
	Star	ted	Exc	avati		24.4.24	Northing	6384632.00	Slope	90	0°		uipment	23T Excavator
						on 24.4.24	Easting	357777.00	Bearing		-		und Le	
E	KCA	VAT	ION				MATERIA	L DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: p	iption of Soil lasticity/grainsize, ither components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
				WW.	CL- CI	TOPSOIL: Silty	CLAY: low to med	lium plasticity, dark grey		~PL to		1		TOPSOIL
			+		CI- CH	Sandy Gravelly coarse grained,	CLAY: medium to angular to subanç	high plasticity, grey, brown gular gravel, fine to coarse ξ	, fine to grained sand	>PL <pl to ~PL</pl 	F to St	3 5		RESIDUAL SOIL DCP:-/10mm HB
			+	//	SC			recovered as Clayey SAND	, fine to					EXTREMELY WEATHERED ROCK
EP LIB 05 GLB Log CW NON-CORED BOREHOLE LOG EP3627 THIRDI GOSFORTH ANAMBAH RD 0.1 AN GPJ <<- DrawingFiles> 22/05/2024 15:04 10:03:00:09 Develoed by Dargel		45 _	1			coarse grained,		20 m		D	VD			Tarret denth
EP36.			+			Test Pit TP31-L	Terminated at 3.2	20 m						Target depth
Log CW NON-CORED BOREHOLE LOG	Ren	43 nark	+ + + + + + + s:											
5.GLB	1 (61)	ııaı K	٥.											
EP LIB 0														





Test Pit No: TP32-P

Engineering Log - Test Pit

	Cli	ient	:		Thi	rdi C	Group c/- Vara	a Consulting					roject No		P3627
		ojed cati					Gosforth Anan ambah Rd. G	nbah Rd osforth NSW :	2320				ogged B		N P
				xca	avati		24.4.24	Northing	6384658.00	Slope	90			uipment	
							on 24.4.24	Easting	357844.00	Bearing				ound Lev	
Е	ХС	AVA	ATIC	NC				MATERIA	L DESCRIPTION				TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Motion .	Water	RL (m)	Depth (m)	Graphic Log	Classification		Descri (soil type: pl colour and o	ption of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
					W.W/	CL- Cl			ium plasticity, grey				1		TOPSOIL
ш	ı		+			CI- CH	Sandy Gravelly coarse grained,	CLAY: medium to angular to subang	high plasticity, grey, brow Jular gravel, fine to mediur	n, fine to n grained sand	>PL	F	1 7		RESIDUAL SOIL DCP:-/90mm HB
			1			SC	Extremely weath coarse grained,		ecovered as Clayey SAN	D, fine to					EXTREMELY WEATHERED ROCK
Jatgel R. P.	<u>:</u>	4	15	1			coarse grained,	brown, grey			D	VD		В	
EP LIB 05.G1B LQ CW NON-CORED BOREHOLE LOG EP3827 THIRDI GOSFORTH ANAMBAH RD 0.1 AN GPJ <cdrawingrile>> 22/05/2024 15:04 10.03:00.09 Developed by Datge</cdrawingrile>					· · · · ·		Test Pit TP32-P	Terminated at 1.2	20 m						Refusal
EP LIB US.GLB LOG CW NON-CC	Remarks:														

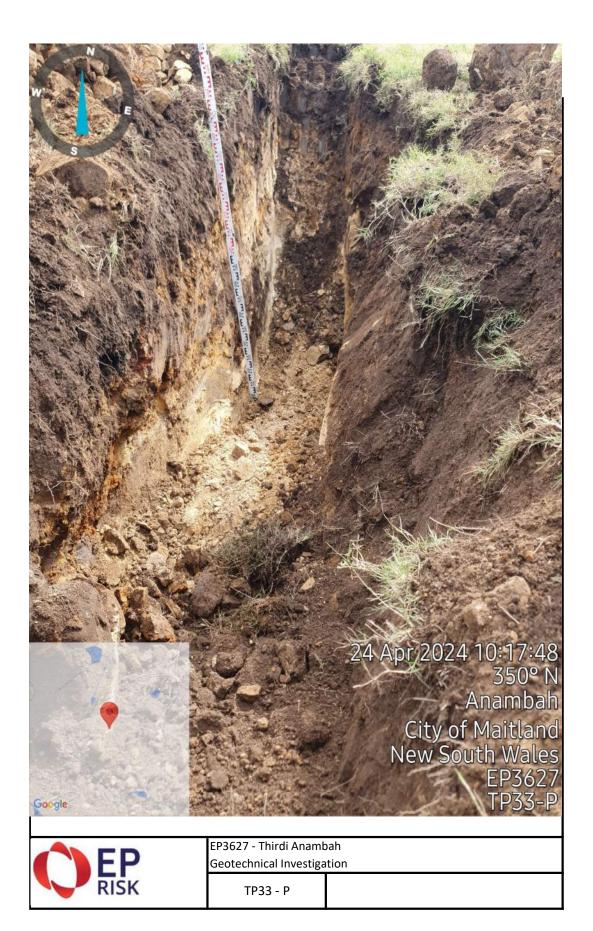




Test Pit No: TP33-P

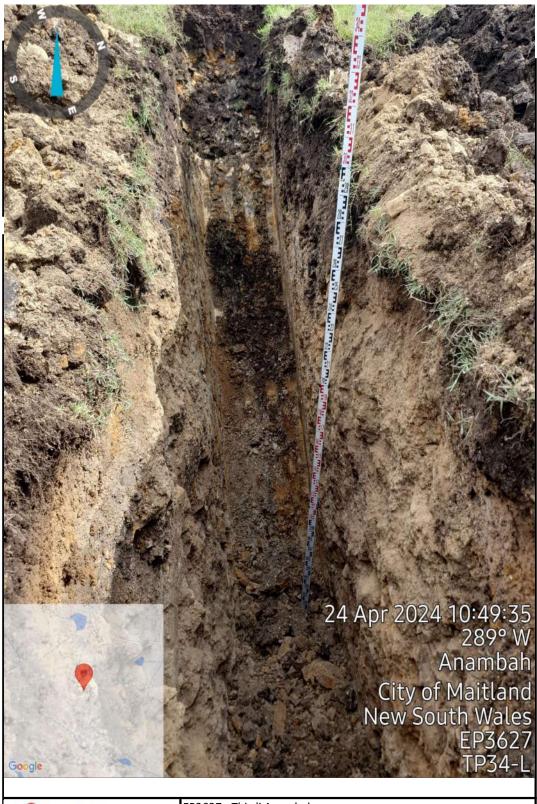
Engineering Log - Test Pit

	Clie	ent		Th	irdi (Group c/- Vara	a Consulting				P	roject No). E	P3627		
		ject	_	Th	irdi (Gosforth Anan	nbah Rd	2220			L	Logged By AN Checked By OP				
		atio					osforth NSW		Clana							
				avat Exca		24.4.24 on 24.4.24	Northing Easting	6384794.00 357810.00	Slope Bearing		0° -		uipment ound Lev			
E	KCA	VAT	ION				MATERIA			TESTI	NG, SA	MPLING & OTHER INFORMATION				
Method	Water	RL (m)	Depth (m)	1	Classification		(soil type: pl	ption of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)		
			Ţ	W.W.	CL- CI	TOPSOIL: Silty	CLAY: low to med	ium plasticity, dark grey		~PL		2		TOPSOIL		
			+		CI- CH	Sandy CLAY: m grained grained		sticity, grey, brown, fine to me	dium	~PL to >PL	F to St	2 5		RESIDUAL SOIL DCP:-HB		
ш		57 .	+ + + + + + + + +		SC	Extremely weat coarse grained,		ecovered as Clayey SAND, f	ine to					EXTREMELY WEATHERED ROCK		
0.03.00.09 Developed by Datgel		-	 - - - - -							D	VD		В			
15:04 1			+													
EP LB 05/GLB Log CW NON-CORED BOREHOLE LOG EP3827 THIRDI GOSFORTH ANAMBAH RD 0.1 AN GPJ < <drawingfile>> 22/05/2024 15;04 10:03:00:09 Developed by Dargel R</drawingfile>		55.				Test Pit TP33-F	Terminated at 1.8	90 m						Refusal		
-P LIB U3.6LB L09	Rei	nark	4 s:	1												



Engineering Log - Test Pit

(Clier	nt		Thi	rdi (Group c/- Vara	a Consulting				Р	roject No	р. Е	P3627
	Proje ∟oca					Gosforth Anan ambah Rd, G		2320				ogged B hecked		N OP
			Exca	avati		24.4.24	Northing	6384824.00	Slope	90	0°		uipment	23T Excavator
-				Exca	vatio	on 24.4.24	Easting	357735.00	Bearing	-	-	Gro	ound Le	vel 57 AHD
EX	EXCAVATION MATERIAL DESCRIPTION											TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		Descr (soil type: p colour and c		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)	
		-	_	WW.	CL- CI	TOPSOIL: Silty	CLAY: low to med	dium plasticity, dark grey				3 5		TOPSOIL
		-	- - -		CI- CH	coarse grained,	CLAY: medium to angular to suban dstone) boulders	high plasticity, grey, brogular gravel, fine to medi	own, fine to um grained	~PL	St to VSt	5 3 7 7		RESIDUAL SOIL
		-	_		CI- CH			recovered as Sandy CLA to coarse grained	AY, medium to			9		EXTREMELY WEATHERED ROCK
		-	_									7		DCP:-/40mm HB
atgel		56	1											
eloped by D		-	-											
3.00.09 Dev		_	_											
EP LIB 05/GLB Log CW NON-CORED BOREHOLE LOG EP3827 THIRDI GOSFORTH ANAMBAH RD 0.1 AN GPJ <-DrawingFile>> 22/05/2024 15.04 10.03.00.09 Developed by Datgel		-	_											
22/05/2024		- - 55								<pl< td=""><td>н</td><td></td><td></td><td></td></pl<>	н			
wingFile>>		_	_											
GPJ < <dra< td=""><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></dra<>		-												
KD 0.1 AN.		-												
ANAMBAH		-	_											
OSFUKIH		54	3											
H KD		-				Test Pit TP34-L	Terminated at 3.0	00 m						Target depth
EP362/ II		-	_											
JOLE LOG		-	-											
ED BORE		-												
NON-COX		-	_											
5 F	Rem	₅₃ arks	<u>4</u>											
LIB 05.GLB														
<u> </u>														





Test Pit No: TP35-P

Engineering Log - Test Pit

F	Clier Proje Loca			Thi	rdi C	Group c/- Vara Consulting Gosforth Anambah Rd nambah Rd, Gosforth NSW 2320					L	roject No ogged B	у А	P3627 N DP
				avati Exca		24.4.24 on 24.4.24	Slope Bearing	9:	0° -		uipment ound Lev			
EX	EXCAVATION MATERIAL DESCRIPTION											TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: pl	ption of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
				WW\ 	CL- CI	TOPSOIL: Silty	CLAY: low to med	ium plasticity, dark grey				1		TOPSOIL
		-	- - -		CI- CH	Silty CLAY: med	lium to high plastic	ity, grey, red		~PL	F to St	1 3 4 6 7		RESIDUAL SOIL
F		47 46 45 45	1	A	SC	to coarse graine		ecovered as Clayey Gravelly ine to coarse grained sand, i ular gravel		D	VD	13 19	В	EXTREMELY WEATHERED ROCK
F	Rem	- - - - - - - - - - - - - - - - - - -				rest Pit TP35-P	Terminated at 3.0	u m						Target depth





Engineering Log - Test Pit

	Clier	nt		Thi	irdi (Group c/- Vara	a Consulting					P	roject No	о. Е	P3627		
ı	⊃roje	ect		Thi	irdi (Gosforth Anan	nbah Rd	2220				L	ogged By AN				
	Loca					ambah Rd, G				·lone		,					
				avati Exca		23.4.24 on 23.4.24	Northing Easting	6384570.00 357500.00		Slope Searing		90° Equipment 23T Excavator Ground Level 56 AHD					
EX	EXCAVATION MATERIAL DESCRIPTION												TESTI	NG, SA	MPLING & OTHER INFORMATION		
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		Descr (soil type: p colour and d)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)			
		-	-	W.W.	CL- CI	TOPSOIL: Sand medium sand	dy CLAY: low to n	nedium plasticity, dark g	grey, fine to		<pl< td=""><td></td><td>2</td><td></td><td>TOPSOIL</td></pl<>		2		TOPSOIL		
		- - -	- - -		CI- CH	Sandy Gravelly grained, subang	CLAY: medium to gular to angular gr	o high plasticity, grey, fir avel, fine to medium gra	ne to coarse ained sand	9	>PL	F and St	1 1 3 2 5		RESIDUAL SOIL		
EP LIB 05 GIB Log CW NON-CORED BOREHOLE LOG EP3627 THIRDI GOSFORTH ANAMBAH RD 0.1 ANI GPJ <-DrawingFile>> 22/05/2024 15:04 10.03.00.09 Developed by Daigel		55	11		CH		hered Sandstone prown, fine to coar	recovered as Sandy Cl	LAY, mediui	n to	<pl< td=""><td>н</td><td>15</td><td>В</td><td>EXTREMELY WEATHERED ROCK DCP:-HB</td></pl<>	н	15	В	EXTREMELY WEATHERED ROCK DCP:-HB		
LIB 05/GLB Log CW NON-CORED BOREHOLE LOG E1382/ I HIRAU GC	Rem	53	3 			Test Pit TP36-L	Terminated at 3.	00 m							Target depth		

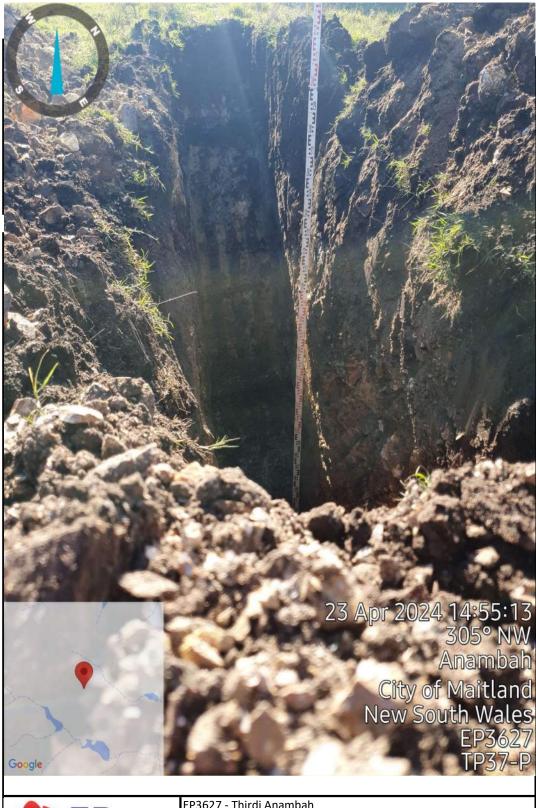




Test Pit No: TP37-P

Engineering Log - Test Pit

	Clie	nt		Thi	irdi (Group c/- Vara	Consulting					roject Na	, F	P3627			
	Project Thirdi Gosforth Anambah Rd L												Project No. EP3627 Logged By AN				
	Loc	atior	1	559	9 An	ambah Rd, G	osforth NSW	2320			С	hecked	Ву С)P			
				avati		23.4.24	Northing	6384452.00	Slope		90° Equipment 23T Excavator						
_					vatio	on 23.4.24	Easting	357571.00	Bearing		-		ound Lev				
E.	EXCAVATION MATERIAL DESCRIPTION												NG, SA	MPLING & OTHER INFORMATION			
Method	Water	RL (m)	Depth (m)		Classification		Descri (soil type: pi colour and c		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)				
			I	W.W.	CL- CI	TOPSOIL: Silty	CLAY: low to med	ium plasticity, dark grey		~PL		1 3		TOPSOIL			
			 - -		CI- CH			high plasticity, grey, brow ular gravel, fine to coarse		<pl< td=""><td>F and St</td><td></td><td></td><td>RESIDUAL SOIL</td></pl<>	F and St			RESIDUAL SOIL			
		48_	+		SC		hered Sandstone i grey, red and bro	ecovered as Clayey SANI wn,	D, fine to			12		EXTREMELY WEATHERED ROCK			
.00.09 Developed by Datgel		-	† ' † † †			1.50m: Become	s grey, green and	brown		D	VD						
2024 15:04 10.03. F			<u>+</u> - -		CI- CH	Extremely weat	hered Mudstone re	ecovered as Sandy CLAY, coarse gained sand	medium to								
EP LIB 05/GLB Log CW NON-CORED BOREHOLE LOG EP3827 THIRDI GOSFORTH ANAMBAH RD 0.1 AN GPJ <-DrawingFile>> 22/05/2024 15.04 10.03.00.09 Developed by Dargel		47 _	2							< <pl< td=""><td>Н</td><td></td><td>В</td><td></td></pl<>	Н		В				
ZZ THIRDI GOSFORTH ANAMB		46 _	3														
CW NON-CORED BOREHOLE LOG EP30		_				Test Pit TP37-P	Terminated at 3.2	20 m						Target depth			
EP LIB 05.GLB Log	Rer	nark	s:														



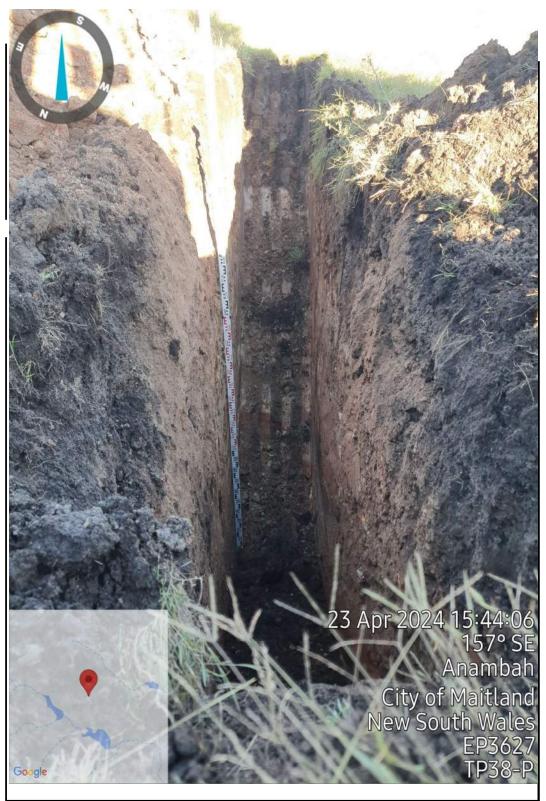


TP37 - P

Test Pit No: TP38-P

Engineering Log - Test Pit

F	Clier Proje	ect		Thi	irdi (Group c/- Vara Consulting Gosforth Anambah Rd nambah Rd, Gosforth NSW 2320						roject No	у А	EP3627 .N
	Start			avati	on	23.4.24 Northing 6384336.00 Slo ion 23.4.24 Easting 357610.00 Bea					0° -		uipment ound Le	
EX	EXCAVATION MATERIAL DESCRIPTION											TESTI	NG, SA	MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		(soil type: pl	ption of Soil asticity/grainsize, ther components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
				₩ <u>₩</u>	CL- CI	TOPSOIL: Silty	CLAY: low to med	lium plasticity, dark grey				1		TOPSOIL
		-	_		CI- CH	Silty CLAY: med	lium to high plastio	city, brown		~PL	F	1 1 1		SLOPE WASH
		- -	_		CI- CH	Sandy CLAY: m sand	redium to high plasticity, grey, brown, fine to coarse grain			>PL	St to VSt	4 4 6		RESIDUAL SOIL
		- - 46	_		SC	Extremely weath coarse, grey, red	nered Sandstone i d and brown, with	recovered as Clayey SAN ferruginous cementations	ID, fine to s (50-150mm)			13		EXTREMELY WEATHERED ROCK DCP:-/50mm HB
F		46								D to M	VD		В	
	- Dam		3			Test Pit TP38-P	Terminated at 3.0	00 m						Target depth
	veiii	arks	••											



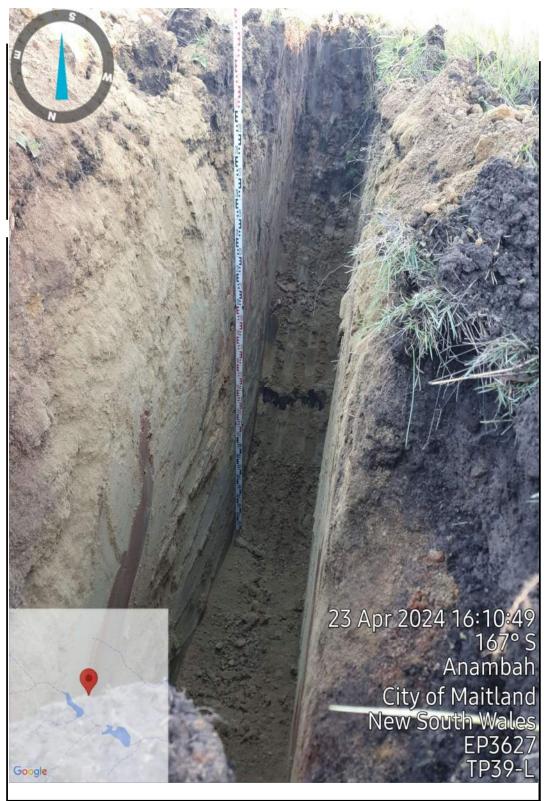


EP3627 - Thirdi Anambah Geotechnical Investigation

Engineering Log - Test Pit

SHEET 1 OF 1

	Clier	nt		Thi	rdi (Group c/- Vara	. Consulting				P	roject No) F	P3627
	⊃roj∈	ect		Thi	rdi C	Sosforth Anan	nbah Rd				L	ogged B	у А	.N
	_oca					ambah Rd, G				Checked By OP				
				avati Exca		23.4.24 on 23.4.24	Northing Easting	6384306.00 357472.00	Slope Bearing	90° Equipment 23T Excavator g Ground Level 43 AHD				
	CAV							L DESCRIPTION						MPLING & OTHER INFORMATION
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		Descr	iption of Soil lasticity/grainsize, other components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
		_		₩W)	CL- Cl	TOPSOIL: Silty	CLAY: low to med	dium plasticity, dark grey		~PL		1		TOPSOIL
		-	_		CL- CI	sand		n plasticity, grey, fine to m		>PL	VS to F	0 1 1 2		SLOPE WASH
		-	_		CI- CH	Sandy CLAY: m sand	edium to high pla	sticity, brown, grey, fine to	o coarse grained		St VS to H	10		RESIDUAL SOIL
EP LIB 05 GLB Log CW NON-CORED BOREHOLE LOG EP3627 THIRDI GOSFORTH ANAMBAH RD 0.1 ANI GPJ <-DrawingFile>> 22/05/2024 15:04 10.03.00.09 Developed by Datgel		41	1		SC	coarse grained,	nered Sandstone grey, red and bro		ND, fine to	D to M	VD	16		EXTREMELY WEATHERED ROCK DCP:-/90mm HB
LIB 05.GLB LOG C	Rem	l39 Iarks	<u> 4</u> 5:											
<u>і</u>														





EP3627 - Thirdi Anambah Geotechnical Investigation

TP39 - L

Test Pit No: TP40-P

Engineering Log - Test Pit

SHEET 1 OF 1

		Clien						a Consulting					roject No		P3627
		roje oca	ect tion				Sosforth Ana ambah Rd, 0	mbah Rd Gosforth NSW	2320				ogged B hecked		N P
					avati		24.4.24	Northing Easting	6384496.00 358135.00	Slope Bearing					
ŀ	Completed Excavation 24.4.24 Easting 358135.00 Bearing EXCAVATION MATERIAL DESCRIPTION								Беаппу					MPLING & OTHER INFORMATION	
	Method	Water	RL (m)	Depth (m)	Graphic Log	Classification		Desc	ription of Soil plasticity/grainsize, other components)		Moisture Condition	Consistency	Tests DCP Results (blows/ 100mm)	Samples	Additional Comments (material origin, pocket penetrometer values, investigation observations)
			-	_	W.W.	CL- CI	TOPSOIL: Silty	y CLAY: low to me	edium plasticity, dark grey		~PL		2		TOPSOIL
			-	-		CI- CH	Silty CLAY: me	edium to high plas	ticity, brown, yellow		~PL	F to St	2 2 2 3		RESIDUAL SOIL
Datgel			32	1		SC	Extremely wear coarse grained	thered Sandstone I, dark brown with	recovered as Clayey SAN fine to coarse grained, sub	ID, fine to angular gravel			7 7 7 10 12 9		EXTREMELY WEATHERED ROCK
< <drawingfile>> 22/05/2024 15:04 10.03.00.09 Developed by Datgel</drawingfile>	Е		- - - - - - 31								M to D	VD	10 10		DCP:-/50mm HB
SOSFORTH ANAMBAH RD 0.1 AN.GPJ < <draw< td=""><td></td><td></td><td>- - - - - 30</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>D</td><td></td></draw<>			- - - - - 30											D	
EP LIB 05.GLB Log CW NON-CORED BOREHOLE LOG EP3627 THIRDI GOSFORTH ANAMBAH RD 0.1 AN.GPJ							Test Pit TP40-	P Terminated at 3							Target depth
EP LIB 05.GLB Log	F	Rem	arks	5:		1									





EP3627 - Thirdi Anambah Geotechnical Investigation



Appendix E LABORATORY TEST RESULTS



Postal: 2/15 Miall Way Albion Park Rail NSW 2527 Lab: 13/31 Riverside Drive, Mayfield West NSW 2304

Telephone: 02 4256 1684

E-Mail: joe.stallard@asct.com.au

Mobile: 0421 989 919 A.B.N. 34 635 062 609

Report No:

Report Date:

Report Page:

Request/Order:

Project No:

Lot Number: ITP/PCP Number:

Control Line:

Report on Material Quality WB080 - Rev 32, 28/11/2023

Client Address: 3/19 Bolton Street, Newcastle NSW 2300

Project: **Material Testing**

Works Component: Thirdi Gorforth Anambah Road

EP Risk

Material Used:

Material Description: Refer to logs

Lot Comments:

Client:

Laboratory testing 02/05/2024 to 07/05/2024

Lab Test Date/s:

Sample Date Sample Number Offset Level of Test Test Depth Chainage/Location 12419 22/04/2024 TP01-L 1.50-2.50

Sampling & Test Methods (Results relate only to the items sampled/tested)

Sampled by Customer: Results apply to the sample/s as received. ** AS 1289.3.6.1 Coarse: (2009)Particle size distribution of a soil

AS 1289.3.1.1: (2009) Determination of Liquid Limit (4 point Casagrande)

AS 1289.3.3.1: (2009)Calculation of the Plastic Index of a soil

(** NATA accreditation does not cover the performance of this service)

17-22-MQ

14/05/2024

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EP3627

17

AS 1289.1.1: (2001)Preparation of disturbed soil samples AS 1289.3.6.1 Fine: (2009)Particle size distribution of a soil

AS 1289.3.2.1: (2009) Determination of the Plastic Limit

AS 1289.3.4.1: (2008)Determination of the Linear Shrinkage of a soil

Report Remarks & Endorsement

NATA

Issued By:

J.Edmunds Approved Signatory

Kelmondo

Accredited for compliance with ISO/IEC 17025 - Testing.

> Lab Site Number: 25677 Base Lab Accreditation: 20656 Base Lab Name: ASCT Illawarra

Specification Name				
Particle Size Distribution (WASHED)	Units	Result	Specification Limits	Graphical Representation
Passing 150mm Sieve	%			Pautiala Ciaa Diatuihautiau
Passing 125mm Sieve	%			Particle Size Distribution
Passing 100mm Sieve	%			
Passing 75.0mm Sieve	%			90
Passing 63.0mm Sieve	%			
Passing 53.0mm Sieve	%			80
Passing 37.5mm Sieve	%	100		70
Passing 31.5mm Sieve	%			
Passing 26.5mm Sieve	%	98		60
Passing 19.0mm Sieve	%	97		<u> %</u>
Passing 16.0mm Sieve	%			60 %) But 150 150 158
Passing 13.2mm Sieve	%	91		8 4
Passing 9.5mm Sieve	%	87		
Passing 6.7mm Sieve	%	83		30
Passing 4.75mm Sieve	%	79		
Passing 2.36mm Sieve	%	74		20
Passing 1.18mm Sieve	%	70		
Passing 0.600mm Sieve	%	68		10
Passing 0.425mm Sieve	%	66		0
Passing 0.300mm Sieve	%	64		150 190 75 26.5. 26.5. 119.0 119.0 11.3. 2.3. 6.7 4.75 2.3. 0.40 0.40 0.40 0.40 0.00
Passing 0.150mm Sieve	%	58		
Passing 0.075mm Sieve	%	44		35 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
Passing 0.0135mm Sieve	%			5.555



Postal: 2/15 Miall Way Albion Park Rail NSW 2527 Lab: 13/31 Riverside Drive, Mayfield West NSW 2304

17-22-MQ

14/05/2024

Page 2 of 2

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EP3627

Telephone: 02 4256 1684

E-Mail: joe.stallard@asct.com.au

Mobile: 0421 989 919 A.B.N. 34 635 062 609

Report No:

Report Date:

Report Page:

Project No:

Report on Material Quality

Client: Client Address: 3/19 Bolton Street, Newcastle NSW 2300

EP Risk

Project: **Material Testing**

Works Component: Thirdi Gorforth Anambah Road

Material Used:

Material Description: Refer to logs

Lot Comments:

Lab Test Date/s: Laboratory testing 02/05/2024 to 07/05/2024 Request/Order: Lot Number:

ITP/PCP Number: Control Line:

Sample Date Chainage/Location Offset Test Depth Sample Number **Level of Test** 12419 22/04/2024 TP01-L 1.50-2.50

Plasticity	Units	Result	Specification Limits	Remarks
Liquid Limit	%	40		Oven Dried & Dry Sieved
Plastic Limit	%	17		Oven Dried & Dry Sieved
Plastic Index	%	23		Oven Dried & Dry Sieved
Linear Shrinkage	%	10.5		



Postal: 2/15 Miall Way Albion Park Rail NSW 2527 Lab: 13/31 Riverside Drive, Mayfield West NSW 2304

17-23-CBR

15/05/2024

Page 1 of 1

EP3627

02 4256 1684 Telephone:

E-Mail: joe.stallard@asct.com.au

Mobile: 0421 989 919 34 635 062 609 A.B.N.

Report on AS CBR and MDD

Client Address: 3/19 Bolton Street, Newcastle NSW 2300

Project: **Material Testing**

Works Component: Thirdi Gorforth Anambah Road

Material Used(Source):

Client:

Material Description: Refer to logs

Lot Boundaries:

Lab Test Date/s:

Laboratory testing 29/04/2024 to 15/05/2024

Lot Number: ITP/PCP Number: Control Line:

Report No:

Report Date:

Report Page:

Test Request/Order:

Project No:

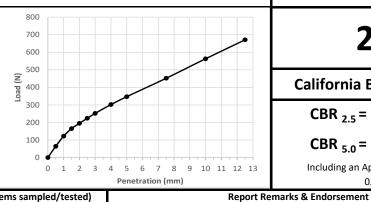
Sample Number Sample Date Chainage/Location Offset **Level of Test Test Depth** TP02-P 12420 22/04/2024 1.50-2.10

Parameters	Units	Test Results		Information
Pretreatment Regime		No Pretreatment		
Portion Retained on AS Sieve	%	0% on 19mm		Retained material excluded from CBR
Material Plasticity (Liquid Limit)		High (More than 50%)		By Technician's Assessment
Sample Curing Time	hrs	MDD = 96 hrs	CBR = 112 hrs	
Soil Particle Density	t/m3	2.65		Estimated value only**
Maximum Dry Density (MDD)	t/m3	1.38		Standard compactive effort
Optimum Moisture Content (OMC)	%	32.0		
Field Moisture Content	%	Field 31.8 %		Passing 19.0mm portion
Compaction Moisture Content	%	Achieved 31.6 %	LMR = 99.5%	Specified LMR = 100%
Compaction Dry Density	t/m3	Achieved 1.38 t/m3	LDR = 100.5%	Specified LDR = 100%
Surcharge Load	kg	4.5		
Period of Soaking	Days	Soaked - 4 Days		Dry Density (after soaking) = 1.35 t/m3.
Specimen Swell	%	3.0		
Moisture Content - Top 30mm	%	37.3		After Penetration
Moisture Content - Remaining	%	33.0		After Penetration

Dry Density Vs Moisture Content

1.42 1.40 1.38 1.36 1.34 1.32 1.30 1 28 26.0 27.0 28.0 29.0 30.0 31.0 32.0 33.0 34.0 35.0

Load-Penetration Curve



Material CBR Value (%)

California Bearing Ratios

CBR _{2.5} = 1.5

CBR _{5.0} = 2.0

Including an Applied Correction of 0.0 mm

Sampling & Test Methods (Results relate only to the items sampled/tested)

Sampled by Customer: Results apply to the sample/s as received. **

AS 1289.1.1: (2001)Preparation of disturbed soil samples

AS1289.2.1.1: (2005) Moisture Content of a Soil (Oven Drying)

Moisture Content (%)

AS1289.5.1.1: (2017) Dry Density/Moisture content relation of a soil (Standard)

AS1289.6.1.1: (2014)California Bearing Ratio of a soil (remoulded specimen)

Issued By:

J.Edmunds

Kelmendo

Accredited for compliance with ISO/IEC 17025 - Testing.

Approved Signatory

Lab Site Number: 25677 Base Lab Accreditation: 20656

Base Lab Name: ASCT Illawarra

WB011 - Rev 33, 05/02/2024



Postal: 2/15 Miall Way Albion Park Rail NSW 2527 Lab: 13/31 Riverside Drive, Mayfield West NSW 2304

Telephone: 02 4256 1684

E-Mail: joe.stallard@asct.com.au

Mobile: 0421 989 919 A.B.N. 34 635 062 609

Report No:

Report Date:

Report Page:

Request/Order:

Project No:

Lot Number: ITP/PCP Number:

Control Line:

WB080 - Rev 32, 28/11/2023 Report on Material Quality

Client: EP Risk
Client Address: 3/19 Bolton Street, Newcastle NSW 2300

Project: Material Testing

Works Component: Thirdi Gorforth Anambah Road

Material Used: -

Material Description: Refer to logs

Lot Comments:

Lab Test Date/s: Laboratory testing 02/05/2024 to 06/05/2024

Sample Number Sample Date Chainage/Location Offset Level of Test Depth
12422 22/04/2024 TP07-P - - 1.00-1.50

Sampling & Test Methods (Results relate only to the items sampled/tested)

Sampled by Customer: Results apply to the sample/s as received. **

AS 1289.3.6.1 Coarse: (2009)Particle size distribution of a soil

AS 1289.3.1.1: (2009)Determination of Liquid Limit (4 point Casagrande)

AS 1289.3.3.1: (2009) Calculation of the Plastic Index of a soil ${\sf AS}$

(** NATA accreditation does not cover the performance of this service)

17-25-MQ

14/05/2024

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AS 1289.1.1: (2001)Preparation of disturbed soil samples AS 1289.3.6.1 Fine: (2009)Particle size distribution of a soil

AS 1289.3.2.1: (2009) Determination of the Plastic Limit

AS 1289.3.4.1: (2008) Determination of the Linear Shrinkage of a soil

Report Remarks & Endorsement



Issued By:

J.Edmunds
Approved Signatory

Kelmindo

Accredited for compliance with ISO/IEC 17025 - Testing.

Lab Site Number: 25677

Base Lab Accreditation: 20656

Base Lab Name: ASCT Illawarra

Specification Name				
Particle Size Distribution (WASHED)	Units	Result	Specification Limits	Graphical Representation
Passing 150mm Sieve	%			Particle Size Distribution
Passing 125mm Sieve	%			100 -
Passing 100mm Sieve	%			
Passing 75.0mm Sieve	%			90
Passing 63.0mm Sieve	%			<u> </u>
Passing 53.0mm Sieve	%			80
Passing 37.5mm Sieve	%			70
Passing 31.5mm Sieve	%			
Passing 26.5mm Sieve	%			60
Passing 19.0mm Sieve	%	100		
Passing 16.0mm Sieve	%			60 %) Suiso Suisse 40
Passing 13.2mm Sieve	%	78] &
Passing 9.5mm Sieve	%	71		
Passing 6.7mm Sieve	%	65		30
Passing 4.75mm Sieve	%	60] [] / /
Passing 2.36mm Sieve	%	51		20
Passing 1.18mm Sieve	%	45] [
Passing 0.600mm Sieve	%	38		10
Passing 0.425mm Sieve	%	33		0
Passing 0.300mm Sieve	%	28		150 100 75 37 26.5 26.5 119.0 119.0 119.0 11.2 9.5 4.75 0.30 0.40 0.40 0.00
Passing 0.150mm Sieve	%	21		1 () (1 () () ()
Passing 0.075mm Sieve	%	15		31.5 Sieve Aperture (mm)
Passing 0.0135mm Sieve	%			Sieve Aperture (IIIII)



Postal: 2/15 Miall Way Albion Park Rail NSW 2527 Lab: 13/31 Riverside Drive, Mayfield West NSW 2304

Telephone: 02 4256 1684

E-Mail: joe.stallard@asct.com.au

0421 989 919 Mobile: A.B.N. 34 635 062 609

Report No:

WB080 - Rev 32, 28/11/2023 **Report on Material Quality**

Client: EP Risk Client Address: 3/19 Bolton Street, Newcastle NSW 2300

Project: **Material Testing**

Works Component: Thirdi Gorforth Anambah Road

Material Used:

Sample Number

Material Description: Refer to logs

Lot Comments:

Lab Test Date/s: Sample Date

Laboratory testing 02/05/2024 to 06/05/2024

Chainage/Location

Report Date: Report Page: 17-25-MQ 14/05/2024 Page 2 of 2

Test Depth

Project No: 17 Request/Order:

Lot Number:

Offset

EP3627

ITP/PCP Number:

Control Line:

Level of Test

12422	22/04/2024		TP07-P		-	-	1.00-1.50
Plasticity		Units	Result	Specification Limits	Remarks		

Plasticity	Units	Result	Specification Limits	Remarks
Liquid Limit	%	39		Oven Dried & Dry Sieved
Plastic Limit	%	17		Oven Dried & Dry Sieved
Plastic Index	%	22		Oven Dried & Dry Sieved
Linear Shrinkage	%	8.5		



Offset

Postal: 2/15 Miall Way Albion Park Rail NSW 2527 Lab: 13/31 Riverside Drive, Mayfield West NSW 2304

02 4256 1684 Telephone:

E-Mail: joe.stallard@asct.com.au

Mobile: 0421 989 919 34 635 062 609 A.B.N.

Report on AS CBR and MDD

Client Address: 3/19 Bolton Street, Newcastle NSW 2300

Sample Date

22/04/2024

Project: **Material Testing**

Works Component: Thirdi Gorforth Anambah Road

Material Used(Source):

Client:

Material Description: Refer to logs

Lot Boundaries:

12423

Lab Test Date/s: Sample Number Laboratory testing 29/04/2024 to 15/05/2024

Chainage/Location

TP09-P

Report No: 17-26-CBR Report Date: 15/05/2024 Report Page: Page 1 of 1

Project No: Test Request/Order: EP3627

Lot Number: ITP/PCP Number:

Control Line: **Level of Test Test Depth**

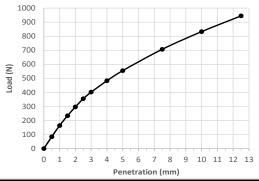
1.10-1.50

Parameters	Units	Test Results		Information
Pretreatment Regime		No Pretreatment		
Portion Retained on AS Sieve	%	0% on 19mm		Retained material excluded from CBR
Material Plasticity (Liquid Limit)		High (More than 50%)		By Technician's Assessment
Sample Curing Time	hrs	MDD = 96 hrs	CBR = 163 hrs	
Soil Particle Density	t/m3	2.67		Estimated value only**
Maximum Dry Density (MDD)	t/m3	1.54		Standard compactive effort
Optimum Moisture Content (OMC)	%	26.5		
Field Moisture Content	%	Field 26.3 %		Passing 19.0mm portion
Compaction Moisture Content	%	Achieved 26.8 %	LMR = 101.5%	Specified LMR = 100%
Compaction Dry Density	t/m3	Achieved 1.53 t/m3	LDR = 99.5%	Specified LDR = 100%
Surcharge Load	kg	4.5		
Period of Soaking	Days	Soaked - 4 Days		Dry Density (after soaking) = 1.50 t/m3.
Specimen Swell	%	2.0		
Moisture Content - Top 30mm	%	32.0		After Penetration
Moisture Content - Remaining	%	28.0		After Penetration

Dry Density Vs Moisture Content

1.58 1.56 1.54 1.52 1.50 1.48 1.46 1 44 21.0 22.0 23.0 24.0 25.0 26.0 27.0 28.0 29.0 30.0 Moisture Content (%)

Load-Penetration Curve



Material CBR Value (%)

California Bearing Ratios

CBR _{2.5} = 2.5

CBR _{5.0} = 3.0

Including an Applied Correction of 0.0 mm

Sampling & Test Methods (Results relate only to the items sampled/tested)

Sampled by Customer: Results apply to the sample/s as received. **

AS 1289.1.1: (2001)Preparation of disturbed soil samples

AS1289.2.1.1: (2005) Moisture Content of a Soil (Oven Drying)

AS1289.5.1.1: (2017) Dry Density/Moisture content relation of a soil (Standard)

AS1289.6.1.1: (2014)California Bearing Ratio of a soil (remoulded specimen)

Report Remarks & Endorsement



Issued By:

J.Edmunds

Kelmindo

Accredited for compliance with ISO/IEC 17025 - Testing.

Approved Signatory 25677

Lab Site Number: Base Lab Accreditation: 20656

Base Lab Name: ASCT Illawarra

WB011 - Rev 33, 05/02/2024



Postal: 2/15 Miall Way Albion Park Rail NSW 2527 Lab: 13/31 Riverside Drive, Mayfield West NSW 2304

02 4256 1684 Telephone:

E-Mail: joe.stallard@asct.com.au

Mobile: 0421 989 919 34 635 062 609 A.B.N.

Report on AS CBR and MDD

Client Address: 3/19 Bolton Street, Newcastle NSW 2300

Sample Date

22/04/2024

Project: **Material Testing**

Works Component: Thirdi Gorforth Anambah Road

Material Used(Source):

Client:

Material Description: Refer to logs

Lot Boundaries:

12424

Lab Test Date/s: Sample Number Laboratory testing 29/04/2024 to 15/05/2024

Chainage/Location

TP15-P

Report No: Report Date:

17-27-CBR 15/05/2024 Page 1 of 1

Report Page: Project No:

Test Request/Order: EP3627

Lot Number: ITP/PCP Number: Control Line:

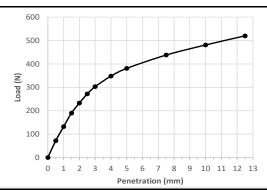
Offset **Level of Test Test Depth** 0.20-0.60

Parameters	Units	Test Results		Information
Pretreatment Regime		No Pretreatment		
Portion Retained on AS Sieve	%	0% on 19mm		Retained material excluded from CBR
Material Plasticity (Liquid Limit)		High (More than 50%)		By Technician's Assessment
Sample Curing Time	hrs	MDD = 97 hrs	CBR = 164 hrs	
Soil Particle Density	t/m3	2.67		Estimated value only**
Maximum Dry Density (MDD)	t/m3	1.46		Standard compactive effort
Optimum Moisture Content (OMC)	%	29.0		
Field Moisture Content	%	Field 33.2 %		Passing 19.0mm portion
Compaction Moisture Content	%	Achieved 29.5 %	LMR = 101.0%	Specified LMR = 100%
Compaction Dry Density	t/m3	Achieved 1.45 t/m3	LDR = 99.5%	Specified LDR = 100%
Surcharge Load	kg	4.5		
Period of Soaking	Days	Soaked - 4 Days		Dry Density (after soaking) = 1.41 t/m3.
Specimen Swell	%	3.0		
Moisture Content - Top 30mm	%	36.4		After Penetration
Moisture Content - Remaining	%	31.4		After Penetration

Dry Density Vs Moisture Content

1.50 1.48 1 46 1.44 1.42 1.40 1.38 1.36 25.0 26.0 27.0 28.0 29.0 30.0 31.0 32.0 33.0 Moisture Content (%)

Load-Penetration Curve



Material CBR Value (%)

California Bearing Ratios

CBR _{2.5} = 2.0

CBR _{5.0} = 2.0

Including an Applied Correction of 0.0 mm

Sampling & Test Methods (Results relate only to the items sampled/tested)

Sampled by Customer: Results apply to the sample/s as received. **

AS 1289.1.1: (2001)Preparation of disturbed soil samples

AS1289.2.1.1: (2005) Moisture Content of a Soil (Oven Drying)

AS1289.5.1.1: (2017) Dry Density/Moisture content relation of a soil (Standard)

AS1289.6.1.1: (2014)California Bearing Ratio of a soil (remoulded specimen)

Report Remarks & Endorsement



Issued By:

J.Edmunds

Kelmindo

Accredited for compliance with ISO/IEC 17025 - Testing.

Approved Signatory 25677

Lab Site Number: Base Lab Accreditation: 20656

ASCT Illawarra Base Lab Name:

WB011 - Rev 33, 05/02/2024



Postal: 2/15 Miall Way Albion Park Rail NSW 2527 Lab: 13/31 Riverside Drive, Mayfield West NSW 2304

Telephone: 02 4256 1684

E-Mail: joe.stallard@asct.com.au

Mobile: 0421 989 919 A.B.N. 34 635 062 609

Report Page:

Request/Order:

Project No:

Lot Number: ITP/PCP Number:

Control Line:

Report on Material Quality WB080 - Rev 32, 28/11/2023

Client: EP Risk Report No: Client Address: 3/19 Bolton Street, Newcastle NSW 2300 Report Date:

Project: **Material Testing**

Works Component: Thirdi Gorforth Anambah Road

Material Used:

Material Description: Refer to logs

Lot Comments:

Lab Test Date/s: Laboratory testing 02/05/2024 to 06/05/2024

Sample Date Sample Number Offset Level of Test Test Depth Chainage/Location 12425 22/04/2024 TP18-L 0.20-0.50

Sampling & Test Methods (Results relate only to the items sampled/tested)

Sampled by Customer: Results apply to the sample/s as received. **

AS 1289.3.6.1 Coarse: (2009)Particle size distribution of a soil

AS 1289.3.1.1: (2009) Determination of Liquid Limit (4 point Casagrande) AS 1289.3.3.1: (2009)Calculation of the Plastic Index of a soil

(** NATA accreditation does not cover the performance of this service)

17-28-MQ

14/05/2024

Page 1 of 2

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AS 1289.1.1: (2001)Preparation of disturbed soil samples AS 1289.3.6.1 Fine: (2009)Particle size distribution of a soil

AS 1289.3.2.1: (2009) Determination of the Plastic Limit

AS 1289.3.4.1: (2008)Determination of the Linear Shrinkage of a soil

Report Remarks & Endorsement



Issued By:

J.Edmunds **Approved Signatory**

Kelmindo

Accredited for compliance with ISO/IEC 17025 - Testing.

Lab Site Number: 25677 Base Lab Accreditation: 20656 Base Lab Name: **ASCT Illawarra**

Specification Name				
Particle Size Distribution (WASHED)	Units	Result	Specification Limits	Graphical Representation
Passing 150mm Sieve	%			Poutiele Sine Distuibution
Passing 125mm Sieve	%			Particle Size Distribution
Passing 100mm Sieve	%			
Passing 75.0mm Sieve	%			90
Passing 63.0mm Sieve	%			
Passing 53.0mm Sieve	%			80
Passing 37.5mm Sieve	%			70
Passing 31.5mm Sieve	%			
Passing 26.5mm Sieve	%			_60
Passing 19.0mm Sieve	%	100		60 %) 50 50 50 50 50
Passing 16.0mm Sieve	%			
Passing 13.2mm Sieve	%	100		8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
Passing 9.5mm Sieve	%	100		
Passing 6.7mm Sieve	%	100		30
Passing 4.75mm Sieve	%	100		
Passing 2.36mm Sieve	%	100		20
Passing 1.18mm Sieve	%	99		10
Passing 0.600mm Sieve	%	97		10
Passing 0.425mm Sieve	%	96		0
Passing 0.300mm Sieve	%	95		150 75 26.5:3 37.5 119.0 119.0 119.0 1.19.0 1.10 2.36 2.36 2.36 1.18 1.18 0.300 0.425 0.000 0.000
Passing 0.150mm Sieve	%	91		150 1: 100 1: 1100 1: 1100 1: 1100 1: 1110
Passing 0.075mm Sieve	%	87		35 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
Passing 0.0135mm Sieve	%			5.555



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Report No:

Report Date:

Report Page:

Request/Order:

Project No:

Lot Number:

WB080 - Rev 32, 28/11/2023 **Report on Material Quality**

Client: Client Address: 3/19 Bolton Street, Newcastle NSW 2300

EP Risk

Project: **Material Testing**

Works Component: Thirdi Gorforth Anambah Road

Material Used:

Material Description: Refer to logs

Lot Comments: Lab Test Date/s:

Laboratory testing 02/05/2024 to 06/05/2024

ITP/PCP Number: Control Line:

17-28-MQ

14/05/2024

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EP3627

Sample Date Chainage/Location Offset Level of Test Test Depth Sample Number 12425 22/04/2024 TP18-L 0.20-0.50

Plasticity	Units	Result	Specification Limits	Remarks
Liquid Limit	%	64		Oven Dried & Dry Sieved
Plastic Limit	%	17		Oven Dried & Dry Sieved
Plastic Index	%	47		Oven Dried & Dry Sieved
Linear Shrinkage	%	16.0		



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Report No:

Report Date:

Report Page:

Test Request/Order:

Project No:

Lot Number:

Report on AS CBR and MDD

Client Address: 3/19 Bolton Street, Newcastle NSW 2300

Project: **Material Testing**

Works Component:

Material Used(Source):

Client:

Material Description: Refer to logs

Lot Boundaries:

Lab Test Date/s:

Laboratory testing 29/04/2024 to 15/05/2024

Thirdi Gorforth Anambah Road

ITP/PCP Number: Control Line:

17-30-CBR

15/05/2024

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EP3627

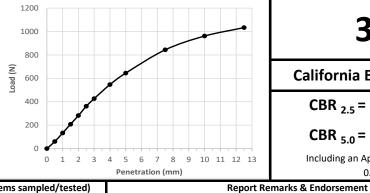
Sample Number Sample Date Chainage/Location Offset **Level of Test Test Depth** 22/04/2024 12427 TP20-P 0.30-0.80

Parameters	Units	Test Results		Information
Pretreatment Regime		No Pretreatment		
Portion Retained on AS Sieve	%	0% on 19mm		Retained material excluded from CBR
Material Plasticity (Liquid Limit)		High (More than 50%)	•	By Technician's Assessment
Sample Curing Time	hrs	MDD = 96 hrs	CBR = 111 hrs	
Soil Particle Density	t/m3	2.67	•	Estimated value only**
Maximum Dry Density (MDD)	t/m3	1.44		Standard compactive effort
Optimum Moisture Content (OMC)	%	30.5		
Field Moisture Content	%	Field 30.1 %		Passing 19.0mm portion
Compaction Moisture Content	%	Achieved 30.1 %	LMR = 98.5%	Specified LMR = 100%
Compaction Dry Density	t/m3	Achieved 1.45 t/m3	LDR = 100.5%	Specified LDR = 100%
Surcharge Load	kg	4.5	•	
Period of Soaking	Days	Soaked - 4 Days		Dry Density (after soaking) = 1.42 t/m3.
Specimen Swell	%	1.5		
Moisture Content - Top 30mm	%	34.7		After Penetration
Moisture Content - Remaining	%	31.0		After Penetration

Dry Density Vs Moisture Content

1.50 1.48 1 46 1.44 1.42 1.40 1.38 1.36 25.0 26.0 27.0 28.0 29.0 30.0 31.0 32.0 33.0

Load-Penetration Curve



Material CBR Value (%)

California Bearing Ratios

CBR _{2.5} = 2.5

CBR _{5.0} = 3.5

Including an Applied Correction of 0.0 mm

Sampling & Test Methods (Results relate only to the items sampled/tested)

Sampled by Customer: Results apply to the sample/s as received. **

AS 1289.1.1: (2001)Preparation of disturbed soil samples

AS1289.2.1.1: (2005) Moisture Content of a Soil (Oven Drying)

Moisture Content (%)

AS1289.5.1.1: (2017) Dry Density/Moisture content relation of a soil (Standard)

AS1289.6.1.1: (2014)California Bearing Ratio of a soil (remoulded specimen)



Issued By:

Kelmendo

Accredited for compliance with ISO/IEC 17025 - Testing.

J.Edmunds Approved Signatory

Lab Site Number: 25677 Base Lab Accreditation: 20656

Base Lab Name: ASCT Illawarra

WB011 - Rev 33, 05/02/2024



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Report on AS CBR and MDD

Client Address: 3/19 Bolton Street, Newcastle NSW 2300

Project: **Material Testing**

Works Component: Thirdi Gorforth Anambah Road

Material Used(Source):

Client:

Material Description: Refer to logs

Lot Boundaries:

Lab Test Date/s: Laboratory testing 29/04/2024 to 15/05/2024 Report No: 17-32-CBR Report Date: 15/05/2024

Report Page: Page 1 of 1

Project No: Test Request/Order: EP3627

Lot Number:

ITP/PCP Number: Control Line:

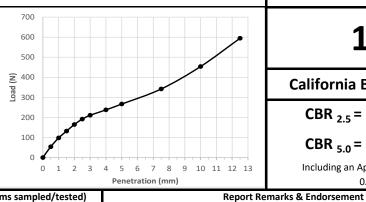
Sample Number	Sample Date	Chainage/Location	Offset	Level of Test	Test Depth
12429	22/04/2024	TP24-P	-	-	0.50-1.00

Parameters	Units	Test Results		Information
Pretreatment Regime		No Pretreatment		
Portion Retained on AS Sieve	%	0% on 19mm		Retained material excluded from CBR
Material Plasticity (Liquid Limit)		High (More than 50%)		By Technician's Assessment
Sample Curing Time	hrs	MDD = 96 hrs	CBR = 163 hrs	
Soil Particle Density	t/m3	2.67		Estimated value only**
Maximum Dry Density (MDD)	t/m3	1.38		Standard compactive effort
Optimum Moisture Content (OMC)	%	33.0		
Field Moisture Content	%	Field 33.2 %		Passing 19.0mm portion
Compaction Moisture Content	%	Achieved 33.4 %	LMR = 101.0%	Specified LMR = 100%
Compaction Dry Density	t/m3	Achieved 1.37 t/m3	LDR = 99.5%	Specified LDR = 100%
Surcharge Load	kg	4.5		
Period of Soaking	Days	Soaked - 4 Days		Dry Density (after soaking) = 1.33 t/m3.
Specimen Swell	%	3.0		
Moisture Content - Top 30mm	%	39.3		After Penetration
Moisture Content - Remaining	%	35.4		After Penetration

Dry Density Vs Moisture Content

1.42 1.40 1.38 1.36 1.34 1.32 1.30 29.0 30.0 31.0 32.0 33.0 34.0 35.0 36.0 37.0 Moisture Content (%)

Load-Penetration Curve



Material CBR Value (%)

California Bearing Ratios

CBR _{2.5} = 1.5

CBR _{5.0} = 1.5

Including an Applied Correction of 0.0 mm

Sampling & Test Methods (Results relate only to the items sampled/tested)

Sampled by Customer: Results apply to the sample/s as received. **

AS 1289.1.1: (2001)Preparation of disturbed soil samples

AS1289.2.1.1: (2005) Moisture Content of a Soil (Oven Drying)

AS1289.5.1.1: (2017) Dry Density/Moisture content relation of a soil (Standard)

AS1289.6.1.1: (2014)California Bearing Ratio of a soil (remoulded specimen)



Issued By: J.Edmunds

Accredited for compliance with ISO/IEC 17025 - Testing.

Approved Signatory

Lab Site Number: 25677 Base Lab Accreditation: 20656

ASCT Illawarra Base Lab Name:

WB011 - Rev 33, 05/02/2024



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Report No:

Report Date:

Report Page:

Request/Order:

Project No:

Lot Number: ITP/PCP Number:

Control Line:

Report on Material Quality

Client: EP Risk
Client Address: 3/19 Bolton Street, Newcastle NSW 2300

Project: Material Testing

Works Component: Thirdi Gorforth Anambah Road

Material Used: -

WB080 - Rev 32, 28/11/2023

Material Description: Refer to logs

Lot Comments:

Lab Test Date/s: Laboratory testing 02/05/2024 to 07/05/2024

Sample Number Sample Date Chainage/Location Offset Level of Test Test Depth
12430 22/04/2024 TP25-P - - 1.50-2.50

Sampling & Test Methods (Results relate only to the items sampled/tested)

Sampled by Customer: Results apply to the sample/s as received. **
AS 1289.3.6.1 Coarse: (2009)Particle size distribution of a soil

AS 1289.3.1.1: (2009)Determination of Liquid Limit (4 point Casagrande)

(** NATA accreditation does not cover the performance of this service)

17-33-MQ

14/05/2024

Page 1 of 2

EP3627

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AS 1289.1.1: (2001)Preparation of disturbed soil samples AS 1289.3.6.1 Fine: (2009)Particle size distribution of a soil

AS 1289.3.2.1: (2009) Determination of the Plastic Limit

Report Remarks & Endorsement



Accredited for compliance with

ISO/IEC 17025 - Testing.

Issued By:

J.Edmunds Approved Signatory

Kelmondo

Lab Site Number: 25677
Base Lab Accreditation: 20656
Base Lab Name: ASCT Illawarra

Specification Name				
Particle Size Distribution (WASHED)	Units	Result	Specification Limits	Graphical Representation
Passing 150mm Sieve	%			Poutiele Ci-e Distuibution
Passing 125mm Sieve	%			Particle Size Distribution
Passing 100mm Sieve	%			
Passing 75.0mm Sieve	%			90
Passing 63.0mm Sieve	%] []
Passing 53.0mm Sieve	%			80
Passing 37.5mm Sieve	%]
Passing 31.5mm Sieve	%			70
Passing 26.5mm Sieve	%			60
Passing 19.0mm Sieve	%	100		(%) (%) (%) (%) (%) (%) (%) (%) (%) (%)
Passing 16.0mm Sieve	%			1
Passing 13.2mm Sieve	%	92		
Passing 9.5mm Sieve	%	86		40
Passing 6.7mm Sieve	%	77		30
Passing 4.75mm Sieve	%	65		
Passing 2.36mm Sieve	%	47		20
Passing 1.18mm Sieve	%	33		
Passing 0.600mm Sieve	%	27		10
Passing 0.425mm Sieve	%	25		
Passing 0.300mm Sieve	%	22		150 75 353,5 26,5,5 119,0 119,0 119,0 119,0 11,1 4,75 2,36 0,60 0,60 0,00 0,00 0,00 0,00 0,00
Passing 0.150mm Sieve	%	18		11. 77. 50 000 8 8 8 8 8 11.
Passing 0.075mm Sieve	%	14		31.5 Sieve Aperture (mm)
Passing 0.0135mm Sieve	%			Sieve Aperture (IIIII)



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Report No:

WB080 - Rev 32, 28/11/2023 Report on Material Quality

Client Address: 3/19 Bolton Street, Newcastle NSW 2300

EP Risk

Project: Material Testing

Works Component: Thirdi Gorforth Anambah Road

Material Used:

Material Description: Refer to logs

Lot Comments:

Client:

Lab Test Date/s: Laboratory testing 02/05/2024 to 07/05/2024

Report Date: 14/05/2024 Report Page: Page 2 of 2 Project No: 17

17-33-MQ

Request/Order: EP3627

Lot Number:

ITP/PCP Number: Control Line: -

Sample NumberSample DateChainage/LocationOffsetLevel of TestTest Depth1243022/04/2024TP25-P--1.50-2.50

Plasticity	Units	Result	Specification Limits	Remarks
Liquid Limit	%	42		Oven Dried & Dry Sieved
Plastic Limit	%	17		Oven Dried & Dry Sieved
Plastic Index	%	25		Oven Dried & Dry Sieved



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Report on AS CBR and MDD

Client Address: 3/19 Bolton Street, Newcastle NSW 2300

Project: **Material Testing**

Works Component: Thirdi Gorforth Anambah Road

Material Used(Source):

Client:

Material Description: Refer to logs

Lot Boundaries:

Laboratory testing 02/05/2024 to 15/05/2024 Lab Test Date/s:

Report No: Report Date: 17-35-CBR

Report Page:

15/05/2024 Page 1 of 1

Project No:

EP3627

Test Request/Order:

Lot Number:

ITP/PCP Number:

Control Line:

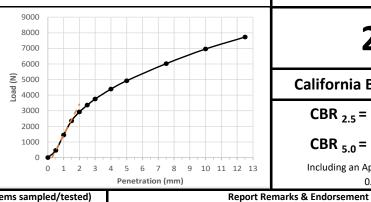
Sample Number	Sample Date	Chainage/Location	Offset	Level of Test	Test Depth
12432	22/04/2024	TP29-P	-		1.50-2.00

Parameters	Units	Test Results		Information
Pretreatment Regime		No Pretreatment		
Portion Retained on AS Sieve	%	1% on 19mm		Retained material excluded from CBR
Material Plasticity (Liquid Limit)		Low (Less than 35%)		By Technician's Assessment
Sample Curing Time	hrs	MDD = 26 hrs	CBR = 89 hrs	
Soil Particle Density	t/m3	2.67		Estimated value only**
Maximum Dry Density (MDD)	t/m3	1.87		Standard compactive effort
Optimum Moisture Content (OMC)	%	15.0		
Field Moisture Content	%	Field 12.5 %		Passing 19.0mm portion
Compaction Moisture Content	%	Achieved 14.6 %	LMR = 99.0%	Specified LMR = 100%
Compaction Dry Density	t/m3	Achieved 1.87 t/m3	LDR = 100.0%	Specified LDR = 100%
Surcharge Load	kg	4.5		
Period of Soaking	Days	Soaked - 4 Days		Dry Density (after soaking) = 1.87 t/m3.
Specimen Swell	%	0.5		
Moisture Content - Top 30mm	%	16.4		After Penetration
Moisture Content - Remaining	%	15.1		After Penetration

Dry Density Vs Moisture Content

1.92 1.90 1.88 1.86 1.84 1.82 1.80 1.78 Dη 1.76 1.74 11.0 12.0 13.0 14.0 15.0 16.0 17.0 18.0 19.0 Moisture Content (%)

Load-Penetration Curve



Material CBR Value (%)

California Bearing Ratios

CBR _{2.5} = 25

CBR _{5.0} = 25

Including an Applied Correction of

Sampling & Test Methods (Results relate only to the items sampled/tested)

Sampled by Customer: Results apply to the sample/s as received. **

AS 1289.1.1: (2001)Preparation of disturbed soil samples

AS1289.2.1.1: (2005) Moisture Content of a Soil (Oven Drying)

AS1289.5.1.1: (2017) Dry Density/Moisture content relation of a soil (Standard)

AS1289.6.1.1: (2014)California Bearing Ratio of a soil (remoulded specimen)

Accredited for compliance with

ISO/IEC 17025 - Testing.

Issued By:

J.Edmunds Approved Signatory

Lab Site Number: 25677 Base Lab Accreditation: 20656

> Base Lab Name: ASCT Illawarra

> > WB011 - Rev 33, 05/02/2024

Celarado



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Report No:

Report Date:

Report Page:

Lot Number: ITP/PCP Number:

Control Line:

Request/Order:

Project No:

Report on Material Quality

Client: EP Risk Client Address: 3/19 Bolton Street, Newcastle NSW 2300

Project: **Material Testing**

Works Component: Thirdi Gorforth Anambah Road

Material Used:

WB080 - Rev 32, 28/11/2023

Material Description: Refer to logs

Lot Comments:

Laboratory testing 02/05/2024 to 06/05/2024 Lab Test Date/s:

Sample Date Offset Test Depth Sample Number Chainage/Location Level of Test 12435 22/04/2024 TP35-P 1.50-2.00

Sampling & Test Methods (Results relate only to the items sampled/tested)

Sampled by Customer: Results apply to the sample/s as received. **

AS 1289.3.6.1 Coarse: (2009)Particle size distribution of a soil

AS 1289.3.1.1: (2009) Determination of Liquid Limit (4 point Casagrande)

AS 1289.3.3.1: (2009)Calculation of the Plastic Index of a soil

(** NATA accreditation does not cover the performance of this service)

17-38-MQ

14/05/2024

Page 1 of 2

EP3627

17

AS 1289.1.1: (2001)Preparation of disturbed soil samples AS 1289.3.6.1 Fine: (2009)Particle size distribution of a soil

AS 1289.3.2.1: (2009) Determination of the Plastic Limit

AS 1289.3.4.1: (2008) Determination of the Linear Shrinkage of a soil

Report Remarks & Endorsement



Accredited for compliance with ISO/IEC 17025 - Testing.

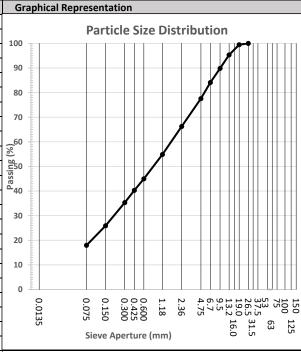
Issued By:

J.Edmunds Approved Signatory

Celmondo

Lab Site Number: 25677 Base Lab Accreditation: 20656 Base Lab Name: ASCT Illawarra

Specification Name				
Particle Size Distribution (WASHED)	Units	Result	Specification Limits	G
Passing 150mm Sieve	%			
Passing 125mm Sieve	%			100
Passing 100mm Sieve	%			100
Passing 75.0mm Sieve	%			90
Passing 63.0mm Sieve	%			
Passing 53.0mm Sieve	%			80
Passing 37.5mm Sieve	%			70
Passing 31.5mm Sieve	%			
Passing 26.5mm Sieve	%	100		% %
Passing 19.0mm Sieve	%	99		%)
Passing 16.0mm Sieve	%			Passing
Passing 13.2mm Sieve	%	95		Pas
Passing 9.5mm Sieve	%	90		41
Passing 6.7mm Sieve	%	84		30
Passing 4.75mm Sieve	%	78		
Passing 2.36mm Sieve	%	66		20
Passing 1.18mm Sieve	%	55		
Passing 0.600mm Sieve	%	45		10
Passing 0.425mm Sieve	%	40		(
Passing 0.300mm Sieve	%	35		
Passing 0.150mm Sieve	%	26		
Passing 0.075mm Sieve	%	18		
Passing 0.0135mm Sieve	%			





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Report No:

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0421 989 919 Mobile: A.B.N. 34 635 062 609

Report on Material Quality

Client: Client Address: 3/19 Bolton Street, Newcastle NSW 2300

EP Risk

Project: **Material Testing**

Works Component: Thirdi Gorforth Anambah Road

Material Used:

Material Description: Refer to logs

Lot Comments:

Laboratory testing 02/05/2024 to 06/05/2024 Lab Test Date/s:

Report Date: 14/05/2024 Report Page: Page 2 of 2

Project No: 17 EP3627

17-38-MQ

Request/Order: Lot Number:

ITP/PCP Number: Control Line:

Sample Date Chainage/Location Offset Level of Test Test Depth Sample Number 12435 22/04/2024 TP35-P 1.50-2.00

Plasticity	Units	Result	Specification Limits	Remarks
Liquid Limit	%	38		Oven Dried & Dry Sieved
Plastic Limit	%	20		Oven Dried & Dry Sieved
Plastic Index	%	18		Oven Dried & Dry Sieved
Linear Shrinkage	%	6.5		



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17-39-CBR

15/05/2024

Page 1 of 1

EP3627

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Report No:

Report Date:

Report Page:

Project No:

Report on AS CBR and MDD

Client Address: 3/19 Bolton Street, Newcastle NSW 2300

Project: **Material Testing**

Works Component: Thirdi Gorforth Anambah Road

Material Used(Source):

Client:

Material Description: Refer to logs

Lot Boundaries:

Laboratory testing 30/04/2024 to 15/05/2024

Lot Number: ITP/PCP Number: Control Line:

Test Request/Order:

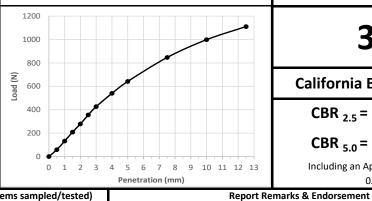
Lab Test Date/s: Sample Number Sample Date Chainage/Location Offset **Level of Test Test Depth** TP37-P 12436 22/04/2024 1.70-2.50

Parameters	Units	Test Results		Information
Pretreatment Regime		No Pretreatment		
Portion Retained on AS Sieve	%	8% on 19mm		Retained material excluded from CBR
Material Plasticity (Liquid Limit)		High (More than 50%)		By Technician's Assessment
Sample Curing Time	hrs	MDD = 96 hrs	CBR = 140 hrs	
Soil Particle Density	t/m3	2.60		Estimated value only**
Maximum Dry Density (MDD)	t/m3	1.34		Standard compactive effort
Optimum Moisture Content (OMC)	%	33.5		
Field Moisture Content	%	Field 31.8 %		Passing 19.0mm portion
Compaction Moisture Content	%	Achieved 33.3 %	LMR = 99.5%	Specified LMR = 100%
Compaction Dry Density	t/m3	Achieved 1.34 t/m3	LDR = 100.0%	Specified LDR = 100%
Surcharge Load	kg	4.5		
Period of Soaking	Days	Soaked - 4 Days		Dry Density (after soaking) = 1.32 t/m3.
Specimen Swell	%	1.5		
Moisture Content - Top 30mm	%	38.5		After Penetration
Moisture Content - Remaining	%	34.8		After Penetration

Dry Density Vs Moisture Content

1.38 1.36 1.34 1.32 1.30 1.28 1.26 1 24 28.0 29.0 30.0 31.0 32.0 33.0 34.0 35.0 36.0 Moisture Content (%)

Load-Penetration Curve



Material CBR Value (%)

California Bearing Ratios

CBR _{2.5} = 2.5

CBR _{5.0} = 3.0

Including an Applied Correction of 0.0 mm

Sampling & Test Methods (Results relate only to the items sampled/tested)

Sampled by Customer: Results apply to the sample/s as received. **

AS 1289.1.1: (2001)Preparation of disturbed soil samples

AS1289.2.1.1: (2005) Moisture Content of a Soil (Oven Drying)

AS1289.5.1.1: (2017) Dry Density/Moisture content relation of a soil (Standard)

AS1289.6.1.1: (2014)California Bearing Ratio of a soil (remoulded specimen)



Issued By:

J.Edmunds

Kelmindo

Accredited for compliance with ISO/IEC 17025 - Testing.

Approved Signatory 25677

Lab Site Number: Base Lab Accreditation: 20656

> Base Lab Name: ASCT Illawarra

> > WB011 - Rev 33, 05/02/2024



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Report on AS CBR and MDD

Client Address: 3/19 Bolton Street, Newcastle NSW 2300

Project: **Material Testing**

Works Component: Thirdi Gorforth Anambah Road

Material Used(Source):

Client:

Material Description: Refer to logs

Lot Boundaries:

Laboratory testing 02/05/2024 to 14/05/2024 Lab Test Date/s:

Report No: 17-40-CBR Report Date: 14/05/2024

Report Page: Page 1 of 1

Project No: 17 Test Request/Order: EP3627

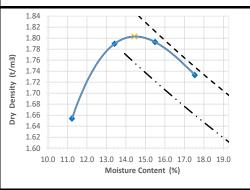
Lot Number: ITP/PCP Number:

Control Line:

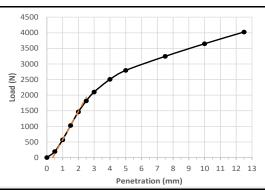
Sample Number	Sample Date	Chainage/Location	Offset	Level of Test	Test Depth
12437	22/04/2024	TP38-P	-	-	1.00-1.75

Parameters	Units	Test Results		Information
Pretreatment Regime		No Pretreatment		
Portion Retained on AS Sieve	%	12% on 19mm		Retained material excluded from CBR
Material Plasticity (Liquid Limit)		Low (Less than 35%)		By Technician's Assessment
Sample Curing Time	hrs	MDD = 24 hrs	CBR = 39 hrs	
Soil Particle Density	t/m3	2.52		Estimated value only**
Maximum Dry Density (MDD)	t/m3	1.80		Standard compactive effort
Optimum Moisture Content (OMC)	%	14.5		
Field Moisture Content	%	Field 12.5 %		Passing 19.0mm portion
Compaction Moisture Content	%	Achieved 14.4 %	LMR = 99.5%	Specified LMR = 100%
Compaction Dry Density	t/m3	Achieved 1.81 t/m3	LDR = 100.5%	Specified LDR = 100%
Surcharge Load	kg	4.5		
Period of Soaking	Days	Soaked - 4 Days		Dry Density (after soaking) = 1.80 t/m3.
Specimen Swell	%	0.5		
Moisture Content - Top 30mm	%	16.9		After Penetration
Moisture Content - Remaining	%	15.7		After Penetration

Dry Density Vs Moisture Content



Load-Penetration Curve



Material CBR Value (%)

California Bearing Ratios

CBR _{2.5} = 15

CBR _{5.0} = 14

Including an Applied Correction of

Sampling & Test Methods (Results relate only to the items sampled/tested)

Sampled by Customer: Results apply to the sample/s as received. **

AS 1289.1.1: (2001)Preparation of disturbed soil samples

AS1289.2.1.1: (2005) Moisture Content of a Soil (Oven Drying)

AS1289.5.1.1: (2017) Dry Density/Moisture content relation of a soil (Standard)

AS1289.6.1.1: (2014)California Bearing Ratio of a soil (remoulded specimen)

Report Remarks & Endorsement



Issued By:

J.Edmunds

Celmondo

Accredited for compliance with ISO/IEC 17025 - Testing.

Approved Signatory

Lab Site Number: 25677 Base Lab Accreditation: 20656

ASCT Illawarra Base Lab Name:

WB011 - Rev 33, 05/02/2024



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Report on Shrink / Swell Index of a Soil

17-21-MQ Client: **EP Risk** Report No: Client Address: 3/19 Bolton Street, Newcastle NSW 2300 Report Date: 14/05/2024 Project: **Material Testing** Report Page: Page 1 of 1

Works Component: Thirdi Gorforth Anambah Road Project No:

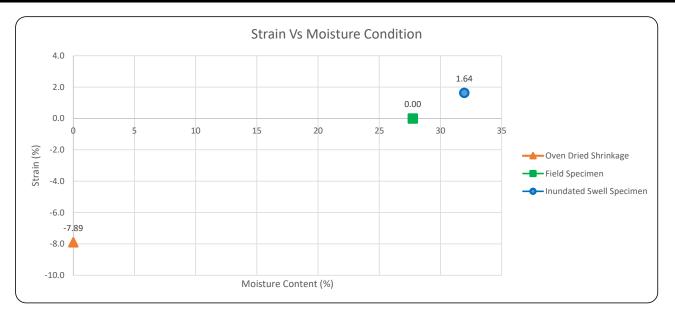
Material Used: Test Request/Order: EP3627

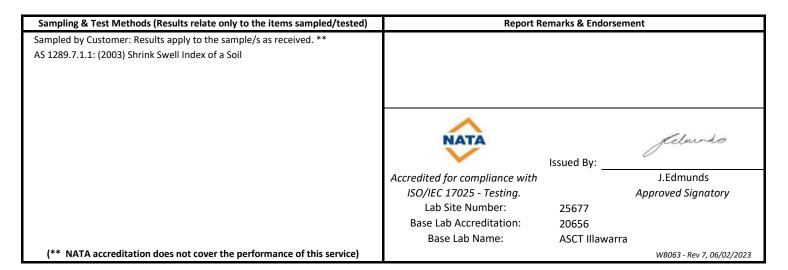
Material Description: Refer to logs Lot Number: Lab Test Date/s: Testing commenced 03/05/2024 and was completed 09/05/2024. ITP/PCP Number:

Lot Comments: Control Line:

Sample Number	Sample Date	Chainage/Location	Offset	Level of Test	Test Depth
12418	22/04/2024	TP01-L	-	-	0.70-1.20

Parameters	Units	Test Results	Soil Description
Shrinkage - Field Moisture Content	%	26.0	
Swell - Field Moisture Content	%	29.5	
Swell - Inundated Moisture Content	%	31.9	
Inert Inclusions in the soil	%	0	CLAY
Extent of Soil Crumbling	-	None	
Extent of Soil Cracking	-	Minor	
Shrink-Swell Index	%	4.8	







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Report on Shrink / Swell Index of a Soil

Client:EP RiskReport No:17-29-MQClient Address:3/19 Bolton Street, Newcastle NSW 2300Report Date:14/05/2024Project:Material TestingReport Page:Page 1 of 1

Works Component: Thirdi Gorforth Anambah Road Project No: 17

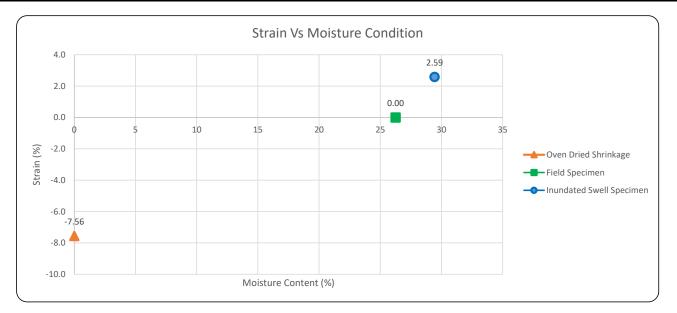
Material Used: - Test Request/Order: EP3627

Material Description: Refer to logs Lot Number: Lab Test Date/s: Testing commenced 03/05/2024 and was completed 09/05/2024. ITP/PCP Number: -

Lab Test Date/s: Testing commenced 03/05/2024 and was completed 09/05/2024. TIP/PCP Number:
Lot Comments: - Control Line: -

Sample Number	Sample Date	Chainage/Location	Offset	Level of Test	Test Depth
12426	22/04/2024	TP19-L	-	-	0.30-0.80

Parameters	Units	Test Results	Soil Description
Shrinkage - Field Moisture Content	%	27.1	
Swell - Field Moisture Content	%	25.4	
Swell - Inundated Moisture Content	%	29.4	
Inert Inclusions in the soil	%	0	CLAY
Extent of Soil Crumbling	-	None	
Extent of Soil Cracking	-	Minor	
Shrink-Swell Index	%	4.9	



Sampling & Test Methods (Results relate only to the items sampled/tested)	Report Remarks & Endorsement						
Sampled by Customer: Results apply to the sample/s as received. ** AS 1289.7.1.1: (2003) Shrink Swell Index of a Soil							
	NATA		felundo				
		Issued By:					
	Accredited for compliance with		J.Edmunds				
	ISO/IEC 17025 - Testing.		Approved Signatory				
	Lab Site Number:	25677					
	Base Lab Accreditation:	20656					
	Base Lab Name:	ASCT Illawarra					
(** NATA accreditation does not cover the performance of this service)			WB063 - Rev 7, 06/02/2023				



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Report on Shrink / Swell Index of a Soil

Client:EP RiskReport No:17-31-MQClient Address:3/19 Bolton Street, Newcastle NSW 2300Report Date:14/05/2024Project:Material TestingReport Page:Page 1 of 1

Works Component: Thirdi Gorforth Anambah Road Project No: 17

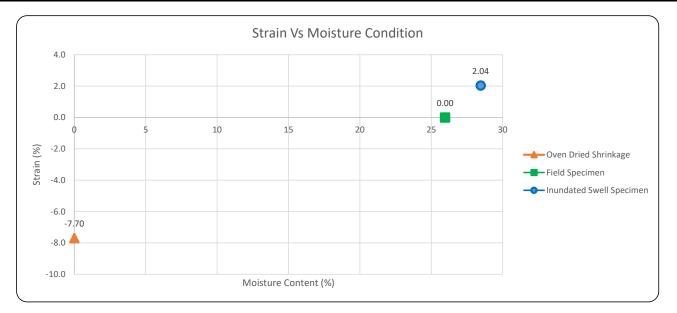
Material Used: Test Request/Order: EP3627

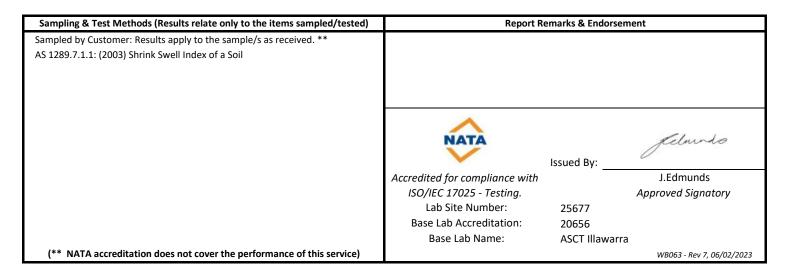
Material Description: Refer to logs Lot Number: -

Lab Test Date/s: Testing commenced 03/05/2024 and was completed 09/05/2024. ITP/PCP Number: Lot Comments: - Control Line: -

Sample Number	Sample Date	Chainage/Location	Offset	Level of Test	Test Depth
12428	22/04/2024	TP23-L	-	-	0.3-0.80

Parameters	Units	Test Results	Soil Description
Shrinkage - Field Moisture Content	%	26.8	
Swell - Field Moisture Content	%	25.1	
Swell - Inundated Moisture Content	%	28.5	
Inert Inclusions in the soil	%	0	CLAY
Extent of Soil Crumbling	-	None	
Extent of Soil Cracking	-	Minor	
Shrink-Swell Index	%	4.8	,







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Sample No:

Report No:

Report Date:

Project No:

ITP/PCP:

Test Request:

Lot Number:

23581

344

EP3627

160A-PL

9/05/2024

TP05-P - 2.50-3.00

0497 979 929 Mobile: A.B.N. 34 635 062 609

Report on the Point Load Strength of Rock

Client: **ASCT Newcastle**

Client Address: 13/31 Riverside Drive, Mayfield West, NSW 2304

Project: **Geotechnical Testing**

Component: EP Risk - Thirdi Gorforth Anambah Road

TP05-P - 2.50-3.00 Material Type:

Material Origin (Source): Unknown

Rock Body Sampled: A sample of rock was submitted to this laboratory, by others.

Date Tested: 7/05/2024 Sampled By Client Sampling Method: Test Method Used: AS 4133.4.1

	The NATA	endors	ement does not includ	le the performance of s	Report Page: 1 of 1		
Parameter	Symbol	Unit		Samp	le Information & Test F	Results	
Individual Rock Piece:			1	2	3	4	5
Lithological Description:			Sedimentary	Sedimentary	Sedimentary	Sedimentary	Sedimentary
Moisture Condition at Test:	:		Moist	Moist	Moist	Moist	Moist
Moisture Storage History:			Specimens w	ere kept in a sealed air-tig	tht container from the poi	nt of sampling (or receipt), until tested.
Test Type:			Lump	Lump	Lump	Lump	Lump
Anisotropic Direction (Note	1):						
Depth / Diameter:	D	(mm)	63.0	58.5	68.5	81.5	64.0
Length:	L	(mm)	-	-	-	-	-
Width:	W	(mm)	93.5	83.5	88.0	87.0	80.0
Uncorrected Point Load Strength:	I_{S}	(MPa)	0.22	0.19	0.19	0.15	0.25
Point Load Strength	I _{S(50)}	(MPa)	0.28	0.23	0.24	0.2	0.31
Index:	-(/				_	_	_
Failure Mode (Note 2):			3	3	3	3	3
Descriptive Strength (Note	3):		Low	Low	Low	Low	Medium

Parameter	Symbol	Unit		Samp	le Information & Test R	Results	
Individual Rock Piece:			6	-	-	-	-
Lithological Description:			Sedimentary	-	-	-	-
Moisture Condition at Test:			Moist	-	-	-	-
Moisture Storage History:			Specimens w	ere kept in a sealed air-tig	tht container from the poi	nt of sampling (or receipt), until tested.
Test Type:			Lump	-	-	-	-
Anisotropic Direction (Note	1):			-	-	-	-
Depth / Diameter:	D	(mm)	59.5	-	-	-	-
Length:	L	(mm)	•	-	-	-	-
Width:	W	(mm)	88.0	-	-	-	-
Uncorrected Point Load Strength:	I_{S}	(MPa)	0.26	-	-	-	-
Point Load Strength Index:	I _{S(50)}	(MPa)	0.32	-	-	-	-
Failure Mode (Note 2):			3	-	-	-	-
Descriptive Strength (Note 3	3):		Medium	-	-	-	-

Mean Point Load Strength Index (MPa)

4133.4.1, Clause 3.2 (a). The value is provided

NATA endorsement.

Note 1 - Anisotropic Direction

Note 2 - Failure Mode 1 Fracture through fabric, oblique to banding.

0.3

Parallel Load applied parallel to banding/foliation.

Anisotropic testing not required/requested.

Load applied at 90° to the banding/foliation. Normal

2 Fracture along banding. 3 Fracture through rock mass.

Mean value calculated in accordance with AS

4J Fracture influenced by Joint Plane. 4M Fracture influenced by $\underline{\mathbf{M}}$ icro-fracture. Note 3 - Descriptive Strength

The strength descriptors used are drawn from T223 (section as information only, and is not included in the 6). They are provided as information only, and are not included

Fracture influenced by **F**oliation. 4F Fracture influenced by Vein. 4V

Invalid Result (Partial fracture, or chip).

Report Remarks / Comments:

Laboratory testing commenced on the 07/05/2024

Accredited for compliance with ISO/IEC 17025 -Testing. The results relate only to the items

P.Baltoski

Approved Signatory WB055 - Rev 11, 20/03/2024

NATA

NATA Accreditation number: 20656

in the NATA endorsement.

Approved By:



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Report on the Point Load Strength of Rock

Client: **ASCT Newcastle**

Client Address: 13/31 Riverside Drive, Mayfield West, NSW 2304

Project: **Geotechnical Testing**

Component: EP Risk - Thirdi Gorforth Anambah Road

Sampled By Client

TP05-P - 2.50-3.00 Material Type:

Sampling Method:

Material Origin (Source): Unknown

Rock Body Sampled: A sample of rock was submitted to this laboratory, by others.

The NATA endorsement does not include the performance of sampling

Sample No: 23581 Report No: 160PL Report Date: 9/05/2024 Project No: 344 Test Request: EP3627 ITP/PCP:

Lot Number: TP05-P - 2.50-3.00

Date Tested: 7/05/2024 Test Method Used: AS 4133.4.1

	The NATA	endors	ement does not includ	e the performance of s	Report Page: 1 of 1			
Parameter	Symbol	Unit	Sample Information & Test Results					
Individual Rock Piece:			1	2	3	4	5	
Lithological Description:			Sedimentary	Sedimentary	Sedimentary	Sedimentary	Sedimentary	
Moisture Condition at Test:			Moist	Moist	Moist	Moist	Moist	
Moisture Storage History:			Specimens we	ere kept in a sealed air-tig	tht container from the po	int of sampling (or receipt), until tested.	
Test Type:			Lump	Lump	Lump	Lump	Lump	
Anisotropic Direction (Note	1):		·					
Depth / Diameter:	D	(mm)	51.0	68.0	47.5	37.5	61.0	
Length:	L	(mm)	-	-	-	-	-	
Width:	W	(mm)	55.0	111.0	78.5	64.5	85.0	
Uncorrected Point Load Strength:	I_{S}	(MPa)	0.29	0.24	0.23	0.42	0.24	
Point Load Strength Index:	I _{S(50)}	(MPa)	0.32	0.32	0.26	0.44	0.3	
Failure Mode (Note 2):			3	3	3	3	3	
Descriptive Strength (Note 3	3):		Medium	Medium	Low	Medium	Low	

Parameter	Symbol	Unit		Samp	le Information & Test F	Results	
Individual Rock Piece:			6	-	-	-	-
Lithological Description:			Sedimentary	-	-	-	-
Moisture Condition at Test:			Moist	•	-	-	-
Moisture Storage History:			Specimens w	ere kept in a sealed air-tig	tht container from the poi	nt of sampling (or receipt), until tested.
Test Type:			Lump	•	-	-	-
Anisotropic Direction (Note	1):			•	-	-	-
Depth / Diameter:	D	(mm)	61.5	-	-	-	-
Length:	L	(mm)	=	•	-	-	-
Width:	W	(mm)	77.5	•	-	-	-
Uncorrected Point Load Strength:	I_{S}	(MPa)	0.23	-	-	-	-
Point Load Strength Index:	I _{S(50)}	(MPa)	0.28	-	-	-	
Failure Mode (Note 2):			3	-	-	-	-
Descriptive Strength (Note 3	3):		Low	-	-	-	-

Mean Point Load Strength Index (MPa)

Note 1 - Anisotropic Direction

Note 3 - Descriptive Strength

in the NATA endorsement.

as information only, and is not included in the 6). They are provided as information only, and are not included

Note 2 - Failure Mode 1 Fracture through fabric, oblique to banding.

0.3

Mean value calculated in accordance with AS

4133.4.1, Clause 3.2 (a). The value is provided

NATA endorsement.

Parallel Load applied parallel to banding/foliation.

Anisotropic testing not required/requested.

Load applied at 90° to the banding/foliation. Normal

The strength descriptors used are drawn from T223 (section

2 Fracture along banding.

3 Fracture through rock mass.

4J Fracture influenced by Joint Plane.

4M Fracture influenced by $\underline{\mathbf{M}}$ icro-fracture.

Fracture influenced by **F**oliation. 4F

Fracture influenced by Vein. 4V

Invalid Result (Partial fracture, or chip).

Report Remarks / Comments:

Laboratory testing commenced on the 07/05/2024

NATA

Accredited for compliance with ISO/IEC 17025 -Testing. The results relate only to the items

> NATA Accreditation number: 20656

Approved By:

P.Baltoski Approved Signatory



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Report on the Point Load Strength of Rock

Client: ASCT Newcastle

Client Address: 13/31 Riverside Drive, Mayfield West, NSW 2304

Project: Geotechnical Testing

Component: EP Risk - Thirdi Gorforth Anambah Road

Material Type: TP28-P - 1.00-1.30

Material Origin (Source): Unknown

Rock Body Sampled: A sample of rock was submitted to this laboratory, by others.

Sampling Method: Sampled By Client

The NATA endorsement does not include the performance of sampling

Project No: 344

Test Request: EP3627

ITP/PCP: -

Sample No:

Report No:

Report Date:

Lot Number: TP28-P - 1.00-1.30

23582

161A-PL

9/05/2024

Date Tested: 8/05/2024
Test Method Used: AS 4133.4.1

Report Page: 1 of 1

	Ine NAIA	endors	ement does not includ	Report Page:	ge: 1 of 1			
Parameter	Symbol	Unit	Sample Information & Test Results					
Individual Rock Piece:			1	2	3	4	5	
Lithological Description:			Sedimentary	Sedimentary	Sedimentary	Sedimentary	Sedimentary	
Moisture Condition at Test:			Moist	Moist	Moist	Moist	Moist	
Moisture Storage History:			Specimens we	ere kept in a sealed air-tig	tht container from the poi	nt of sampling (or receipt), until tested.	
Test Type:			Lump	Lump	Lump	Lump	Lump	
Anisotropic Direction (Note	1):							
Depth / Diameter:	D	(mm)	49.0	84.0	58.5	57.0	48.0	
Length:	L	(mm)	-	-	-	-	-	
Width:	W	(mm)	70.0	84.5	91.0	86.5	70.5	
Uncorrected Point Load Strength:	I_S	(MPa)	0.066	0.2	0.38	0.16	0.61	
Point Load Strength Index:	I _{S(50)}	(MPa)	0.075	0.27	0.48	0.2	0.69	
Failure Mode (Note 2):			3	3	3	3	3	
Descriptive Strength (Note 3	s):		Very Low	Low	Medium	Low	Medium	

Parameter	Symbol	Unit	Sample Information & Test Results						
Individual Rock Piece:			6	-	-	-	-		
Lithological Description:			Sedimentary	-	-	-	-		
Moisture Condition at Test:			Moist	-	-	-	-		
Moisture Storage History:			Specimens were kept in a sealed air-tight container from the point of sampling (or receipt), until tested.						
Test Type:			Lump	-	-	-	-		
Anisotropic Direction (Note	1):			-	-	-	-		
Depth / Diameter:	D	(mm)	48.5	-	-	-	-		
Length:	L	(mm)	-	-	-	-	-		
Width:	W	(mm)	70.0	-	-	-	-		
Uncorrected Point Load Strength:	I_{S}	(MPa)	0.51	-	-	-	-		
Point Load Strength	l _{c(F0)}	(MPa)	0.58	-	-	-	-		
Index:	IS(50)	(4,	U.50						
Failure Mode (Note 2):			3	-	-	-	-		
Descriptive Strength (Note 3	3):		Medium	-	-	-	-		

Mean Point Load Strength Index (MPa)

Note 1 - Anisotropic Direction

Note 3 - Descriptive Strength

in the NATA endorsement.

as information only, and is not included in the 6). They are provided as information only, and are not included

Note 2 - Failure Mode 1 Fracture through fabric, oblique to banding.

0.4

Mean value calculated in accordance with AS

4133.4.1, Clause 3.2 (a). The value is provided

NATA endorsement.

Parallel Load applied parallel to banding/foliation.

The strength descriptors used are drawn from T223 (section

Anisotropic testing not required/requested.

Normal Load applied at 90° to the banding/foliation.

2 Fracture along banding.

Fracture through rock mass.Fracture influenced by <u>Joint Plane</u>.

4M Fracture influenced by <u>M</u>icro-fracture.

4F Fracture influenced by **F**oliation.

4r Fracture influenced by Foliation

4V Fracture influenced by <u>V</u>ein.

5 Invalid Result (Partial fracture, or chip).

Report Remarks / Comments:

Laboratory testing commenced on the 08/05/2024

NATA

Accredited for compliance with ISO/IEC 17025 -Testing. The results relate only to the items

NATA Accreditation number: 20656

Approved By:

P.Baltoski Approved Signatory



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Report on the Point Load Strength of Rock

Client: **ASCT Newcastle** Client Address: 13/31 Riverside Drive, Mayfield West, NSW 2304

Project: **Geotechnical Testing**

Component: EP Risk - Thirdi Gorforth Anambah Road

TP28-P - 1.00-1.30 Material Type:

Material Origin (Source): Unknown

Rock Body Sampled: A sample of rock was submitted to this laboratory, by others.

Sampled By Client Sampling Method:

Report No: 161PL Report Date: 9/05/2024 Project No: 344 Test Request: EP3627 ITP/PCP:

Sample No:

Lot Number: TP28-P - 1.00-1.30 8/05/2024 Date Tested:

23582

Test Method Used: AS 4133.4.1

	The NATA	endorse	ment does not includ	le the performance of	sampling.	Report Page:	1 of 1
Parameter	Symbol	Unit		Samp	le Information & Test I	Results	
Individual Rock Piece:			1	2	3	4	5
Lithological Description:			Sedimentary	Sedimentary	Sedimentary	Sedimentary	Sedimentary
Moisture Condition at Test:	:		Moist	Moist	Moist	Moist	Moist
Moisture Storage History:			Specimens w	ere kept in a sealed air-ti	ght container from the po	int of sampling (or receipt), until tested.
Test Type:			Lump	Lump	Lump	Lump	Lump
Anisotropic Direction (Note	1):						
Depth / Diameter:	D	(mm)	52.5	61.5	72.5	80.0	65.0
Length:	L	(mm)	-	-	-	-	-
Width:	W	(mm)	92.5	67.0	80.5	87.0	77.5
Uncorrected Point Load Strength:	I_{S}	(MPa)	0.61	0.88	0.67	0.63	0.24
Point Load Strength Index:	I _{S(50)}	(MPa)	0.75	1	0.86	0.83	0.3
Failure Mode (Note 2):			3	3	3	3	3
Descriptive Strength (Note	3):		Medium	High	Medium	Medium	Medium

Parameter	Symbol	Unit		Samp	le Information & Test F	Results	
Individual Rock Piece:		Î	6	-	-	-	-
Lithological Description:			Sedimentary	-	-	-	-
Moisture Condition at Test:			Moist	-	-	-	-
Moisture Storage History:			Specimens w	ere kept in a sealed air-tig	tht container from the poi	nt of sampling (or receipt), until tested.
Test Type:			Lump	-	-	-	-
Anisotropic Direction (Note	1):			-	-	-	-
Depth / Diameter:	D	(mm)	64.0	•	-	-	-
Length:	L	(mm)	-	-	-	-	-
Width:	W	(mm)	102.0	•	-	-	-
Uncorrected Point Load Strength:	I_{S}	(MPa)	0.64	-	-	-	-
Point Load Strength Index:	I _{S(50)}	(MPa)	0.84	-	-	-	-
Failure Mode (Note 2):			3	-	-	-	-
Descriptive Strength (Note 3	3):		Medium	-	-	-	-

Note 1 - Anisotropic Direction

Note 2 - Failure Mode Anisotropic testing not required/requested. 1

0.8

4133.4.1, Clause 3.2 (a). The value is provided

NATA endorsement.

Parallel Load applied parallel to banding/foliation. Load applied at 90° to the banding/foliation. Normal

Note 3 - Descriptive Strength Mean value calculated in accordance with AS

The strength descriptors used are drawn from T223 (section as information only, and is not included in the 6). They are provided as information only, and are not included in the NATA endorsement.

Fracture through fabric, oblique to banding.

2 Fracture along banding.

3 Fracture through rock mass. 4J Fracture influenced by Joint Plane.

4M Fracture influenced by $\underline{\mathbf{M}}$ icro-fracture.

Fracture influenced by **F**oliation. 4F

Fracture influenced by Vein. 4V

Invalid Result (Partial fracture, or chip).

Report Remarks / Comments:

Laboratory testing commenced on the 08/05/2024

NATA

Accredited for compliance with ISO/IEC 17025 -Testing. The results relate only to the items

> NATA Accreditation number: 20656

Approved By:

P.Baltoski Approved Signatory



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Report on the Point Load Strength of Rock

Client: **ASCT Newcastle**

Client Address: 13/31 Riverside Drive, Mayfield West, NSW 2304

Project: **Geotechnical Testing**

Component: EP Risk - Thirdi Gorforth Anambah Road

Sampled By Client

TP32-P - 0.50-1.20 Material Type:

Material Origin (Source): Unknown

Sampling Method:

Rock Body Sampled: A sample of rock was submitted to this laboratory, by others.

Report No: 162A-PL Report Date: 9/05/2024 Project No: 344 Test Request: EP3627 ITP/PCP:

Sample No:

Lot Number:

TP32-P - 0.50-1.20

23583

Date Tested: 8/05/2024 Test Method Used: AS 4133.4.1

	The NATA	endors	ement does not includ	le the performance of s	sampling.	Report Page: 1 of 1		
Parameter	Symbol	Unit		Samp	le Information & Test F	Results		
Individual Rock Piece:			1	2	3	4	5	
Lithological Description:			Sedimentary	Sedimentary	Sedimentary	Sedimentary	Sedimentary	
Moisture Condition at Test:			Moist	Moist	Moist	Moist	Moist	
Moisture Storage History: Specimens were kept in a sealed air-tight container from the point of sampling (or receipt), until tested.								
Test Type:			Lump	Lump	Lump	Lump	Lump	
Anisotropic Direction (Note	1):							
Depth / Diameter:	D	(mm)	61.5	46.5	68.0	66.0	39.0	
Length:	L	(mm)	=	-	-	-	=	
Width:	W	(mm)	84.5	83.5	75.0	90.5	69.0	
Uncorrected Point Load Strength:	I_{S}	(MPa)	0.42	0.24	0.14	0.17	0.74	
Point Load Strength Index:	I _{S(50)}	(MPa)	0.52	0.28	0.17	0.22	0.8	
Failure Mode (Note 2):			3	3	3	3	3	
Descriptive Strength (Note:	3):	Ī	Medium	Low	Low	Low	Medium	

Parameter	Symbol	Unit	Sample Information & Test Results						
Individual Rock Piece:			6	-	-	-	-		
Lithological Description:			Sedimentary	-	-	-	-		
Moisture Condition at Test:			Moist	-	-	-	-		
Moisture Storage History:			Specimens w	Specimens were kept in a sealed air-tight container from the point of sampling (or receipt), until tested.					
Test Type:			Lump	-	-	-	-		
Anisotropic Direction (Note	1):			-	-	-	-		
Depth / Diameter:	D	(mm)	68.5	-	-	-	-		
Length:	L	(mm)	-	-	-	-	-		
Width:	W	(mm)	66.5	-	-	-	-		
Uncorrected Point Load Strength:	I_{S}	(MPa)	0.3	-	-	-	-		
Point Load Strength		(0.4D-)	0.36						
Index:	IS(50)	(MPa)	0.30	_	-	_	-		
Failure Mode (Note 2):			3	-	-	-	-		
Descriptive Strength (Note:	3):		Medium	-	-	-	-		

Mean Point Load Strength Index (MPa)

0.3

Mean value calculated in accordance with AS

4133.4.1, Clause 3.2 (a). The value is provided

NATA endorsement.

Note 1 - Anisotropic Direction

Note 3 - Descriptive Strength

in the NATA endorsement.

as information only, and is not included in the 6). They are provided as information only, and are not included

Note 2 - Failure Mode 1 Fracture through fabric, oblique to banding.

Parallel Load applied parallel to banding/foliation.

Anisotropic testing not required/requested.

Load applied at 90° to the banding/foliation. Normal

The strength descriptors used are drawn from T223 (section

2 Fracture along banding.

3

Fracture through rock mass.

4J Fracture influenced by Joint Plane. 4M Fracture influenced by $\underline{\mathbf{M}}$ icro-fracture.

Fracture influenced by **F**oliation. 4F

Fracture influenced by Vein. 4V

Invalid Result (Partial fracture, or chip).

Report Remarks / Comments:

Laboratory testing commenced on the 08/05/2024

NATA

Accredited for compliance with ISO/IEC 17025 -Testing. The results relate only to the items

> NATA Accreditation number: 20656

Approved By:

P.Baltoski Approved Signatory



A.B.N.

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34 635 062 609

E-Mail: illawarra@asct.com.au Mobile: 0497 979 929

Report on the Point Load Strength of Rock

Client: **ASCT Newcastle**

Client Address: 13/31 Riverside Drive, Mayfield West, NSW 2304

Project: **Geotechnical Testing**

Component: EP Risk - Thirdi Gorforth Anambah Road

TP32-P - 0.50-1.20 Material Type:

Material Origin (Source): Unknown Rock Body Sampled: A sample of rock was submitted to this laboratory, by others.

Date Tested:

Sampled By Client Sampling Method: The NATA endorsement does not include the performance of sampling.

23583 Sample No: Report No: 162PL Report Date: 9/05/2024

Project No: 344 Test Request: EP3627

ITP/PCP:

Lot Number: TP32-P - 0.50-1.20

8/05/2024 Test Method Used: AS 4133.4.1

> 1 of 1 Report Page:

•	Unit	Sample Information & Test Results						
		1	2	3	4	5		
		Sedimentary	Sedimentary	Sedimentary	Sedimentary	Sedimentary		
		Moist	Moist	Moist	Moist	Moist		
		Specimens we	ere kept in a sealed air-tig	ht container from the poi	nt of sampling (or receipt), until tested.		
		Lump	Lump	Lump	Lump	Lump		
L) :								
D	(mm)	53.0	61.5	62.0	65.5	67.0		
L	(mm)	=	=	=	-	-		
W	(mm)	78.0	84.0	88.5	85.0	85.0		
I_S	(MPa)	0.22	0.28	0.34	0.29	0.47		
	(84De)	0.26	0.25	0.42	0.27	0.6		
S(50)	(IVIPa)	0.26	0.55	0.45	0.57	0.6		
		3	3	3	3	3		
) :		Low	Medium	Medium	Medium	Medium		
	L W	D (mm) L (mm) W (mm) I _S (MPa) I _{S(50)} (MPa)	Moist Specimens we Lump 1): D (mm) 53.0 L (mm) - W (mm) 78.0 I _S (MPa) 0.22 I _{S(50)} (MPa) 0.26 3	Sedimentary Sedimentary Moist Moist Specimens were kept in a sealed air-tig Lump Lump Lump	Sedimentary Sedimentary Sedimentary Moist Moist Moist Moist Specimens were kept in a sealed air-tight container from the point Lump Lump	Sedimentary Sedimentary Sedimentary Sedimentary Moist Moist Moist Moist Moist Moist Moist Moist Specimens were kept in a sealed air-tight container from the point of sampling (or receipt Lump Lump		

Parameter	Symbol	Unit		Samp	le Information & Test F	Results	
Individual Rock Piece:		Î	6	-	-	-	-
Lithological Description:			Sedimentary	-	-	-	-
Moisture Condition at Test:			Moist	-	-	-	-
Moisture Storage History:			Specimens w	ere kept in a sealed air-tig	tht container from the poi	int of sampling (or receipt), until tested.
Test Type:			Lump	-	-	-	-
Anisotropic Direction (Note	1):			-	-	-	-
Depth / Diameter:	D	(mm)	59.0	•	-	-	-
Length:	L	(mm)	-	-	-	-	-
Width:	W	(mm)	76.5	•	-	-	-
Uncorrected Point Load Strength:	I_{S}	(MPa)	1.2	-	-	-	-
Point Load Strength Index:	I _{S(50)}	(MPa)	1.5	-	-	-	-
Failure Mode (Note 2):			3	-	-	-	-
Descriptive Strength (Note 3	3):		High	-	-	-	-

Mean Point Load Strength Index (MPa)

Mean value calculated in accordance with AS

4133.4.1, Clause 3.2 (a). The value is provided

NATA endorsement.

Note 1 - Anisotropic Direction Anisotropic testing not required/requested.

Note 3 - Descriptive Strength

in the NATA endorsement.

as information only, and is not included in the 6). They are provided as information only, and are not included

Note 2 - Failure Mode 1 Fracture through fabric, oblique to banding.

0.4

Parallel Load applied parallel to banding/foliation.

Normal Load applied at 90° to the banding/foliation.

The strength descriptors used are drawn from T223 (section

2

Fracture along banding.

3 Fracture through rock mass. 4J Fracture influenced by Joint Plane.

4M Fracture influenced by $\underline{\mathbf{M}}$ icro-fracture.

4F Fracture influenced by **F**oliation. Fracture influenced by Vein. 4V

Invalid Result (Partial fracture, or chip).

Report Remarks / Comments:

Laboratory testing commenced on the 08/05/2024

NATA

Accredited for compliance with ISO/IEC 17025 -Testing. The results relate only to the items

> NATA Accreditation number: 20656

Approved By:

P.Baltoski Approved Signatory



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Mobile: 0497 979 929 A.B.N. 34 635 062 609

Report on the Point Load Strength of Rock

Client: **ASCT Newcastle** Client Address: 13/31 Riverside Drive, Mayfield West, NSW 2304

Project: **Geotechnical Testing**

Component: EP Risk - Thirdi Gorforth Anambah Road

Sampled By Client

TP33-P - 1.00-1.80 Material Type:

Material Origin (Source): Unknown

Sampling Method:

Descriptive Strength (Note 3):

Rock Body Sampled: A sample of rock was submitted to this laboratory, by others.

The NATA endorsement does not include the performance of sampling.

Very Low

23584 Sample No: Report No: 163A-PL Report Date: 9/05/2024 Project No: 344 Test Request: EP3627

illawarra@asct.com.au

ITP/PCP:

TP33-P - 1.00-1.80 Lot Number:

Extremeley Low

9/05/2024 Date Tested: Test Method Used: AS 4133.4.1

1 of 1 Report Page: Unit Sample Information & Test Results Parameter Symbol Individual Rock Piece: 1 3 Lithological Description: Sedimentary Sedimentary Sedimentary Sedimentary Sedimentary Moisture Condition at Test: Moist Moist Moist Moist Moist Moisture Storage History: Specimens were kept in a sealed air-tight container from the point of sampling (or receipt), until tested. Lump Test Type: Lump Lump Lump Lump Anisotropic Direction (Note 1): 81.0 62.0 44.0 53.0 50.5 Depth / Diameter: D (mm) Length: (mm) 82.0 100.5 68.0 87.0 89.0 L Width: (mm) 53.5 70.0 49.5 77.0 90.0 W Uncorrected Point Load 0.48 0.29 0.085 0.019 0.033 (MPa) Strength: **Point Load Strength** 0.039 0.57 0.29 0.1 0.023 I_{S(50)} (MPa) Index: Failure Mode (Note 2): 3 3

Parameter	Symbol	Unit		Samp	le Information & Test F	Results	
Individual Rock Piece:		Î	6	-	-	-	-
Lithological Description:			Sedimentary	-	-	-	-
Moisture Condition at Test:			Moist	-	-	-	-
Moisture Storage History:			Specimens w	ere kept in a sealed air-tig	tht container from the poi	nt of sampling (or receipt), until tested.
Test Type:			Lump	•	-	-	=
Anisotropic Direction (Note	1):			-	-	-	-
Depth / Diameter:	D	(mm)	54.0	•	-	-	=
Length:	L	(mm)	97.0	-	-	-	-
Width:	W	(mm)	69.5	-	-	-	-
Uncorrected Point Load Strength:	I_{S}	(MPa)	0.2	-	-	-	-
Point Load Strength Index:	I _{S(50)}	(MPa)	0.24	-	-	-	-
Failure Mode (Note 2):			3	-	-	-	-
Descriptive Strength (Note 3	3):		Low	-	-	-	-

Medium

Low

Mean Point Load Strength Index (MPa)

Note 1 - Anisotropic Direction Anisotropic testing not required/requested.

included in the NATA endorsement.

1 Fracture through fabric, oblique to banding.

Fracture influenced by Joint Plane.

0.2

Mean value calculated in accordance with AS

4133.4.1, Clause 3.2 (a). The value is provided

as information only, and is not included in the

NATA endorsement.

Parallel Load applied parallel to banding/foliation. Load applied at 90° to the banding/foliation. Normal

3 Fracture through rock mass.

Note 2 - Failure Mode

2

4J

Note 3 - Descriptive Strength The strength descriptors used are drawn from T223 (section

6). They are provided as information only, and are not

4M Fracture influenced by $\underline{\mathbf{M}}$ icro-fracture.

Very Low

Fracture influenced by **F**oliation. 4F

Fracture along banding.

Fracture influenced by Vein. 4V

Invalid Result (Partial fracture, or chip).

Report Remarks / Comments:

Laboratory testing commenced on the 09/05/2024

NATA

Accredited for compliance with ISO/IEC 17025 -Testing. The results relate only to the items

> NATA Accreditation number: 20656 Approved By:

P.Baltoski Approved Signatory



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Sample No:

Report No:

Report Date:

Test Request:

Lot Number:

Project No:

ITP/PCP:

23584

163PL

EP3627

344

9/05/2024

9/05/2024

TP33-P - 1.00-1.80

E-Mail: illawarra@asct.com.au 0497 979 929 Mobile: A.B.N. 34 635 062 609

Report on the Point Load Strength of Rock

Client: **ASCT Newcastle** Client Address: 13/31 Riverside Drive, Mayfield West, NSW 2304

Project: **Geotechnical Testing**

Component: EP Risk - Thirdi Gorforth Anambah Road

TP33-P - 1.00-1.80 Material Type:

Material Origin (Source): Unknown

Rock Body Sampled: A sample of rock was submitted to this laboratory, by others.

Date Tested: Sampling Method:

Sampled By Client Test Method Used: AS 4133.4.1 The NATA endorsement does not include the performance of sampling. Report Page: 1 of 1

	IIIE NAIA	enuorse	ment does not includ	e the periormance of s	amping.	Nepoltrage. 1011			
Parameter	Symbol	Unit		Samp	le Information & Test I	Results			
Individual Rock Piece:			1	2	3	4	5		
Lithological Description:			Sedimentary	Sedimentary	Sedimentary	Sedimentary	Sedimentary		
Moisture Condition at Test:			Dry	Dry	Dry	Dry	Dry		
Moisture Storage History:			Specimens we	ere kept in a sealed air-tig	in a sealed air-tight container from the point of sampling (or receipt), until tested.				
Test Type:			Lump	Lump	Lump	Lump	Lump		
Anisotropic Direction (Note	1):								
Depth / Diameter:	D	(mm)	50.5	50.5	63.0	48.5	47.5		
Length:	L	(mm)	-	-	-	-	-		
Width:	W	(mm)	69.0	73.0	73.5	68.5	60.0		
Uncorrected Point Load Strength:	I_{S}	(MPa)	0.31	0.25	0.3	0.8	0.21		
Point Load Strength Index:	I _{S(50)}	(MPa)	0.35	0.29	0.36	0.9	0.22		
Failure Mode (Note 2):			1	1	1	1	1		
Descriptive Strength (Note 3	3):		Medium	Low	Medium	Medium	Low		

Parameter	Symbol	Unit	Sample Information & Test Results						
Individual Rock Piece:			6	-	-	-	-		
Lithological Description:			Sedimentary	-	-	-	-		
Moisture Condition at Test:			Dry	-	-	-	-		
Moisture Storage History:			Specimens were kept in a sealed air-tight container from the point of sampling (or receipt), until tested.						
Test Type:			Lump	-	-	-	-		
Anisotropic Direction (Note	1):			-	-	-	-		
Depth / Diameter:	D	(mm)	64.5	-	-	-	-		
Length:	L	(mm)	-	-	-	-	-		
Width:	W	(mm)	91.0	-	-	-	-		
Uncorrected Point Load Strength:	I_{S}	(MPa)	0.13	-	-	-	-		
Point Load Strength		(04Da)	0.17						
Index:	^I S(50)	(MPa)	0.17	-	<u>-</u>	-	_		
Failure Mode (Note 2):			1	-	-	-	-		
Descriptive Strength (Note 3	3):		Low	-	-	-	-		

Mean Point Load Strength Index (MPa)

0.3

Mean value calculated in accordance with AS

4133.4.1, Clause 3.2 (a). The value is provided

as information only, and is not included in the

NATA endorsement.

Note 1 - Anisotropic Direction

Anisotropic testing not required/requested. 1 Fracture through fabric, oblique to banding.

Note 2 - Failure Mode

Parallel Load applied parallel to banding/foliation.

Load applied at 90° to the banding/foliation. Normal

2 Fracture along banding. 3 Fracture through rock mass.

4J Fracture influenced by Joint Plane.

4M Fracture influenced by $\underline{\mathbf{M}}$ icro-fracture. Note 3 - Descriptive Strength The strength descriptors used are drawn from T223 (section Fracture influenced by **F**oliation. 4F

6). They are provided as information only, and are not Fracture influenced by Vein. 4V

included in the NATA endorsement. Invalid Result (Partial fracture, or chip).

Report Remarks / Comments:

Laboratory testing commenced on the 09/05/2024

NATA

Accredited for compliance with ISO/IEC 17025 -Testing. The results relate only to the items

> NATA Accreditation number: 20656

Approved By:

P.Baltoski Approved Signatory



Environment Testing

EP Risk Management (NSW) 80 Mount Street, North Sydney NSW 2060





NATA Accredited Accreditation Number 1261 Site Number 18217

Accredited for compliance with ISO/IEC 17025 – Testing NATA is a signatory to the ILAC Mutual Recognition Arrangement for the mutual recognition of the equivalence of testing, medical testing, calibration, inspection, proficiency testing scheme providers and reference materials producers reports and certificates.

Attention: Ovidiu Pruteanu

Report1090775-SProject nameGOSFORTHProject IDEP3627Received DateApr 24, 2024

Client Sample ID			TP11-L-2.8-3.0	TP36-L-2.8-3.0	TP40-P-2.8-3.0	
Sample Matrix			Soil	Soil	Soil	
Eurofins Sample No.			N24- Ap0063563	N24- Ap0063564	N24- Ap0063565	
Date Sampled			Apr 22, 2024	Apr 23, 2024	Apr 24, 2024	
Test/Reference	LOR	Unit				
Chloride	10	mg/kg	100	100	220	
Conductivity (1:5 aqueous extract at 25 °C as rec.)	10	uS/cm	130	150	310	
pH (1:5 Aqueous extract at 25 °C as rec.)	0.1	pH Units	9.0	8.7	9.5	
Resistivity*	0.5	ohm.m	75	68	32	
Sulphate (as SO4)	10	mg/kg	< 25	< 25	< 25	
Sample Properties						
% Moisture	1	%	7.4	8.6	10.0	

Report Number: 1090775-S



Environment Testing

Sample History

Where samples are submitted/analysed over several days, the last date of extraction is reported.

If the date and time of sampling are not provided, the Laboratory will not be responsible for compromised results should testing be performed outside the recommended holding time.

Description	Testing Site	Extracted	Holding Time
Chloride	Sydney	Apr 30, 2024	28 Days
- Method: In-house method LTM-INO-4090 Chloride by Discrete Analyser			
Conductivity (1:5 aqueous extract at 25 °C as rec.)	Sydney	Apr 30, 2024	7 Days
- Method: LTM-INO-4030 Conductivity			
pH (1:5 Aqueous extract at 25 °C as rec.)	Sydney	Apr 30, 2024	7 Days
- Method: LTM-GEN-7090 pH by ISE			
Sulphate (as SO4)	Sydney	Apr 30, 2024	28 Days
- Method: In-house method LTM-INO-4110 Sulphate by Discrete Analyser			
% Moisture	Sydney	Apr 24, 2024	14 Days
Mark A TAM OF N TOO MARK			



Eurofins Environment Testing Australia Pty Ltd

ABN: 50 005 085 521

Melbourne Geelong Sydney Canberra 6 Monterey Road 19/8 Lewalan Street 179 Magowar Road Unit 1,2 Dacre Street 1/21 Smallwood Place 1/2 Frost Drive Dandenong South Grovedale Girraween Mitchell VIC 3175 VIC 3216 NSW 2145 ACT 2911 +61 2 9900 8400 +61 3 8564 5000 +61 3 8564 5000 +61 2 6113 8091 NATA# 1261 NATA# 1261 NATA# 1261 NATA# 1261 Site# 1254 Site# 25403 Site# 18217 Site# 25466

Brisbane Newcastle Murarrie Mayfield West QLD 4172 NSW 2304 T: +61 7 3902 4600 +61 2 4968 8448 NATA# 1261 NATA# 1261 Site# 25079 & 25289 Site# 20794

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Company Name:

email: EnviroSales@eurofins.com

web: www.eurofins.com.au

EP Risk Management (Newcastle)

Address: 80 Mount Street.

North Sydney

NSW 2060

Project Name: Project ID:

GOSFORTH EP3627

EP3627 Order No.: Report #:

Phone: Fax:

1090775 02 99225021

Received: Apr 24, 2024 2:05 PM

Due: May 2, 2024 **Priority:** 5 Day

Contact Name: Ovidiu Pruteanu

Eurofins Analytical Services Manager: Bonnie Pu

	Sample Detail				Aggressivity Soil Set	Moisture Set	
Sydr	Sydney Laboratory - NATA # 1261 Site # 18217				Χ	Х	
Exte	External Laboratory						
No	Sample ID	Sample Date	Sampling Time	Matrix	LAB ID		
1	TP11-L-2.8-3.0	Apr 22, 2024		Soil	N24-Ap0063563	Χ	Х
2	TP36-L-2.8-3.0	Apr 23, 2024		Soil	N24-Ap0063564	Χ	Х
3	TP40-L-2.8-3.0	Apr 24, 2024		Soil	N24-Ap0063565	Χ	Х
Test	Counts					3	3



Internal Quality Control Review and Glossary

General

- 1. Laboratory QC results for Method Blanks, Duplicates, Matrix Spikes, and Laboratory Control Samples follow guidelines delineated in the National Environment Protection (Assessment of Site Contamination) Measure 1999, as amended May 2013. They are included in this QC report where applicable. Additional QC data may be available on request
- 2. Unless otherwise stated, all soil/sediment/solid results are reported on a dry weight basis.
- 3. Unless otherwise stated, all biota/food results are reported on a wet weight basis on the edible portion.
- 4. For CEC results where the sample's origin is unknown or environmentally contaminated, the results should be used advisedly.
- Actual LORs are matrix dependent. Quoted LORs may be raised where sample extracts are diluted due to interferences
- Results are uncorrected for matrix spikes or surrogate recoveries except for PFAS compounds where annotated.
- 7. SVOC analysis on waters is performed on homogenised, unfiltered samples unless noted otherwise.
- 8. Samples were analysed on an 'as received' basis.
- 9. Information identified in this report with blue colour indicates data provided by customers that may have an impact on the results.
- 10. This report replaces any interim results previously issued.

Holding Times

Please refer to the 'Sample Preservation and Container Guide' for holding times (QS3001).

For samples received on the last day of holding time, notification of testing requirements should have been received at least 6 hours before sample receipt deadlines as stated on the SRA

If the Laboratory did not receive the information in the required timeframe, and despite any other integrity issues, suitably qualified results may still be reported.

Holding times apply from the sampling date: therefore, compliance with these may be outside the laboratory's control.

For VOCs containing vinyl chloride, styrene and 2-chloroethyl vinyl ether, the holding time is seven days; however, for all other VOCs, such as BTEX or C6-10 TRH, the holding time is 14 days

Units

mg/kg: milligrams per kilogram mg/L: milligrams per litre ppm: parts per million μg/L: micrograms per litre ppb: parts per billion %: Percentage

org/100 mL: Organisms per 100 millilitres NTU: Nephelometric Turbidity Units MPN/100 mL: Most Probable Number of organisms per 100 millilitres

Colour: Pt-Co Units (CU) CFU: Colony Forming Unit

Terms

APHA American Public Health Association CEC Cation Exchange Capacity COC Chain of Custody

CP Client Parent - QC was performed on samples pertaining to this report CRM Certified Reference Material (ISO17034) - reported as percent recovery.

Dry Where moisture has been determined on a solid sample, the result is expressed on a dry weight basis

Duplicate A second piece of analysis from the same sample and reported in the same units as the result to show comparison.

LOR Limit of Reporting.

LCS Laboratory Control Sample - reported as percent recovery.

Method Blank In the case of solid samples, these are performed on laboratory-certified clean sands and in the case of water samples, these are performed on de-ionised water Non-Client Parent - QC performed on samples not pertaining to this report, QC represents the sequence or batch that client samples were analysed within. NCP

RPD Relative Percent Difference between two Duplicate pieces of analysis SPIKE Addition of the analyte to the sample and reported as percentage recovery

SRA Sample Receipt Advice

The addition of a similar compound to the analyte target is reported as percentage recovery. See below for acceptance criteria Surr - Surrogate

Tributyltin oxide (bis-tributyltin oxide) - individual tributyltin compounds cannot be identified separately in the environment; however, free tributyltin was measured, and its values were converted stoichiometrically into tributyltin oxide for comparison with regulatory limits. TRTO

TCI P Toxicity Characteristic Leaching Procedure TEQ Toxic Equivalency Quotient or Total Equivalence

QSM US Department of Defense Quality Systems Manual Version 6.0

US EPA United States Environmental Protection Agency

WA DWER Sum of PFBA, PFPeA, PFHxA, PFHpA, PFOA, PFBS, PFHxS, PFOS, 6:2 FTSA, 8:2 FTSA

QC - Acceptance Criteria

The acceptance criteria should only be used as a guide and may be different when site-specific Sampling Analysis and Quality Plan (SAQP) have been implemented.

RPD Duplicates: Global RPD Duplicates Acceptance Criteria is ≤30%; however, the following acceptance guidelines are equally applicable:

Results <10 times the LOR: No Limit

Results between 10-20 times the LOR: RPD must lie between 0-50% Results >20 times the LOR: RPD must lie between 0-30%

NOTE: pH duplicates are reported as a range, not as RPD

Surrogate Recoveries: Recoveries must lie between 20-130% for Speciated Phenols & 50-150% for PFAS. SVOCs recoveries 20 - 150%, VOC recoveries 50 - 150%

PFAS field samples containing surrogate recoveries above the QC limit designated in QSM 6.0, where no positive PFAS results have been reported or reviewed, and no data was affected.

QC Data General Comments

- 1. Where a result is reported as less than (<), higher than the nominated LOR, this is due to either matrix interference, extract dilution required due to interferences or contaminant levels within the sample, high moisture content or insufficient sample provided
- 2. Duplicate data shown within this report that states the word "BATCH" is a Batch Duplicate from outside of your sample batch but within the laboratory sample batch at a 1:10 ratio. The Parent and Duplicate data shown are not data from your samples.
- 3. pH and Free Chlorine analysed in the laboratory Analysis on this test must begin within 30 minutes of sampling. Therefore, laboratory analysis is unlikely to be completed within holding time. Analysis will begin as soon as possible after sample receipt.
- 4. Recovery Data (Spikes & Surrogates) where chromatographic interference does not allow the determination of recovery, the term "INT" appears against that analyte.
- 5. For Matrix Spikes and LCS results, a dash "-" in the report means that the specific analyte was not added to the QC sample.
- 6. Duplicate RPDs are calculated from raw analytical data; thus, it is possible to have two sets of data



Environment Testing

Quality Control Results

Test			Units	Result 1			Acceptance Limits	Pass Limits	Qualifying Code
Method Blank									
Conductivity (1:5 aqueous extract a	t 25 °C as rec.)		uS/cm	< 10			10	Pass	
Method Blank									
Chloride			mg/kg	< 10			10	Pass	
LCS - % Recovery									
Conductivity (1:5 aqueous extract a	t 25 °C as rec.)		%	98			70-130	Pass	
Resistivity*			%	98			70-130	Pass	
LCS - % Recovery									
Chloride			%	101			70-130	Pass	
Sulphate (as SO4)			%	102			70-130	Pass	
Test	Lab Sample ID	QA Source	Units	Result 1			Acceptance Limits	Pass Limits	Qualifying Code
Spike - % Recovery									
				Result 1					
Chloride	R24-Ap0063424	NCP	%	103			70-130	Pass	
Sulphate (as SO4)	R24-Ap0063424	NCP	%	107			70-130	Pass	
Test	Lab Sample ID	QA Source	Units	Result 1			Acceptance Limits	Pass Limits	Qualifying Code
Duplicate									
				Result 1	Result 2	RPD			
Conductivity (1:5 aqueous extract at 25 °C as rec.)	R24-Ap0063424	NCP	uS/cm	< 10	< 10	<1	30%	Pass	
pH (1:5 Aqueous extract at 25 °C as rec.)	S24-My0000098	NCP	pH Units	5.5	5.6	<1	30%	Pass	
Resistivity*	R24-Ap0063424	NCP	ohm.m	2000	2400	20	30%	Pass	
Duplicate									
				Result 1	Result 2	RPD			
Chloride	N24-Ap0063565	CP	mg/kg	220	230	1.8	30%	Pass	
Sulphate (as SO4)	N24-Ap0063565	СР	mg/kg	< 25	< 25	<1	30%	Pass	



Environment Testing

Comments

Sample Integrity

Custody Seals Intact (if used)

Attempt to Chill was evident

No
Sample correctly preserved

Appropriate sample containers have been used

Yes
Sample containers for volatile analysis received with minimal headspace

Samples received within HoldingTime

Yes
Some samples have been subcontracted

No

Authorised by:

Nileshni Goundar Analytical Services Manager Ryan Phillips Senior Analyst-Inorganic



Glenn Jackson Managing Director

Final Report - this report replaces any previously issued Report

- Indicates Not Requested
- * Indicates NATA accreditation does not cover the performance of this service

Measurement uncertainty of test data is available on request or please click here.

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Project Name: Project ID:

GOSFORTH EP3627

EP3627 Order No.: Report #:

Phone: Fax:

1090775

02 99225021

Received: Apr 24, 2024 2:05 PM Due: May 2, 2024

Priority: 5 Day

Ovidiu Pruteanu **Contact Name:**

Eurofins Analytical Services Manager: Bonnie Pu

	Sample Detail				Aggressivity Soil Set	Moisture Set	
Sydney Laboratory - NATA # 1261 Site # 18217					Χ	Х	
External Laboratory							
No	Sample ID	Sample Date	Sampling Time	Matrix	LAB ID		
1	TP11-L-2.8-3.0	Apr 22, 2024		Soil	N24-Ap0063563	Χ	Х
2	TP36-L-2.8-3.0	Apr 23, 2024		Soil	N24-Ap0063564	Χ	Х
3	TP40-L-2.8-3.0	Apr 24, 2024		Soil	N24-Ap0063565	Χ	Х
Гest	Counts					3	3

CHAIN OF CUSTODY RECORD Episodos Episod	Unit F3 Bld.F 16 Mars Road Lane Cove West NSW 2066 02 9900 8400 EnviroSampleNSW@eurofins.com	Brisbane Laboratory Unit 1 21 Smallwood Place Murame QLD 4172	Perth Laboratory Unit 2 91 Leach Highway Kewdale WA	Melbourne Laboratory 6 Moniterey Road Dandenong South VIC 3175
NEWCASTIE 2300	Project Name Grasfarth	07.350/4600 EnviroSampleQLD@eurofins.com Project Manager EDD Format Field II, ED255 et	08 9251 9600 EnviroSampleWA@au	rofins.com 03.8564.5000 EnviroSampleVic@eurofins.com
Contact Name Ovidiu Prutanu PHone Ne 0497875336 Special Directions	RESTUCTS			Containers Change continue & Required Turnaround Time (TAT) Extra transfer and tra
Purchase Order EP 3627 Quote ID Na Ne Client Sample ID Sampled Batter DeterTime Society Sampley Schrim Water	Ų D		500mL Plastic	250mL Plastic 725mL Plastic 725mL Plastic 725mL Plastic 725mL Plastic 725mL VoA vial 725mL VoA vial 725mL VoA vial 725mL VoA vial 725mL Plastic 725mL VoA vial 725mL Plastic 725mL VoA vial 725mL Plastic 725mL Plas
TP11-12-2-3-0 22/04 TP36-L 2-8-3-0 23/04	X			1 Dangerous Goods Hazard Warning
TP40-L 2-8-30 29/04	×			
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Appendix F FOUNDATION MAINTENANCE AND FOOTING PERFOMANCE

Foundation Maintenance and Footing Performance: A Homeowner's Guide



BTF 18 replaces Information Sheet 10/91

Buildings can and often do move. This movement can be up, down, lateral or rotational. The fundamental cause of movement in buildings can usually be related to one or more problems in the foundation soil. It is important for the homeowner to identify the soil type in order to ascertain the measures that should be put in place in order to ensure that problems in the foundation soil can be prevented, thus protecting against building movement.

This Building Technology File is designed to identify causes of soil-related building movement, and to suggest methods of prevention of resultant cracking in buildings.

Soil Types

The types of soils usually present under the topsoil in land zoned for residential buildings can be split into two approximate groups – granular and clay. Quite often, foundation soil is a mixture of both types. The general problems associated with soils having granular content are usually caused by erosion. Clay soils are subject to saturation and swell/shrink problems.

Classifications for a given area can generally be obtained by application to the local authority, but these are sometimes unreliable and if there is doubt, a geotechnical report should be commissioned. As most buildings suffering movement problems are founded on clay soils, there is an emphasis on classification of soils according to the amount of swell and shrinkage they experience with variations of water content. The table below is Table 2.1 from AS 2870, the Residential Slab and Footing Code.

Causes of Movement

Settlement due to construction

There are two types of settlement that occur as a result of construction:

- Immediate settlement occurs when a building is first placed on its foundation soil, as a result of compaction of the soil under the weight of the structure. The cohesive quality of clay soil mitigates against this, but granular (particularly sandy) soil is susceptible.
- Consolidation settlement is a feature of clay soil and may take
 place because of the expulsion of moisture from the soil or because
 of the soil's lack of resistance to local compressive or shear stresses.
 This will usually take place during the first few months after
 construction, but has been known to take many years in
 exceptional cases.

These problems are the province of the builder and should be taken into consideration as part of the preparation of the site for construction. Building Technology File 19 (BTF 19) deals with these problems.

Erosion

All soils are prone to erosion, but sandy soil is particularly susceptible to being washed away. Even clay with a sand component of say 10% or more can suffer from erosion.

Saturation

This is particularly a problem in clay soils. Saturation creates a bog-like suspension of the soil that causes it to lose virtually all of its bearing capacity. To a lesser degree, sand is affected by saturation because saturated sand may undergo a reduction in volume – particularly imported sand fill for bedding and blinding layers. However, this usually occurs as immediate settlement and should normally be the province of the builder.

Seasonal swelling and shrinkage of soil

All clays react to the presence of water by slowly absorbing it, making the soil increase in volume (see table below). The degree of increase varies considerably between different clays, as does the degree of decrease during the subsequent drying out caused by fair weather periods. Because of the low absorption and expulsion rate, this phenomenon will not usually be noticeable unless there are prolonged rainy or dry periods, usually of weeks or months, depending on the land and soil characteristics.

The swelling of soil creates an upward force on the footings of the building, and shrinkage creates subsidence that takes away the support needed by the footing to retain equilibrium.

Shear failure

This phenomenon occurs when the foundation soil does not have sufficient strength to support the weight of the footing. There are two major post-construction causes:

- Significant load increase.
- Reduction of lateral support of the soil under the footing due to erosion or excavation.
- In clay soil, shear failure can be caused by saturation of the soil adjacent to or under the footing.

GENERAL DEFINITIONS OF SITE CLASSES					
Class	Foundation				
A	Most sand and rock sites with little or no ground movement from moisture changes				
S	Slightly reactive clay sites with only slight ground movement from moisture changes				
M	Moderately reactive clay or silt sites, which can experience moderate ground movement from moisture changes				
Н	Highly reactive clay sites, which can experience high ground movement from moisture changes				
Е	Extremely reactive sites, which can experience extreme ground movement from moisture changes				
A to P	Filled sites				
P	Sites which include soft soils, such as soft clay or silt or loose sands; landslip; mine subsidence; collapsing soils; soils subject to erosion; reactive sites subject to abnormal moisture conditions or sites which cannot be classified otherwise				

Tree root growth

Trees and shrubs that are allowed to grow in the vicinity of footings can cause foundation soil movement in two ways:

- Roots that grow under footings may increase in cross-sectional size, exerting upward pressure on footings.
- Roots in the vicinity of footings will absorb much of the moisture in the foundation soil, causing shrinkage or subsidence.

Unevenness of Movement

The types of ground movement described above usually occur unevenly throughout the building's foundation soil. Settlement due to construction tends to be uneven because of:

- Differing compaction of foundation soil prior to construction.
- Differing moisture content of foundation soil prior to construction.

Movement due to non-construction causes is usually more uneven still. Erosion can undermine a footing that traverses the flow or can create the conditions for shear failure by eroding soil adjacent to a footing that runs in the same direction as the flow.

Saturation of clay foundation soil may occur where subfloor walls create a dam that makes water pond. It can also occur wherever there is a source of water near footings in clay soil. This leads to a severe reduction in the strength of the soil which may create local shear failure.

Seasonal swelling and shrinkage of clay soil affects the perimeter of the building first, then gradually spreads to the interior. The swelling process will usually begin at the uphill extreme of the building, or on the weather side where the land is flat. Swelling gradually reaches the interior soil as absorption continues. Shrinkage usually begins where the sun's heat is greatest.

Effects of Uneven Soil Movement on Structures

Erosion and saturation

Erosion removes the support from under footings, tending to create subsidence of the part of the structure under which it occurs. Brickwork walls will resist the stress created by this removal of support by bridging the gap or cantilevering until the bricks or the mortar bedding fail. Older masonry has little resistance. Evidence of failure varies according to circumstances and symptoms may include:

- Step cracking in the mortar beds in the body of the wall or above/below openings such as doors or windows.
- Vertical cracking in the bricks (usually but not necessarily in line with the vertical beds or perpends).

Isolated piers affected by erosion or saturation of foundations will eventually lose contact with the bearers they support and may tilt or fall over. The floors that have lost this support will become bouncy, sometimes rattling ornaments etc.

Seasonal swelling/shrinkage in clay

Swelling foundation soil due to rainy periods first lifts the most exposed extremities of the footing system, then the remainder of the perimeter footings while gradually permeating inside the building footprint to lift internal footings. This swelling first tends to create a dish effect, because the external footings are pushed higher than the internal ones.

The first noticeable symptom may be that the floor appears slightly dished. This is often accompanied by some doors binding on the floor or the door head, together with some cracking of cornice mitres. In buildings with timber flooring supported by bearers and joists, the floor can be bouncy. Externally there may be visible dishing of the hip or ridge lines.

As the moisture absorption process completes its journey to the innermost areas of the building, the internal footings will rise. If the spread of moisture is roughly even, it may be that the symptoms will temporarily disappear, but it is more likely that swelling will be uneven, creating a difference rather than a disappearance in symptoms. In buildings with timber flooring supported by bearers and joists, the isolated piers will rise more easily than the strip footings or piers under walls, creating noticeable doming of flooring.



As the weather pattern changes and the soil begins to dry out, the external footings will be first affected, beginning with the locations where the sun's effect is strongest. This has the effect of lowering the external footings. The doming is accentuated and cracking reduces or disappears where it occurred because of dishing, but other cracks open up. The roof lines may become convex.

Doming and dishing are also affected by weather in other ways. In areas where warm, wet summers and cooler dry winters prevail, water migration tends to be toward the interior and doming will be accentuated, whereas where summers are dry and winters are cold and wet, migration tends to be toward the exterior and the underlying propensity is toward dishing.

Movement caused by tree roots

In general, growing roots will exert an upward pressure on footings, whereas soil subject to drying because of tree or shrub roots will tend to remove support from under footings by inducing shrinkage.

Complications caused by the structure itself

Most forces that the soil causes to be exerted on structures are vertical – i.e. either up or down. However, because these forces are seldom spread evenly around the footings, and because the building resists uneven movement because of its rigidity, forces are exerted from one part of the building to another. The net result of all these forces is usually rotational. This resultant force often complicates the diagnosis because the visible symptoms do not simply reflect the original cause. A common symptom is binding of doors on the vertical member of the frame.

Effects on full masonry structures

Brickwork will resist cracking where it can. It will attempt to span areas that lose support because of subsided foundations or raised points. It is therefore usual to see cracking at weak points, such as openings for windows or doors.

In the event of construction settlement, cracking will usually remain unchanged after the process of settlement has ceased.

With local shear or erosion, cracking will usually continue to develop until the original cause has been remedied, or until the subsidence has completely neutralised the affected portion of footing and the structure has stabilised on other footings that remain effective.

In the case of swell/shrink effects, the brickwork will in some cases return to its original position after completion of a cycle, however it is more likely that the rotational effect will not be exactly reversed, and it is also usual that brickwork will settle in its new position and will resist the forces trying to return it to its original position. This means that in a case where swelling takes place after construction and cracking occurs, the cracking is likely to at least partly remain after the shrink segment of the cycle is complete. Thus, each time the cycle is repeated, the likelihood is that the cracking will become wider until the sections of brickwork become virtually independent.

With repeated cycles, once the cracking is established, if there is no other complication, it is normal for the incidence of cracking to stabilise, as the building has the articulation it needs to cope with the problem. This is by no means always the case, however, and monitoring of cracks in walls and floors should always be treated seriously.

Upheaval caused by growth of tree roots under footings is not a simple vertical shear stress. There is a tendency for the root to also exert lateral forces that attempt to separate sections of brickwork after initial cracking has occurred.

The normal structural arrangement is that the inner leaf of brickwork in the external walls and at least some of the internal walls (depending on the roof type) comprise the load-bearing structure on which any upper floors, ceilings and the roof are supported. In these cases, it is internally visible cracking that should be the main focus of attention, however there are a few examples of dwellings whose external leaf of masonry plays some supporting role, so this should be checked if there is any doubt. In any case, externally visible cracking is important as a guide to stresses on the structure generally, and it should also be remembered that the external walls must be capable of supporting themselves.

Effects on framed structures

Timber or steel framed buildings are less likely to exhibit cracking due to swell/shrink than masonry buildings because of their flexibility. Also, the doming/dishing effects tend to be lower because of the lighter weight of walls. The main risks to framed buildings are encountered because of the isolated pier footings used under walls. Where erosion or saturation cause a footing to fall away, this can double the span which a wall must bridge. This additional stress can create cracking in wall linings, particularly where there is a weak point in the structure caused by a door or window opening. It is, however, unlikely that framed structures will be so stressed as to suffer serious damage without first exhibiting some or all of the above symptoms for a considerable period. The same warning period should apply in the case of upheaval. It should be noted, however, that where framed buildings are supported by strip footings there is only one leaf of brickwork and therefore the externally visible walls are the supporting structure for the building. In this case, the subfloor masonry walls can be expected to behave as full brickwork walls.

Effects on brick veneer structures

Because the load-bearing structure of a brick veneer building is the frame that makes up the interior leaf of the external walls plus perhaps the internal walls, depending on the type of roof, the building can be expected to behave as a framed structure, except that the external masonry will behave in a similar way to the external leaf of a full masonry structure.

Water Service and Drainage

Where a water service pipe, a sewer or stormwater drainage pipe is in the vicinity of a building, a water leak can cause erosion, swelling or saturation of susceptible soil. Even a minuscule leak can be enough to saturate a clay foundation. A leaking tap near a building can have the same effect. In addition, trenches containing pipes can become watercourses even though backfilled, particularly where broken rubble is used as fill. Water that runs along these trenches can be responsible for serious erosion, interstrata seepage into subfloor areas and saturation.

Pipe leakage and trench water flows also encourage tree and shrub roots to the source of water, complicating and exacerbating the problem.

Poor roof plumbing can result in large volumes of rainwater being concentrated in a small area of soil:

 Incorrect falls in roof guttering may result in overflows, as may gutters blocked with leaves etc.

- · Corroded guttering or downpipes can spill water to ground.
- Downpipes not positively connected to a proper stormwater collection system will direct a concentration of water to soil that is directly adjacent to footings, sometimes causing large-scale problems such as erosion, saturation and migration of water under the building.

Seriousness of Cracking

In general, most cracking found in masonry walls is a cosmetic nuisance only and can be kept in repair or even ignored. The table below is a reproduction of Table C1 of AS 2870.

AS 2870 also publishes figures relating to cracking in concrete floors, however because wall cracking will usually reach the critical point significantly earlier than cracking in slabs, this table is not reproduced here.

Prevention/Cure

Plumbing

Where building movement is caused by water service, roof plumbing, sewer or stormwater failure, the remedy is to repair the problem. It is prudent, however, to consider also rerouting pipes away from the building where possible, and relocating taps to positions where any leakage will not direct water to the building vicinity. Even where gully traps are present, there is sometimes sufficient spill to create erosion or saturation, particularly in modern installations using smaller diameter PVC fixtures. Indeed, some gully traps are not situated directly under the taps that are installed to charge them, with the result that water from the tap may enter the backfilled trench that houses the sewer piping. If the trench has been poorly backfilled, the water will either pond or flow along the bottom of the trench. As these trenches usually run alongside the footings and can be at a similar depth, it is not hard to see how any water that is thus directed into a trench can easily affect the foundation's ability to support footings or even gain entry to the subfloor area.

Ground drainage

In all soils there is the capacity for water to travel on the surface and below it. Surface water flows can be established by inspection during and after heavy or prolonged rain. If necessary, a grated drain system connected to the stormwater collection system is usually an easy solution

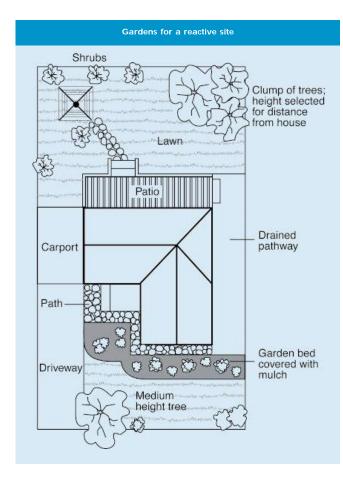
It is, however, sometimes necessary when attempting to prevent water migration that testing be carried out to establish watertable height and subsoil water flows. This subject is referred to in BTF 19 and may properly be regarded as an area for an expert consultant.

Protection of the building perimeter

It is essential to remember that the soil that affects footings extends well beyond the actual building line. Watering of garden plants, shrubs and trees causes some of the most serious water problems.

For this reason, particularly where problems exist or are likely to occur, it is recommended that an apron of paving be installed around as much of the building perimeter as necessary. This paving

CLASSIFICATION OF DAMAGE WITH REFERENCE TO WALLS Description of typical damage and required repair **Damage** Approximate crack width limit (see Note 3) category Hairline cracks < 0.1 mm 0 Fine cracks which do not need repair <1 mm 1 Cracks noticeable but easily filled. Doors and windows stick slightly <5 mm 2 Cracks can be repaired and possibly a small amount of wall will need 5-15 mm (or a number of cracks 3 to be replaced. Doors and windows stick. Service pipes can fracture. 3 mm or more in one group) Weathertightness often impaired Extensive repair work involving breaking-out and replacing sections of walls, 15-25 mm but also depend 4 especially over doors and windows. Window and door frames distort. Walls lean on number of cracks or bulge noticeably, some loss of bearing in beams. Service pipes disrupted



should extend outwards a minimum of 900 mm (more in highly reactive soil) and should have a minimum fall away from the building of 1:60. The finished paving should be no less than 100 mm below brick vent bases.

It is prudent to relocate drainage pipes away from this paving, if possible, to avoid complications from future leakage. If this is not practical, earthenware pipes should be replaced by PVC and backfilling should be of the same soil type as the surrounding soil and compacted to the same density.

Except in areas where freezing of water is an issue, it is wise to remove taps in the building area and relocate them well away from the building – preferably not uphill from it (see BTF 19).

It may be desirable to install a grated drain at the outside edge of the paving on the uphill side of the building. If subsoil drainage is needed this can be installed under the surface drain.

Condensation

In buildings with a subfloor void such as where bearers and joists support flooring, insufficient ventilation creates ideal conditions for condensation, particularly where there is little clearance between the floor and the ground. Condensation adds to the moisture already present in the subfloor and significantly slows the process of drying out. Installation of an adequate subfloor ventilation system, either natural or mechanical, is desirable.

Warning: Although this Building Technology File deals with cracking in buildings, it should be said that subfloor moisture can result in the development of other problems, notably:

- Water that is transmitted into masonry, metal or timber building elements causes damage and/or decay to those elements.
- High subfloor humidity and moisture content create an ideal environment for various pests, including termites and spiders.
- Where high moisture levels are transmitted to the flooring and walls, an increase in the dust mite count can ensue within the living areas. Dust mites, as well as dampness in general, can be a health hazard to inhabitants, particularly those who are abnormally susceptible to respiratory ailments.

The garden

The ideal vegetation layout is to have lawn or plants that require only light watering immediately adjacent to the drainage or paving edge, then more demanding plants, shrubs and trees spread out in that order.

Overwatering due to misuse of automatic watering systems is a common cause of saturation and water migration under footings. If it is necessary to use these systems, it is important to remove garden beds to a completely safe distance from buildings.

Existing trees

Where a tree is causing a problem of soil drying or there is the existence or threat of upheaval of footings, if the offending roots are subsidiary and their removal will not significantly damage the tree, they should be severed and a concrete or metal barrier placed vertically in the soil to prevent future root growth in the direction of the building. If it is not possible to remove the relevant roots without damage to the tree, an application to remove the tree should be made to the local authority. A prudent plan is to transplant likely offenders before they become a problem.

Information on trees, plants and shrubs

State departments overseeing agriculture can give information regarding root patterns, volume of water needed and safe distance from buildings of most species. Botanic gardens are also sources of information. For information on plant roots and drains, see Building Technology File 17.

Excavation

Excavation around footings must be properly engineered. Soil supporting footings can only be safely excavated at an angle that allows the soil under the footing to remain stable. This angle is called the angle of repose (or friction) and varies significantly between soil types and conditions. Removal of soil within the angle of repose will cause subsidence.

Remediation

Where erosion has occurred that has washed away soil adjacent to footings, soil of the same classification should be introduced and compacted to the same density. Where footings have been undermined, augmentation or other specialist work may be required. Remediation of footings and foundations is generally the realm of a specialist consultant.

Where isolated footings rise and fall because of swell/shrink effect, the homeowner may be tempted to alleviate floor bounce by filling the gap that has appeared between the bearer and the pier with blocking. The danger here is that when the next swell segment of the cycle occurs, the extra blocking will push the floor up into an accentuated dome and may also cause local shear failure in the soil. If it is necessary to use blocking, it should be by a pair of fine wedges and monitoring should be carried out fortnightly.

This BTF was prepared by John Lewer FAIB, MIAMA, Partner, Construction Diagnosis.

The information in this and other issues in the series was derived from various sources and was believed to be correct when published.

The information is advisory. It is provided in good faith and not claimed to be an exhaustive treatment of the relevant subject.

Further professional advice needs to be obtained before taking any action based on the information provided.

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